

Mass transfer in semi-aqueous MEA for CO₂ Capture

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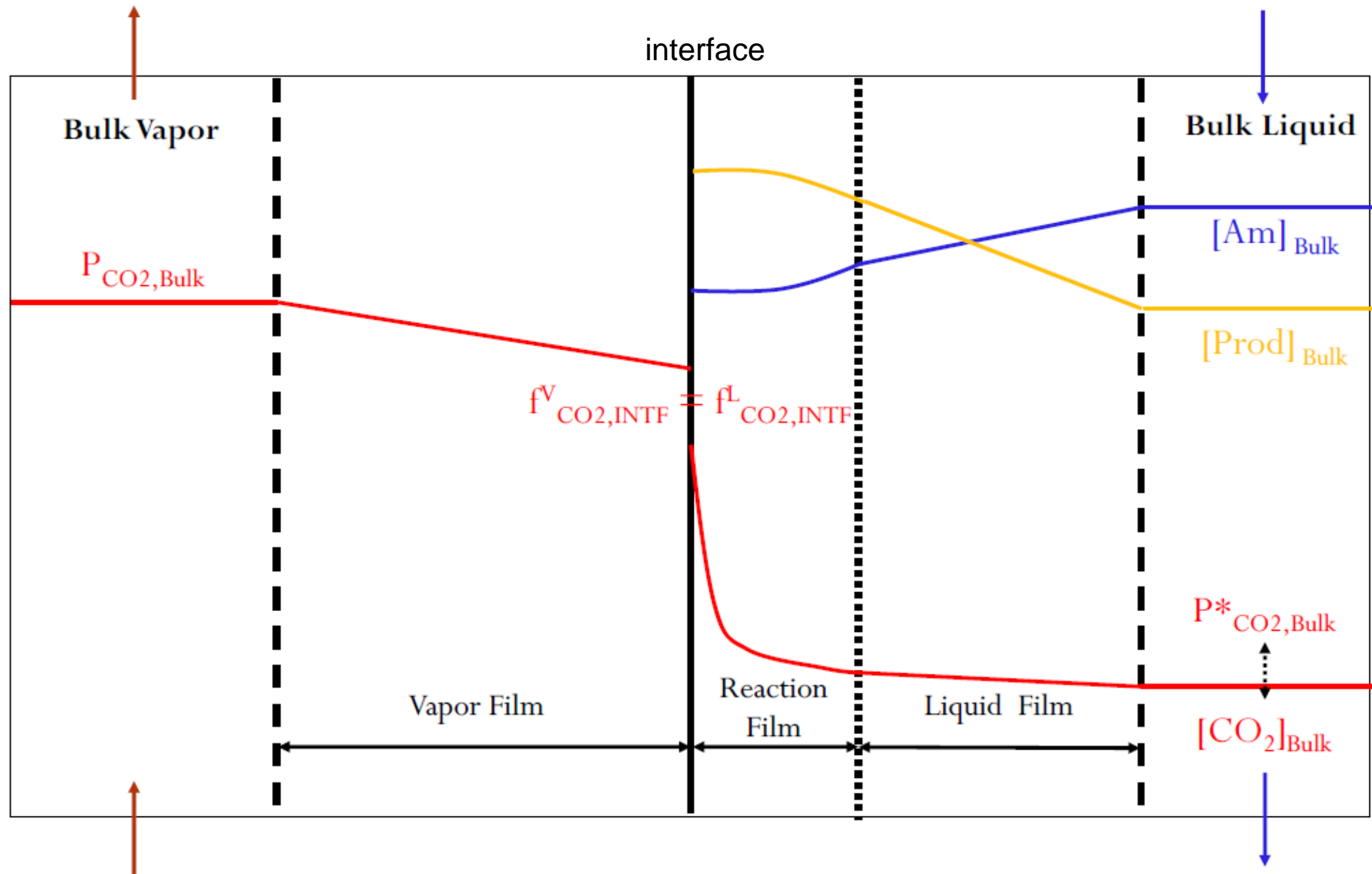
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- **Introduction:**
 - CO₂ diffuse and react with amine
 - MEA_(semi-aq): MEA-physical solvent-water
- **Theory**
- **Experiment Method**
 - WWC, FTIR, N₂O analogy
- **Results**
- **Conclusion**



Mass balance: CO₂ reacts with amine



$$\frac{dc_i}{dt} = -Di \frac{d^2c_i}{dx^2} + V_i * R$$

$$R = k_3 * a_{CO_2} * a_{MEA}^2 - \frac{k_3}{K_{eq}} a_{MEACOO^-} * a_{MEAH^+}$$

$$a_i = \gamma_i * C_i$$

- $i = CO_2, MEA, MEACOO^-, MEAH^+$
- Can't solve analytically
- Can be solved with assumptions (PFO)

Solve k_g' by film theory and PFO (Danckwerts, 1970)

- [amine] \gg [CO₂], constant
- Pseudo First Order (PFO)

$$D_{CO_2} \frac{\partial^2 [CO_2]}{\partial x^2} - k[Am]^2 [CO_2] = 0$$

$$N_{CO_2} = \frac{\sqrt{D_{CO_2} k} * [Am]}{H_{CO_2-solution}} (P_{CO_2,i} - P_{CO_2,b}^*)$$

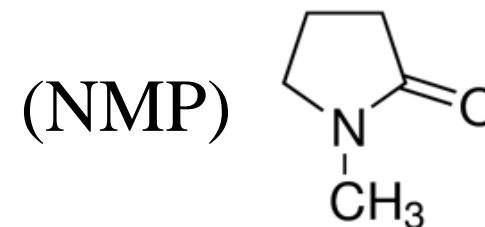
$$k_g' = \frac{\sqrt{D_{CO_2} k_3} * [Am]}{\gamma_{CO_2} H_{CO_2}}$$

activity based

$$k_g' = \frac{\sqrt{D_{CO_2} k_3} * a_{am}}{\gamma_{CO_2}^{0.5} H_{CO_2}}$$

Semi-aqueous amine, Why higher k_g' ?

Amine-water-physical solvent



$$k_g' = \frac{\sqrt{D_{CO_2} k_3} * a_{am}}{\gamma_{CO_2}^{0.5} H_{CO_2}}$$

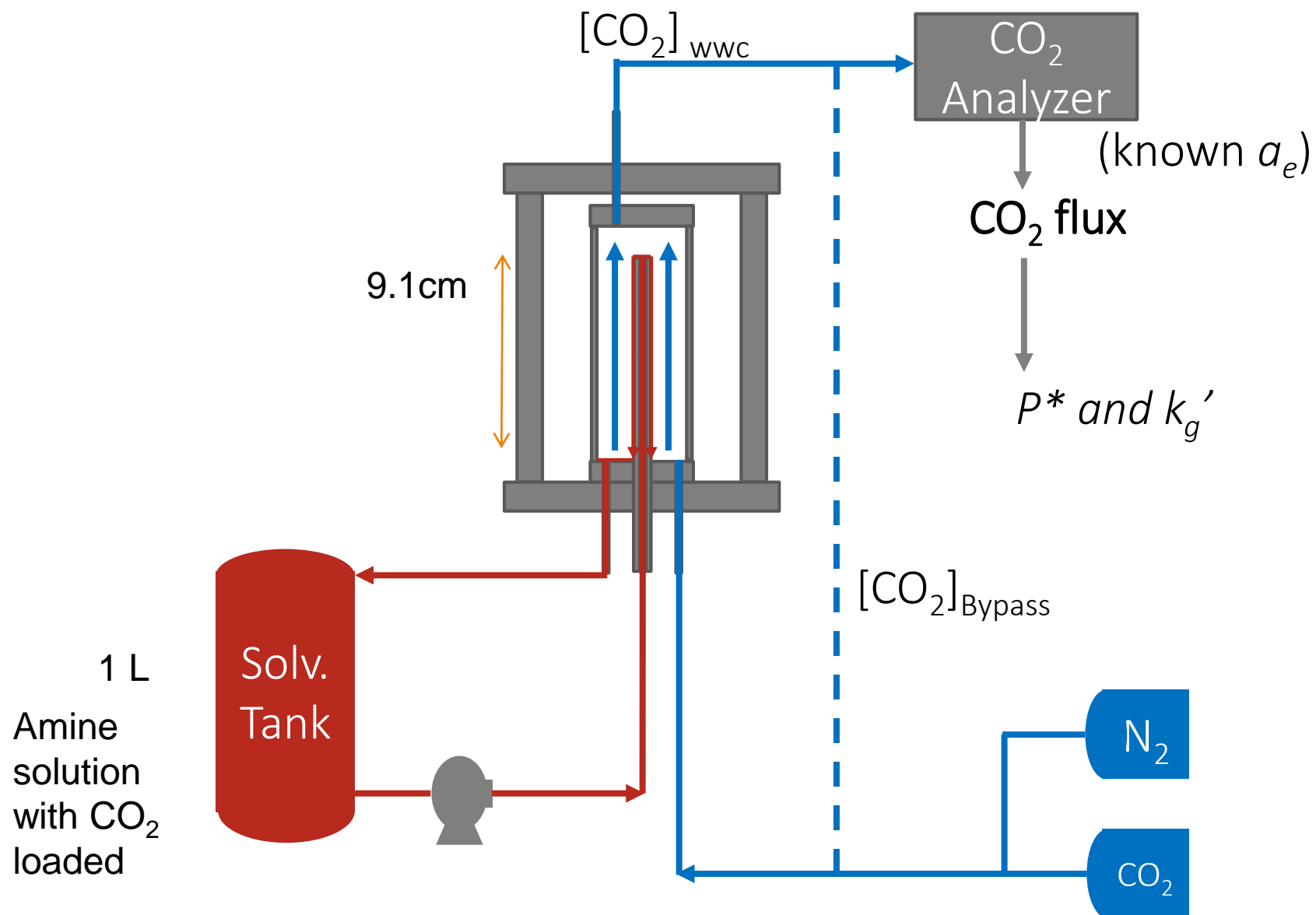
Hypothesis

- γ_{CO_2} reduced, k_g' increase
- a_{am} increase, k_g' increase
- Viscosity increase, D_{CO_2} decrease, k_g' decrease

Experiment method

- k_g ' & $P_{CO_2}^*$
by the WWC
- γ_{CO_2} ,
by N_2O analogy
- a_{am} ,
by FTIR

Wetted Wall Column (WWC)



Measuring CO₂ physical solubility using N₂O analogy (Versteeg 1988)

$$H_{CO_2-solution} = \frac{H_{CO_2 \text{ in water}}}{H_{N_2O \text{ in water}}} * H_{N_2O-solution}$$



Known,
0.73



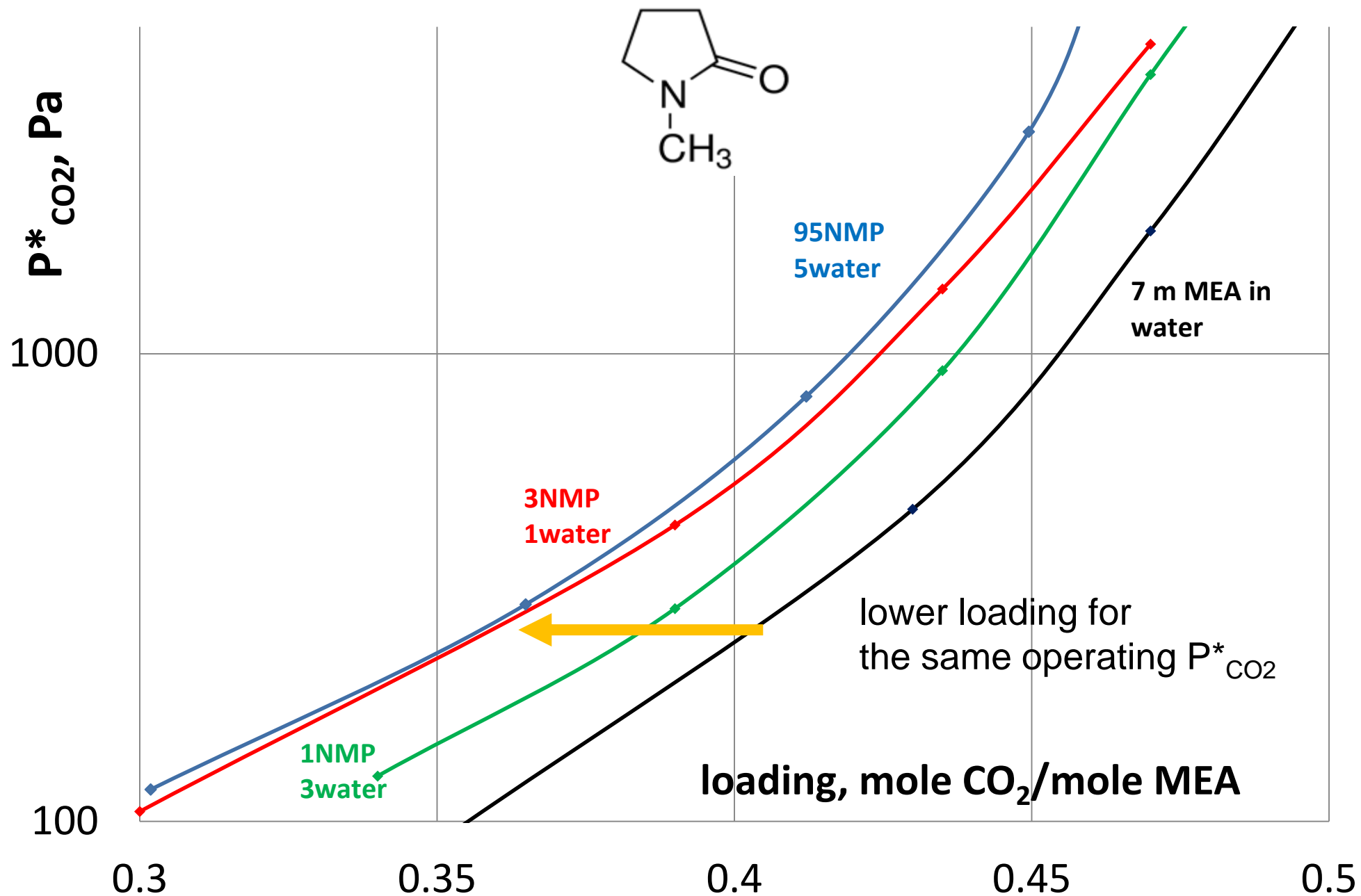
measured

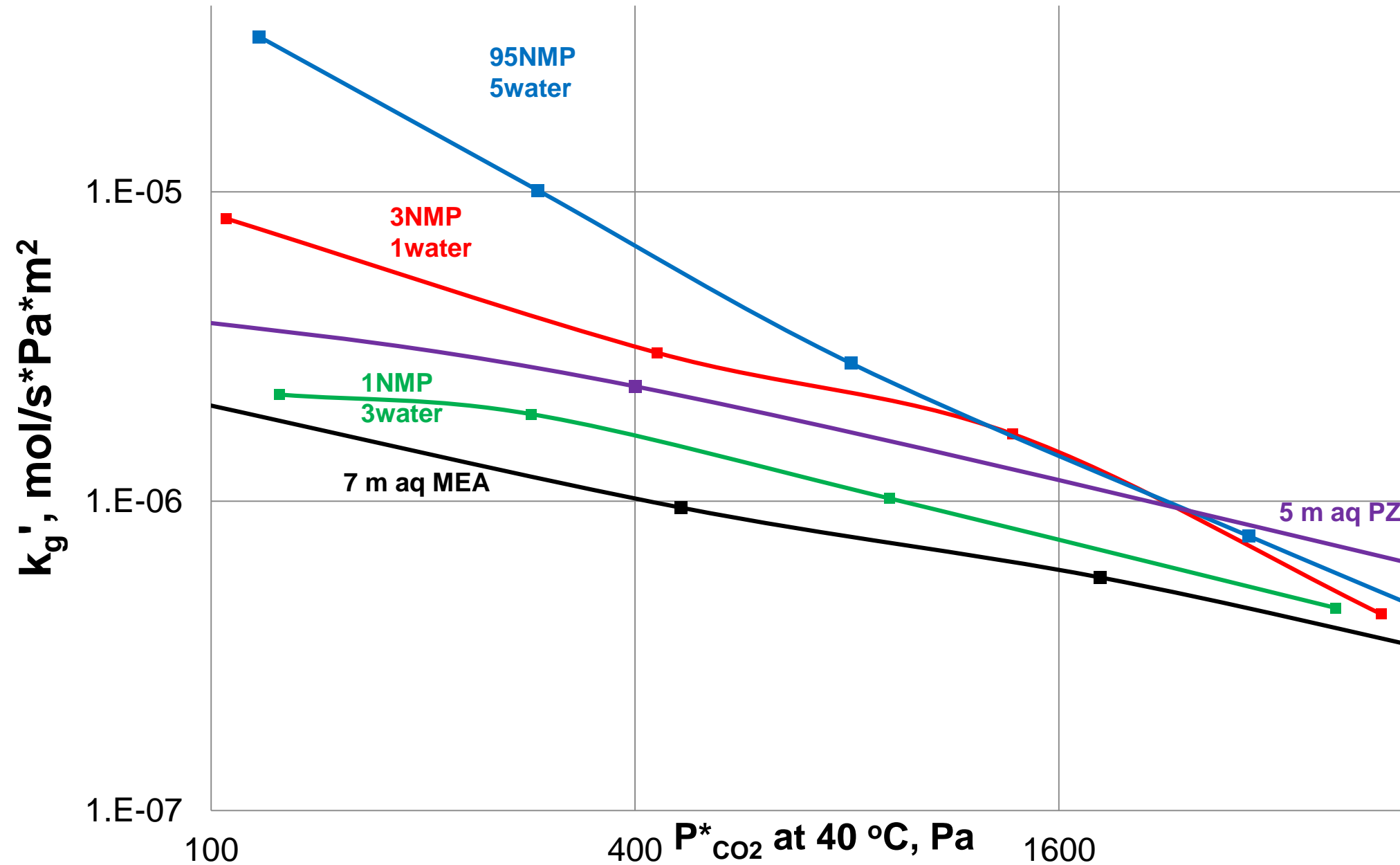
$$H_{CO_2-solution} = \gamma_{CO_2} H_{CO_2}$$

H_{CO_2} is the Henry's constant (std.)

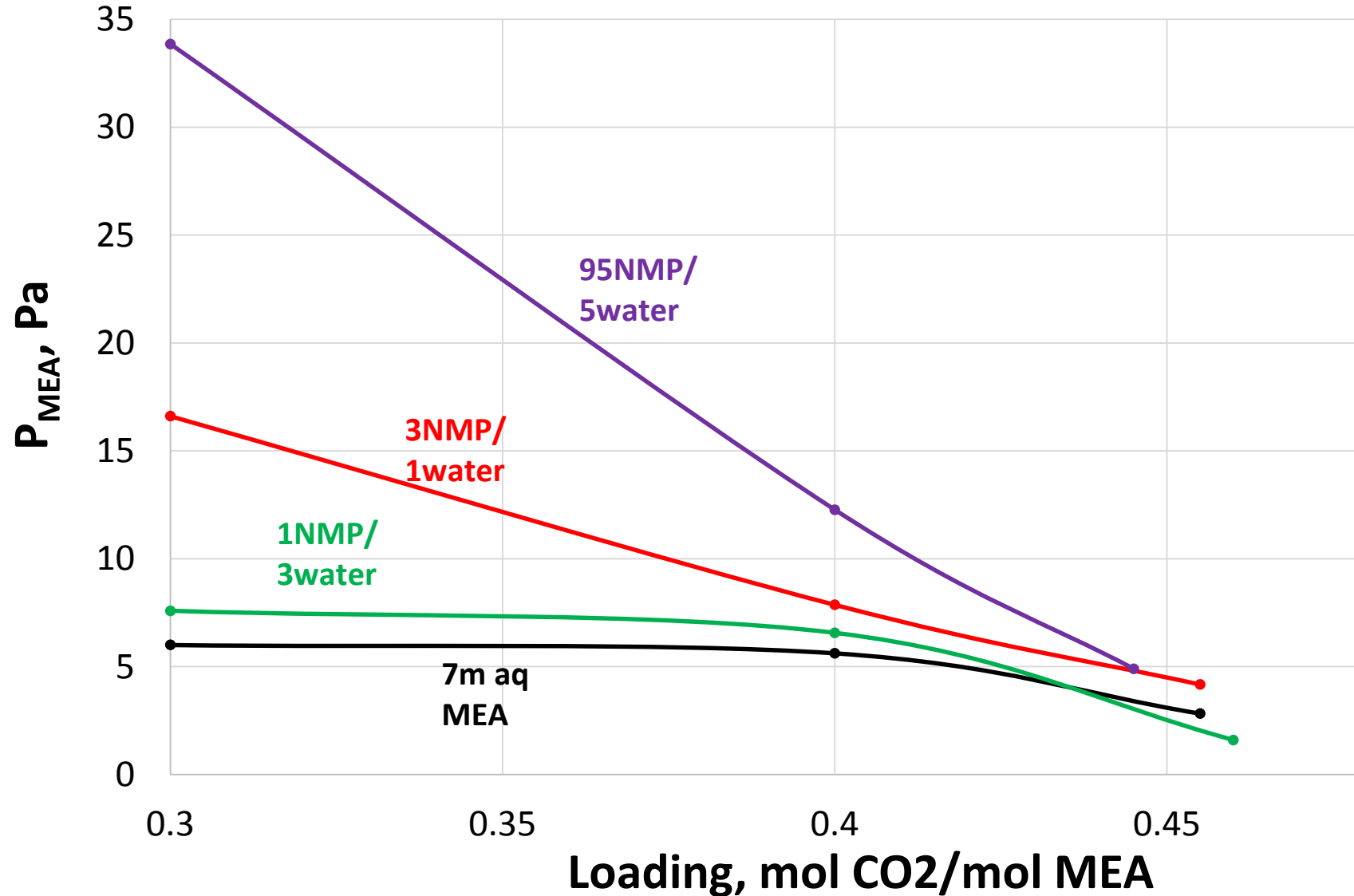
Activity of amine

- $P_{am} = H_{am}\gamma_{am}x_{am} = H_{am}a_{am}$
- $a_{am} = P_{am} / H_{am}$
- H_{am} is the Henry's constant (std.)
- γ_{am} is the activity coefficient
- a_{am} is the activity of the amine.
- $\frac{P_{am,2}}{P_{am,1}} = \frac{a_{am,2}}{a_{am,1}}$





P_{MEA} above different 7 m semi-aqueous MEA at 40 °C by FTIR



$$\frac{P_{am,2}}{P_{am,1}} = \frac{a_{am,2}}{a_{am,1}}$$

Numerical solution of penetration theory by MATLAB



$$\frac{dc_i}{dt} = -Di \frac{d^2c_i}{dx^2} + V_i * R$$

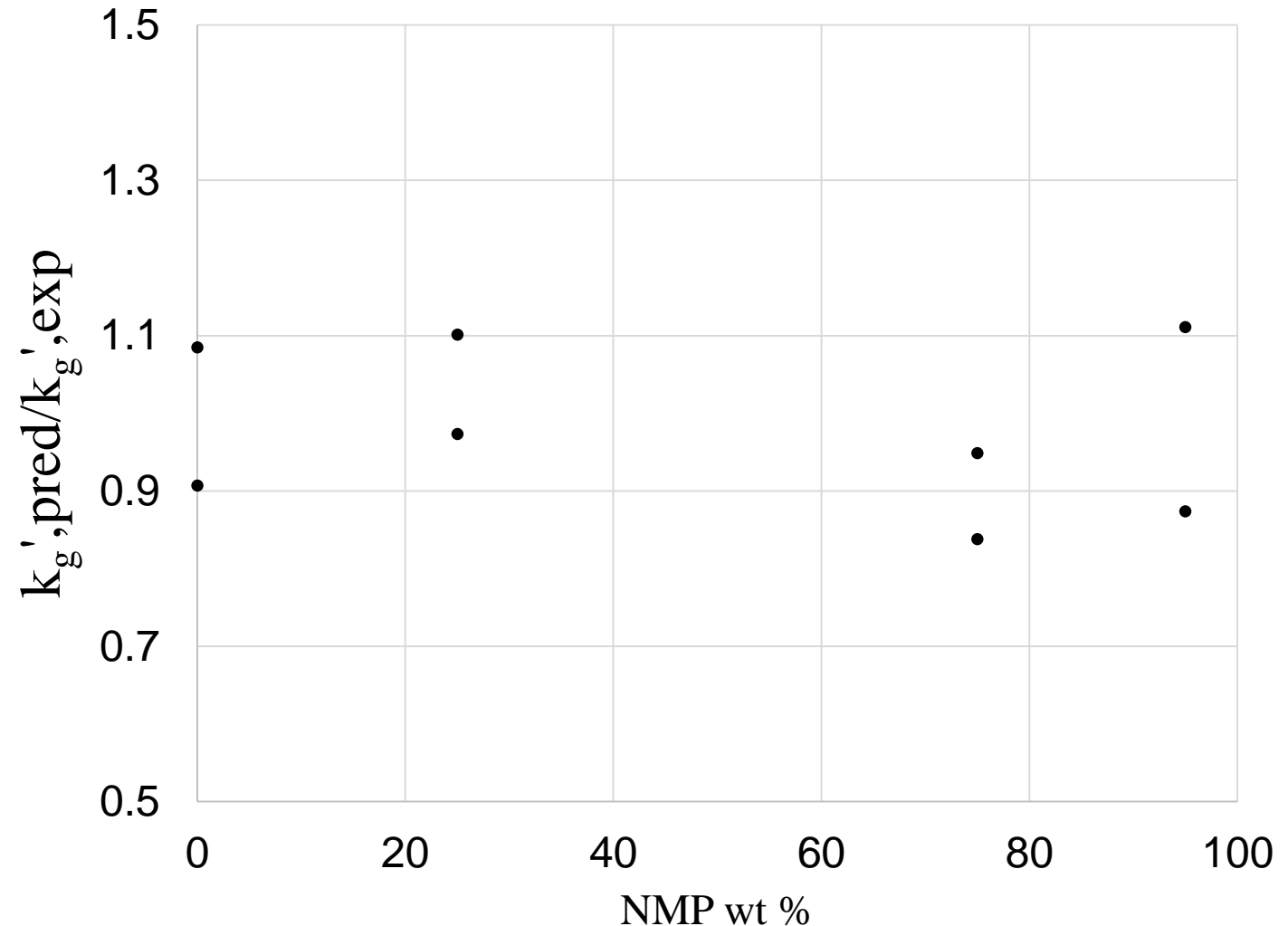
$$R = k_3 * a_{CO2} * a_{MEA}^2 - \frac{k_3}{K_{eq}} a_{MEACOO} * a_{MEAH}$$

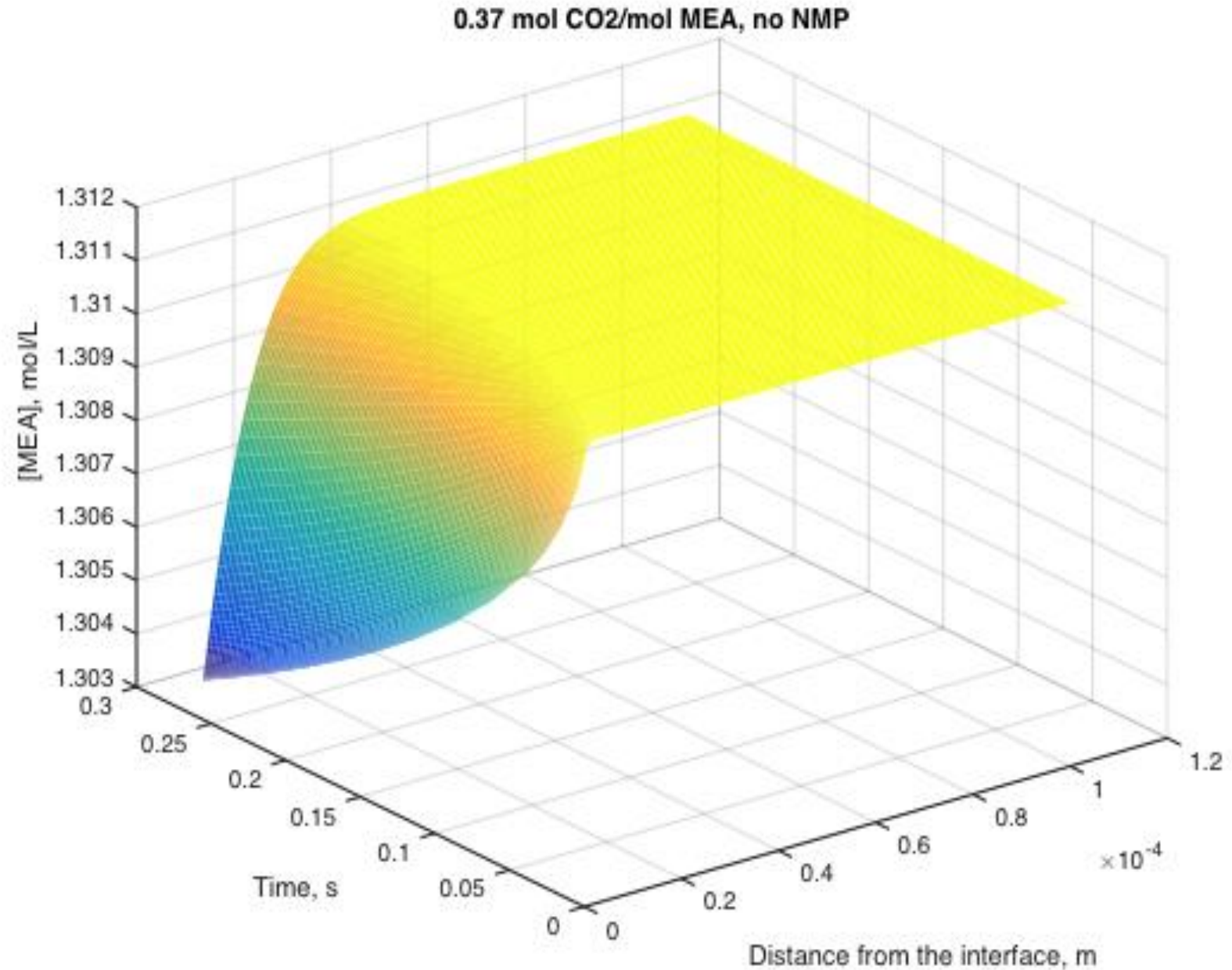
$$a_i = \gamma_i * C_i$$

regressed parameters

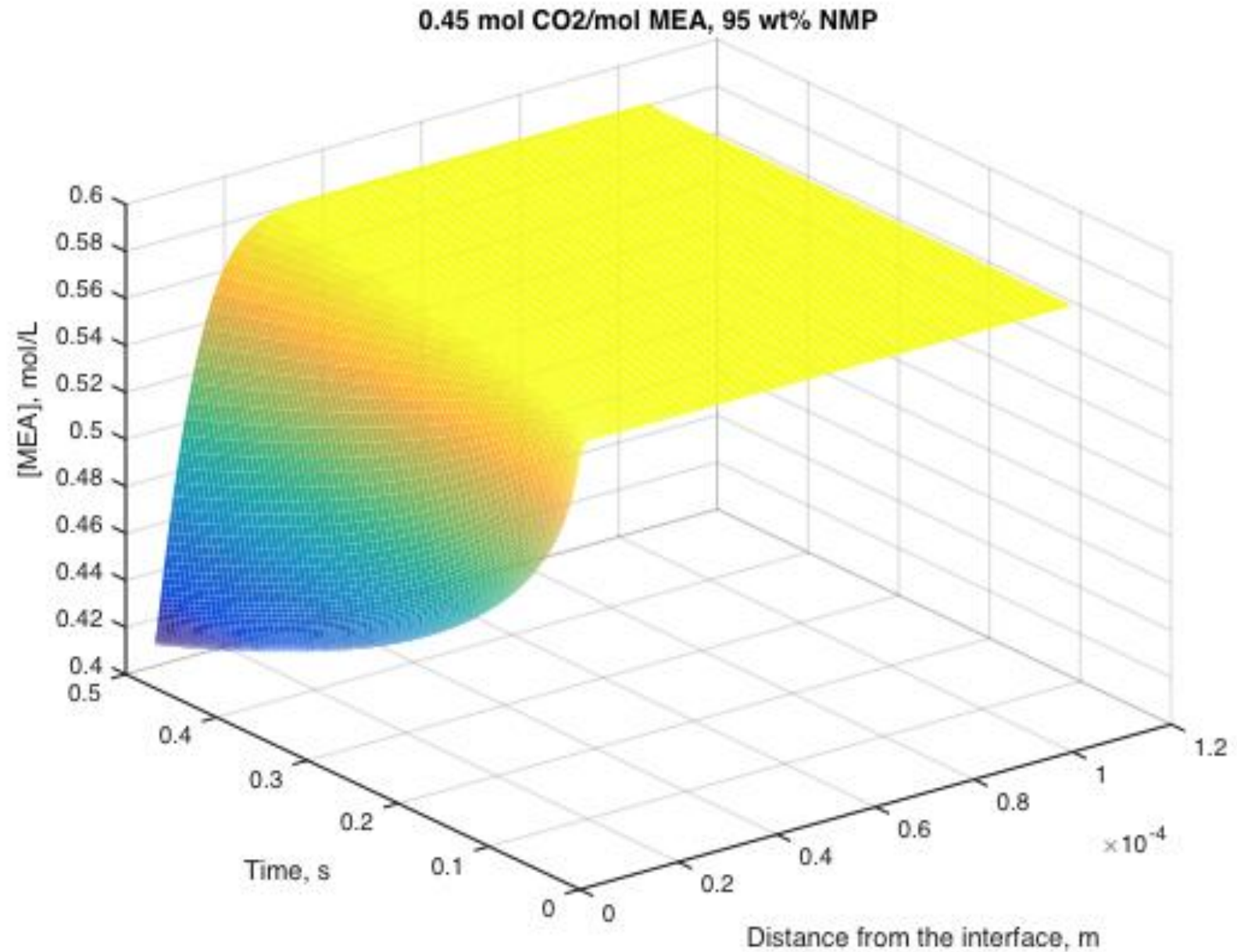
$$k_3 = 12711 \frac{m^6}{mol^2 * s}$$

$$D_{co2} = D_{co2,aq} \left(\frac{\mu}{\mu_{aq}} \right)^{-0.52}$$



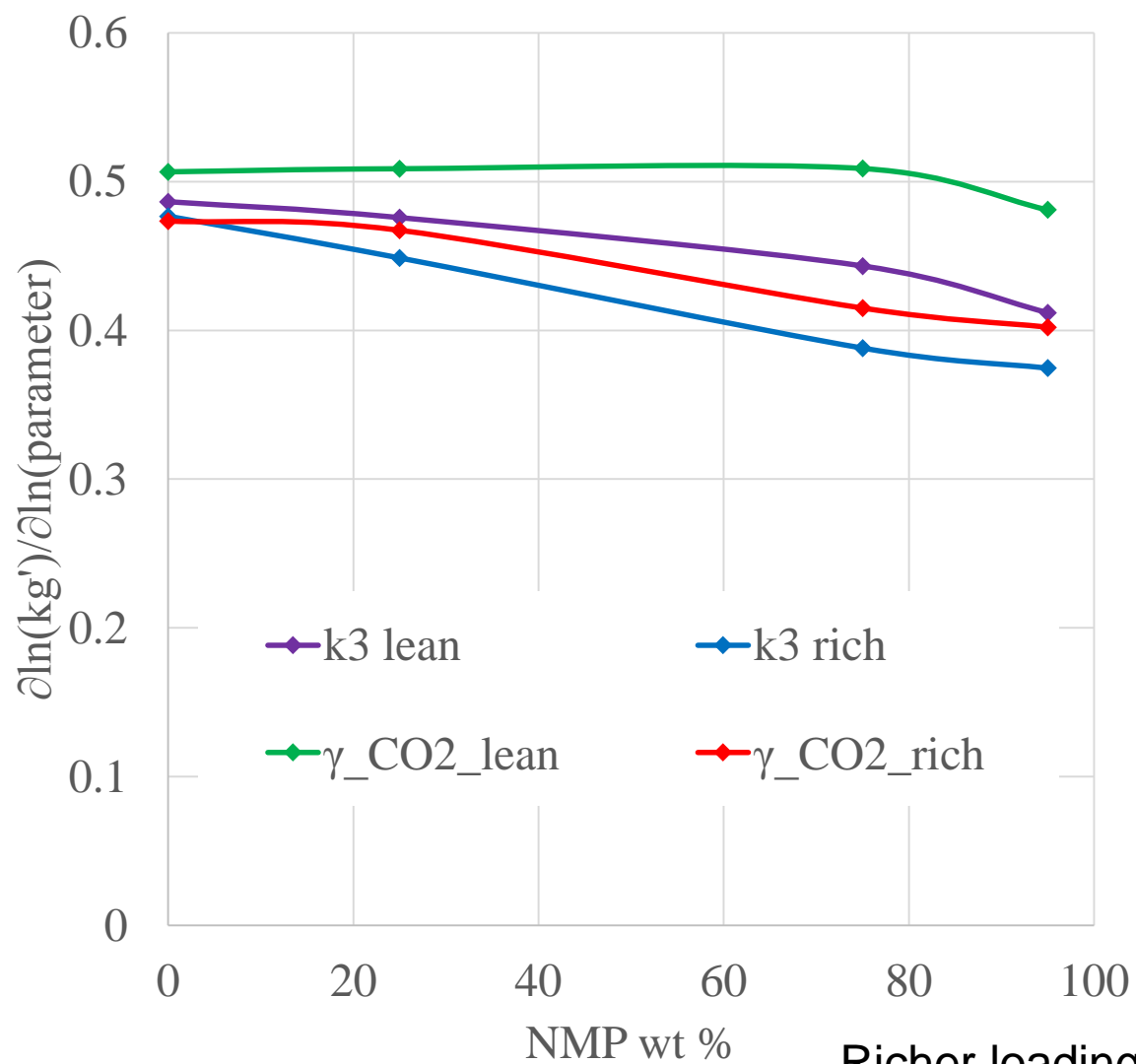


PFO approximation is adequate

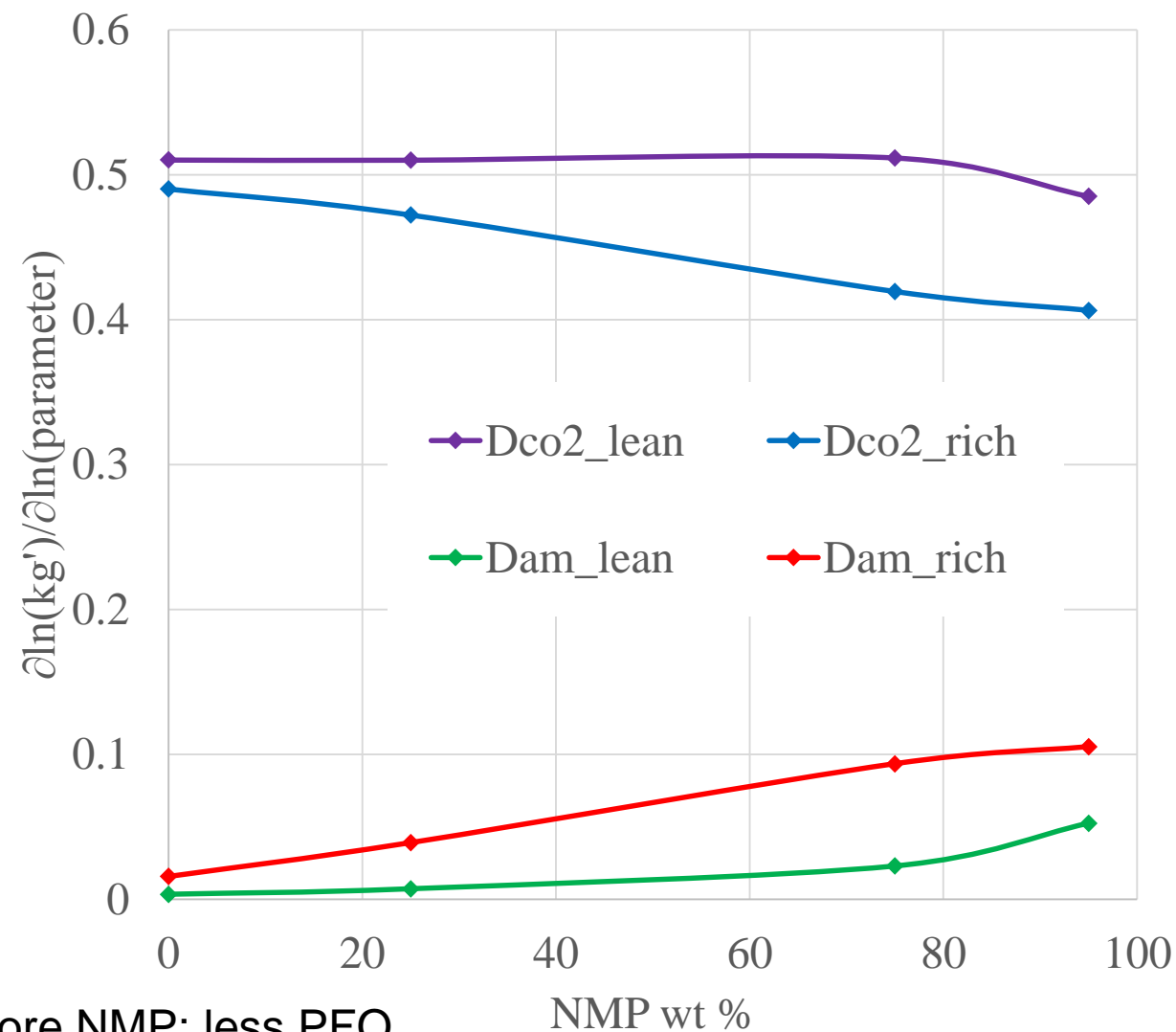


Rich loading, more NMP:
PFO is not accurate

Sensitivity analysis: $\frac{\partial \ln k'_g}{\partial \ln \text{parameter}}$, deviation from $k'_g = \frac{\sqrt{D_{CO2} k_3^* a_{am}}}{\gamma_{CO2}^{0.5} H_{CO2}}$



Richer loading, more NMP: less PFO



Explain the rate increase by PFO

Lean: 0.37 mol CO₂/mol MEA

$$k_g' = \frac{\sqrt{D_{CO_2} k_3^* a_{am}}}{\gamma_{CO_2}^{0.5} H_{CO_2}}$$

$$D_{CO_2} \propto \mu^{-0.52}$$

Solvent mass ratio		μ , 40 °C	γ_{CO_2}	γ_{MEA}	k_g' , exp	k_g' , predict
NMP	water					$a_{MEA} * \mu^{-0.26} * \gamma_{CO_2}^{-0.5}$
0	1	1	1	1	1	1.0
1	3	1.84	0.95	1.60	1.2	1.4
3	1	6.08	0.58	2.67	2.1	2.2
95	5	5.76	0.28	4.44	5.2	5.3

Rich loading: not PFO, must use the MATLAB model

Conclusion

- At lean loading ($P^*_{\text{CO}_2}$ at 40 °C = 100 Pa) , k_g' of 7 m MEA in 3 water/1 NMP, 1 water/3 NMP, and 5 water/95 NMP is 1.25 times, 4 times, and 17 times that of 7 m MEA(aq), respectively.
- Adding NMP increases k_g' : lower loading, higher physical solubility, higher MEA activity.
- A MATLAB mass transfer model was built for semi-aqueous MEA.
- PFO approximation is adequate to represent the CO_2 mass transfer in aqueous MEA but not accurate for semi-aqueous MEA.



Thanks

Comments & Questions?



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