

From MEA 30 wt.% to demixing solvents: investigation of an aqueous-alcoholic MEA-based solution

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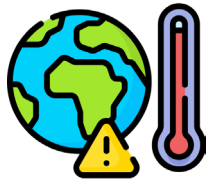
*8th Post-Combustion Capture Conference
Marseille – France*

16th September 2025 – Session 3A

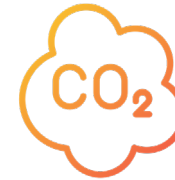


PCCC-8

Carbon capture context

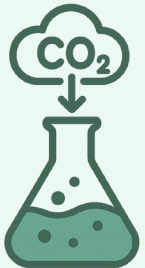


+ 1.55°C in 2024
since pre-industrial level era



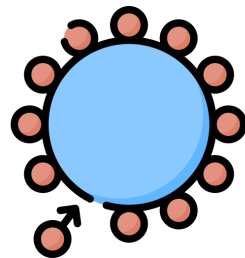
425.48 ppm in August 2025
CO₂ atmospheric concentration

Carbon capture technologies

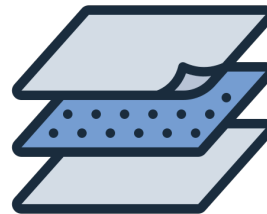


Absorption

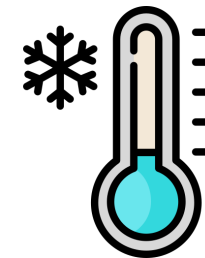
TRL 9



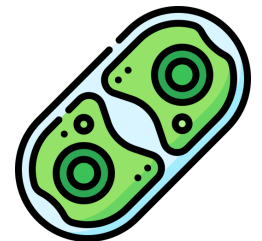
Adsorption



Membrane



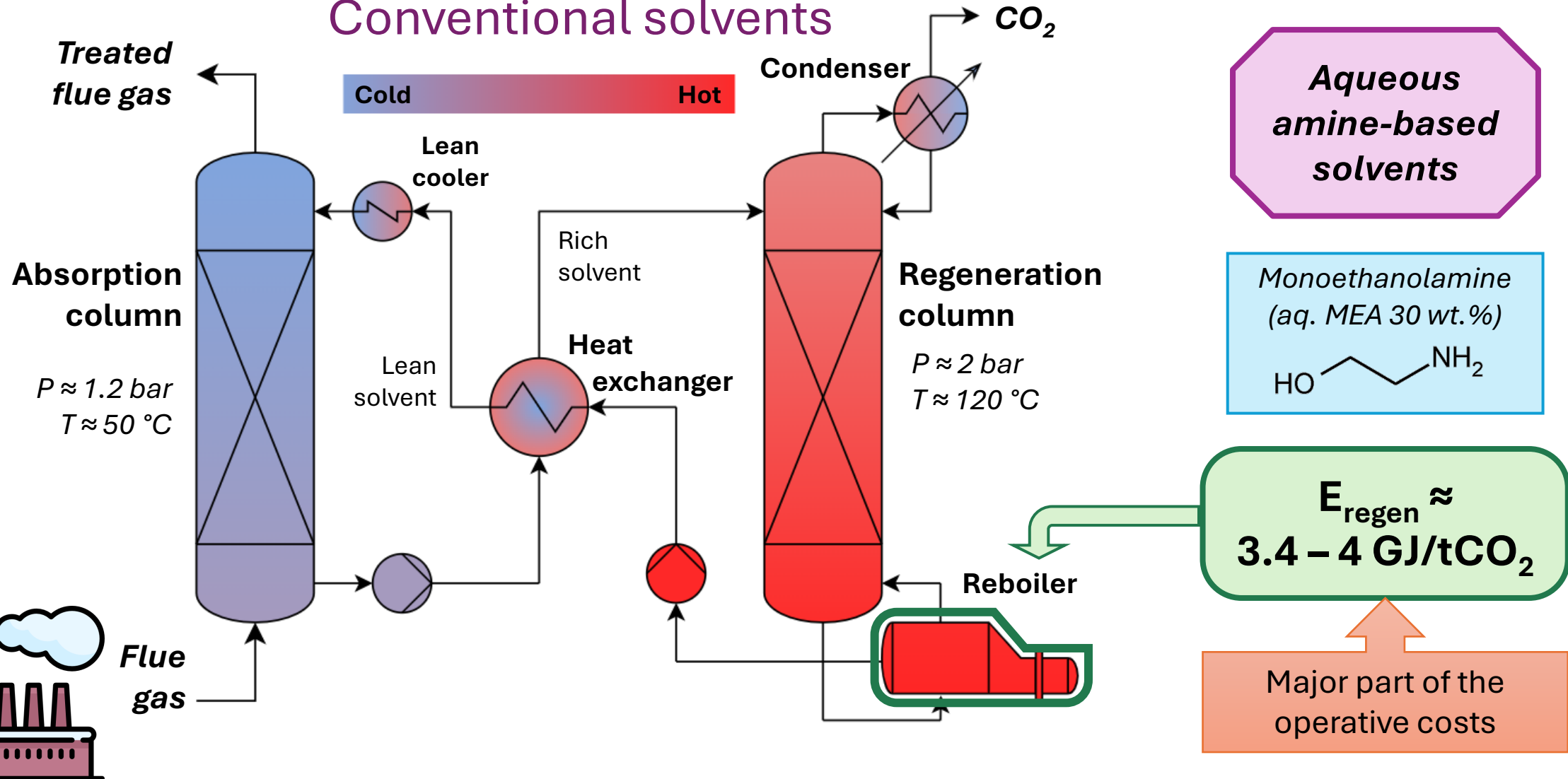
Cryogenics



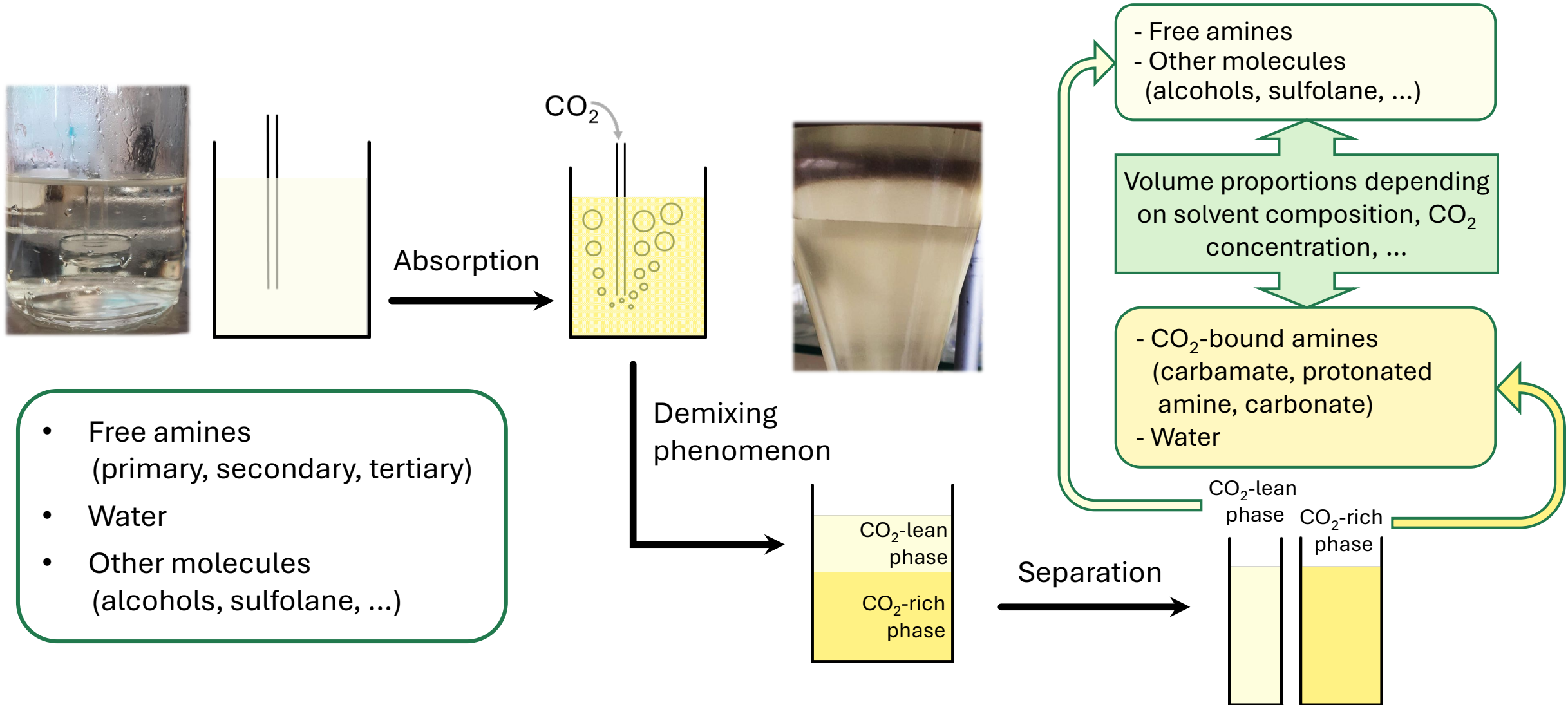
Microalgae

Carbon capture Absorption-Regeneration process

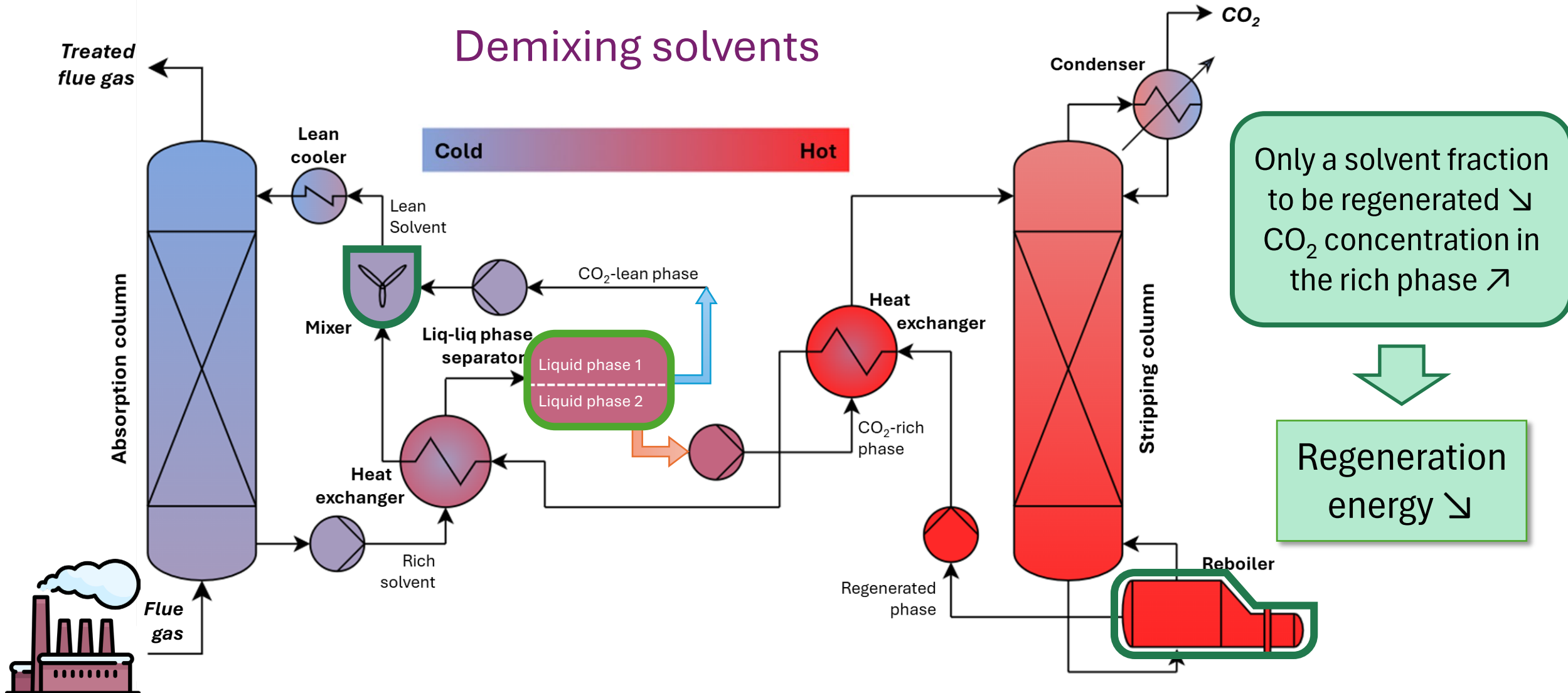
Conventional solvents



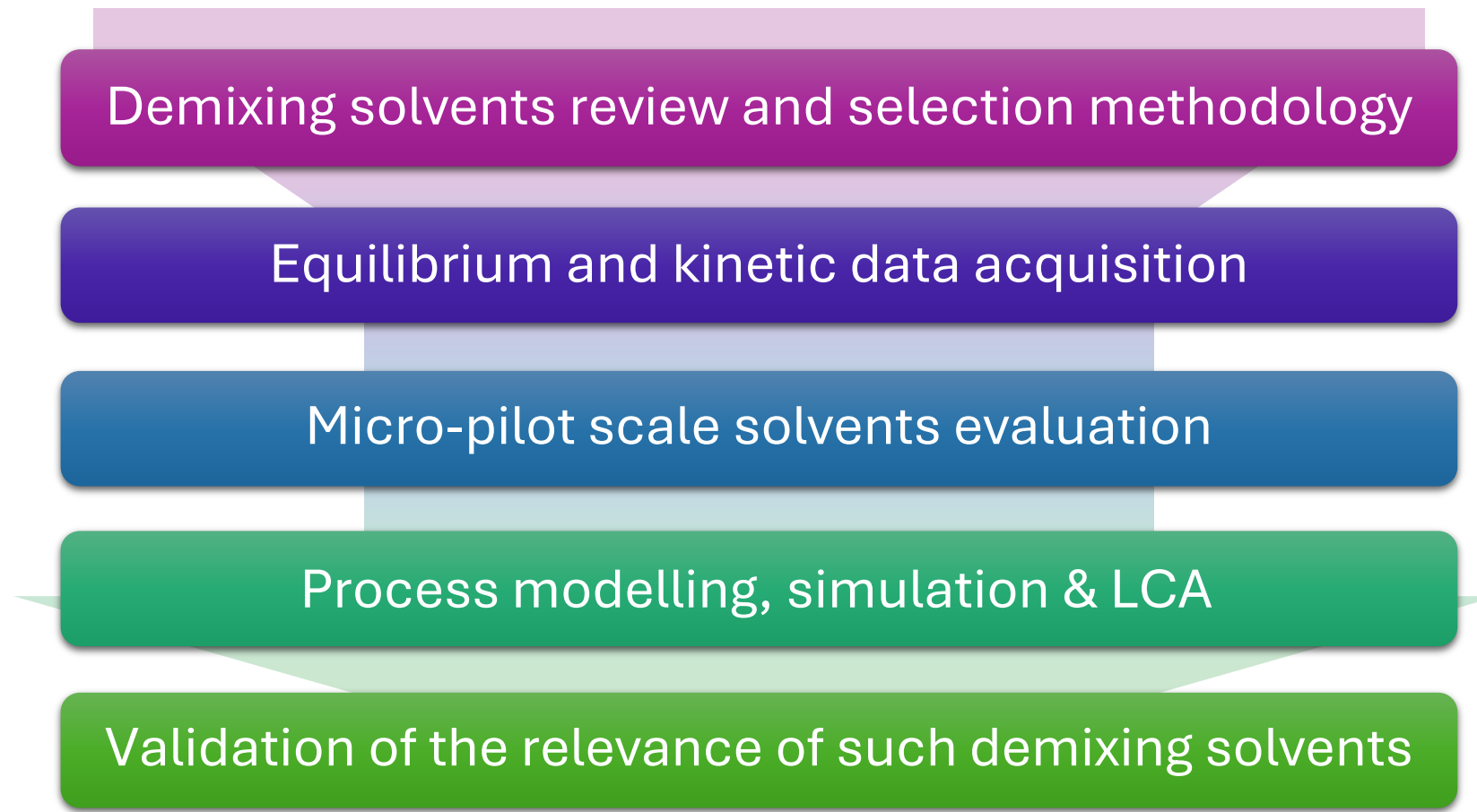
Demixing liquid-liquid amine-based solvents



Carbon capture Absorption-Regeneration process

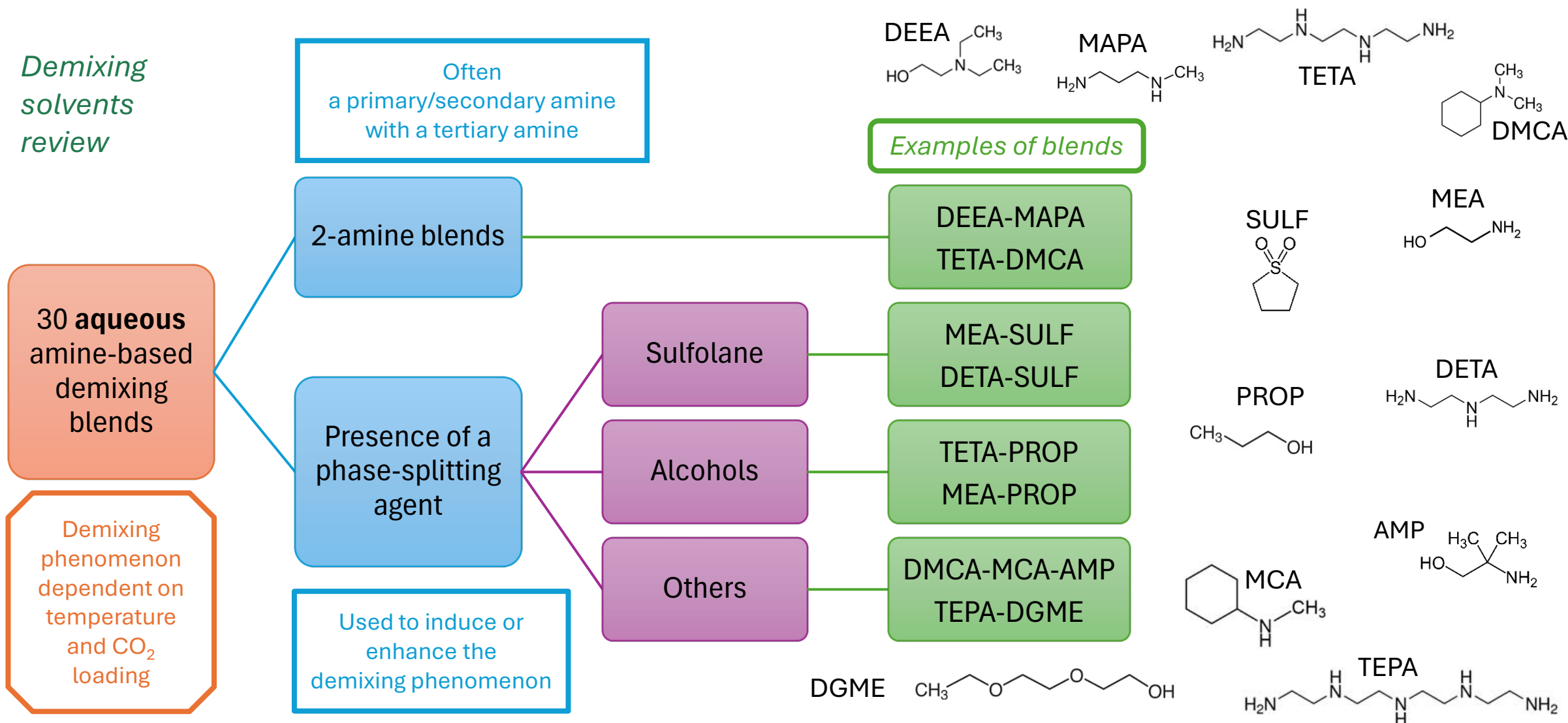


Demixing liquid-liquid amine-based solvents



Demixing liquid-liquid amine-based solvents

Demixing
solvents
review



Selection methodology of demixing solvents

Step 1 – Techno-economic evaluation

Based on 6 key indicators ...	Regeneration energy	... having each a specific weight	0.42
	CO ₂ absorption rate		0.17
	Demixing volume ratio*		0.15
	CO ₂ absorption capacity		0.12
	Volatility of organic compounds**		0.08
	Solvent cost		0.06

Scale from 1 (best case) to 5 (worst case) for each indicator

Estimated values if missing in literature

$$* = V_{\text{rich}} / V_{\text{lean}}$$

$$** = y_{\text{organic}} / x_{\text{organic}}$$

For each solvent

$$\text{Global score} = \sum_{i=1}^6 p_i * s_i$$

p_i : weight of indicator i
 s_i : score of indicator i
 $\{1,2,3,4,5\}$

Step 2 – Health, safety and environment analysis

A solvent is **excluded** from the final ranking if at least one of its components causes:

Death

Serious fertility problem

Corrosion to metals

Very toxic to aquatic life

Rejection of
17 solvents

Database: European Chemistry Agency
(CLP regulation and REACH legislation)

Selection methodology of demixing solvents

Final classification

1	TETA (30 wt.%) – PROP (50 wt.%)
2	TETA (15 wt.%) – DMCA (35 wt.%)
3	DEEA (64 wt.%) – MAPA (19 wt.%)
4	DEEA (50 wt.%) – MEA (25 wt.%)
5	DEEA (62 wt.%) – MAPA (9 wt.%)
6	DMBA (47 wt.%) – DEEA (27 wt.%)
7	TETA (31 wt.%) – 1DMA2P (22 wt.%)
8	DEEA (47 wt.%) – TETA (15 wt.%)
9	DEEA (47 wt.%) – TETA (15 wt.%) – PROP (17 wt.%)
10	MEA (30 wt.%) – PROP (40 wt.%)
11	AEP (20 wt.%) – PROP (40 wt.%)
12	MEA (30 wt.%) – BUT (40 wt.%)
13	MAE (30 wt.%) – BUT (40 wt.%)

Methodological Selection of Demixing Liquid–Liquid Solvents Used in the Absorption–Regeneration Carbon Capture Process

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Damien Verdonck, Lionel Dubois, Guy De Weireld, and Diane Thomas*



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17th International Conference on Greenhouse Gas Control Technologies, GHGT-17

20th -24th October 2024 Calgary, Canada

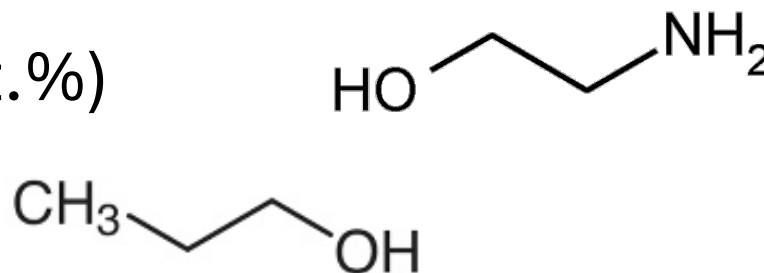
Methodological evaluation of demixing solvents
used in the absorption-regeneration carbon capture process

Damien Verdonck, Lionel Dubois, Guy De Weireld, Diane Thomas*

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An aqueous-alcoholic MEA-based solution

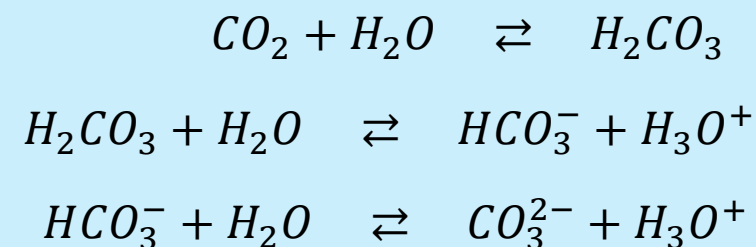
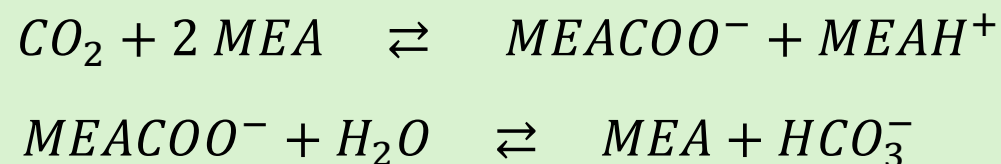
- Monoethanolamine (30 wt.%)
- Propan-1-ol (40 wt.%)
- Water (30 wt.%)



Open
access
solvent

Chemical reactions

- Same as for aqueous MEA 30 wt.%
- No reaction products with propanol



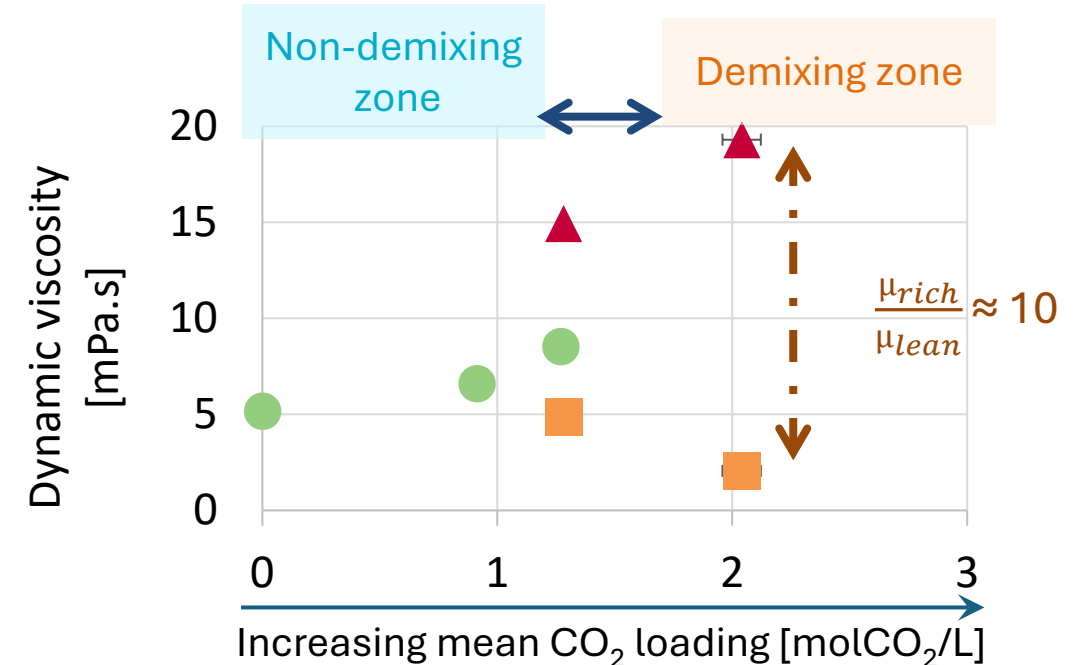
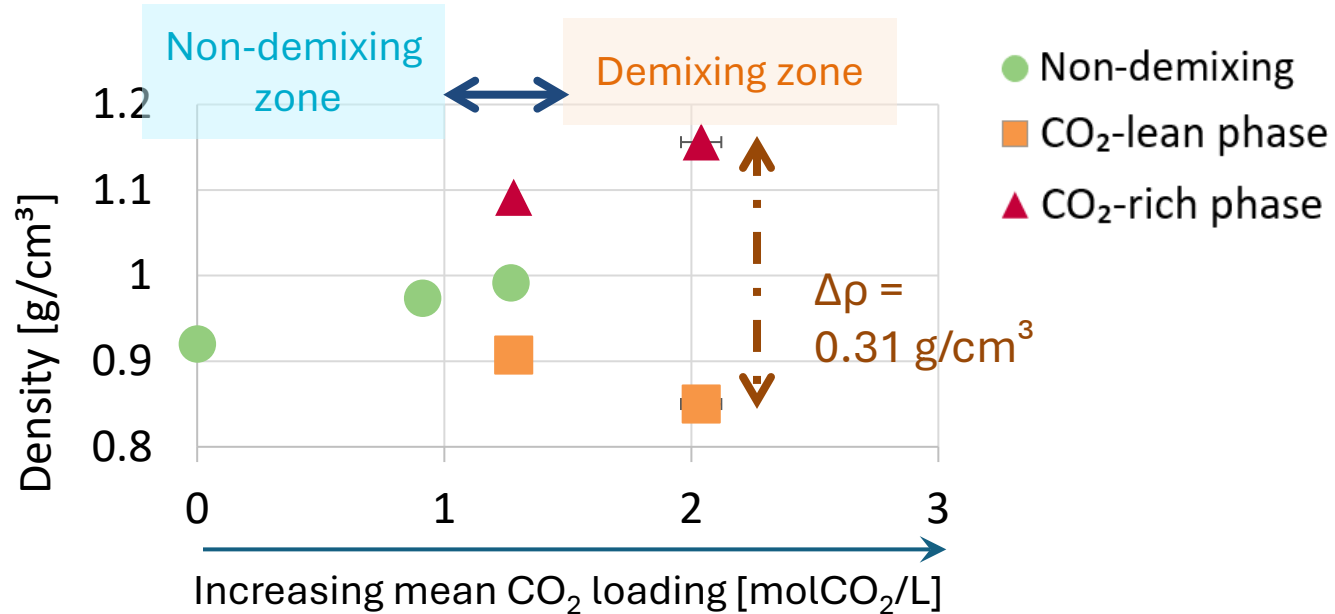
An aqueous-alcoholic MEA-based solution

MEA (30 wt.%) – PROP (40 wt.%)

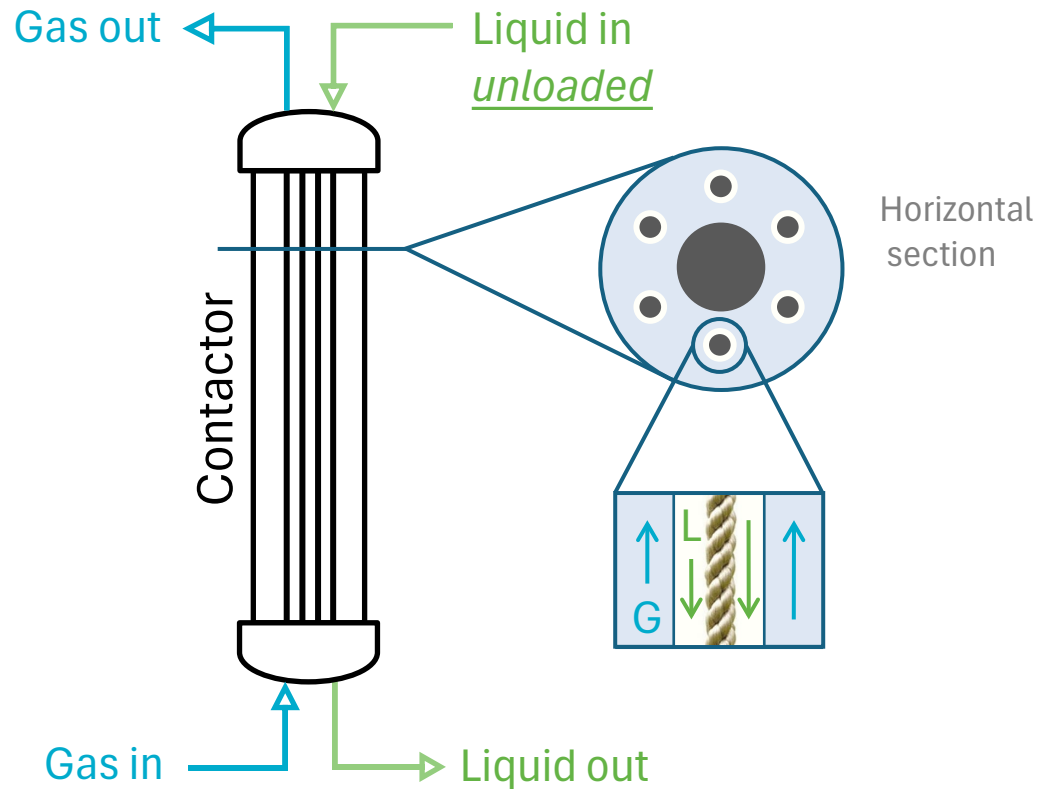
Critical CO₂ concentration at 25 °C
1.28 molCO₂/L



Volume of the CO₂-rich phase from 44 to 60%
(from 2.15 up to 3.22 molCO₂/L)



Absorption performance on cable-bundle contactor

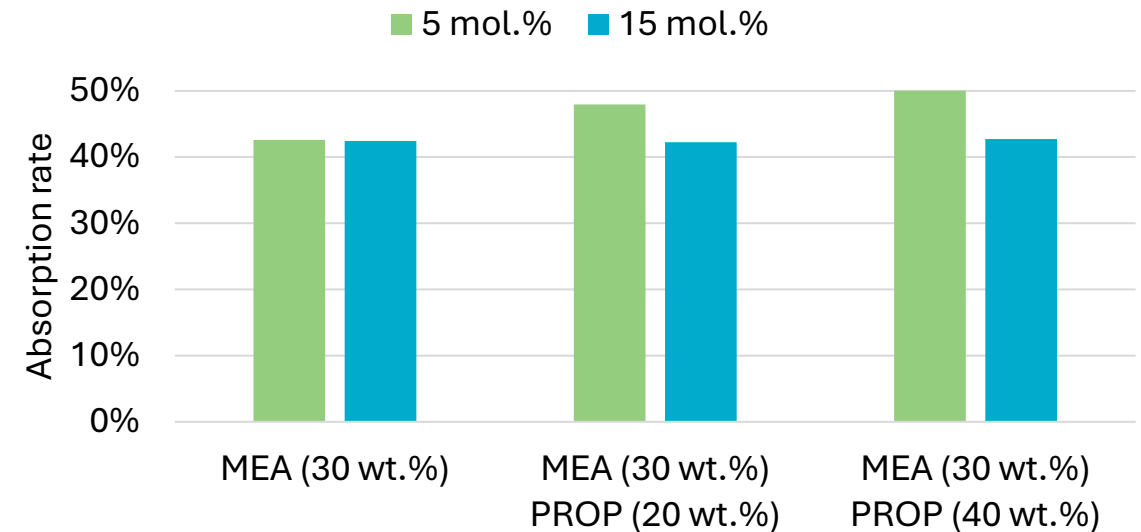


Height	54 cm
Number of cables	6
Diameter of a cable	1.6 mm

$$A = \frac{G_{CO_2,in} - G_{CO_2,out}}{G_{CO_2,in}} = 1 - \frac{y_{CO_2,out}}{y_{CO_2,in}} * \frac{1 - y_{CO_2,in}}{1 - y_{CO_2,out}}$$

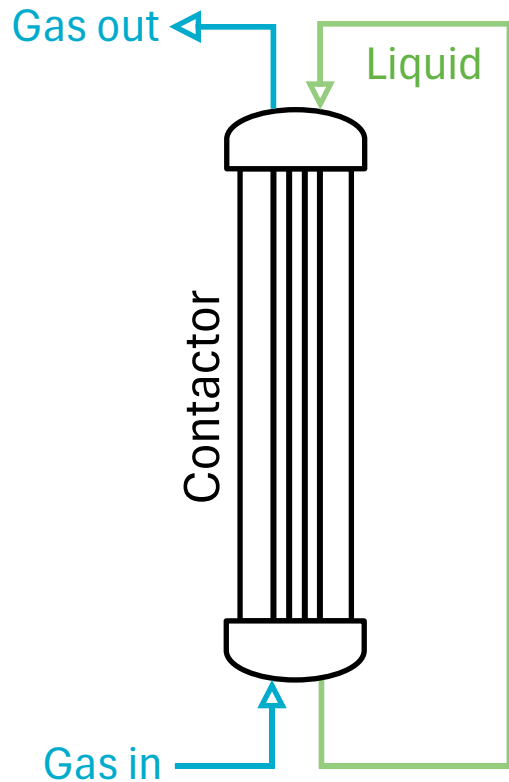
Continuous tests

a single pass of liquid



Liquid flow rate	Gas flowrate	CO ₂ gas fraction
11.4 L/h	762 NL/h	5 - 15 mol.%

Absorption performance on cable-bundle contactor



*Recirculation
of liquid until
CO₂ saturation
is achieved*

Height	54 cm
Number of cables	6
Diameter of a cable	1.6 mm

$$A = \frac{G_{CO_2,in} - G_{CO_2,out}}{G_{CO_2,in}} = 1 - \frac{y_{CO_2,out}}{y_{CO_2,in}} * \frac{1 - y_{CO_2,in}}{1 - y_{CO_2,out}}$$

Semi-continuous tests

For aqueous blend
MEA (30 wt.) – PROPAN-1-OL (40 wt.)

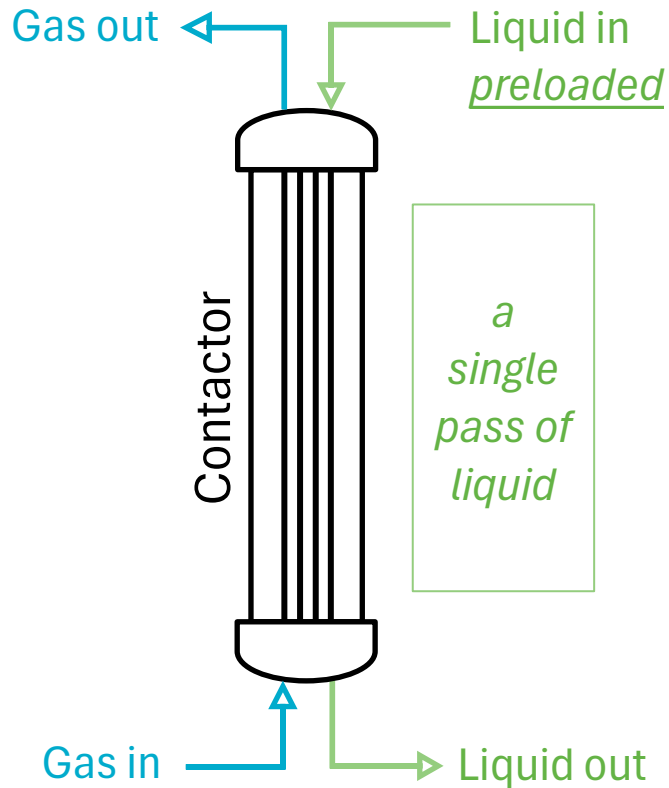
Volume loss of
the liquid solvent



Volatility of
propan-1-ol



Absorption performance on cable-bundle contactor

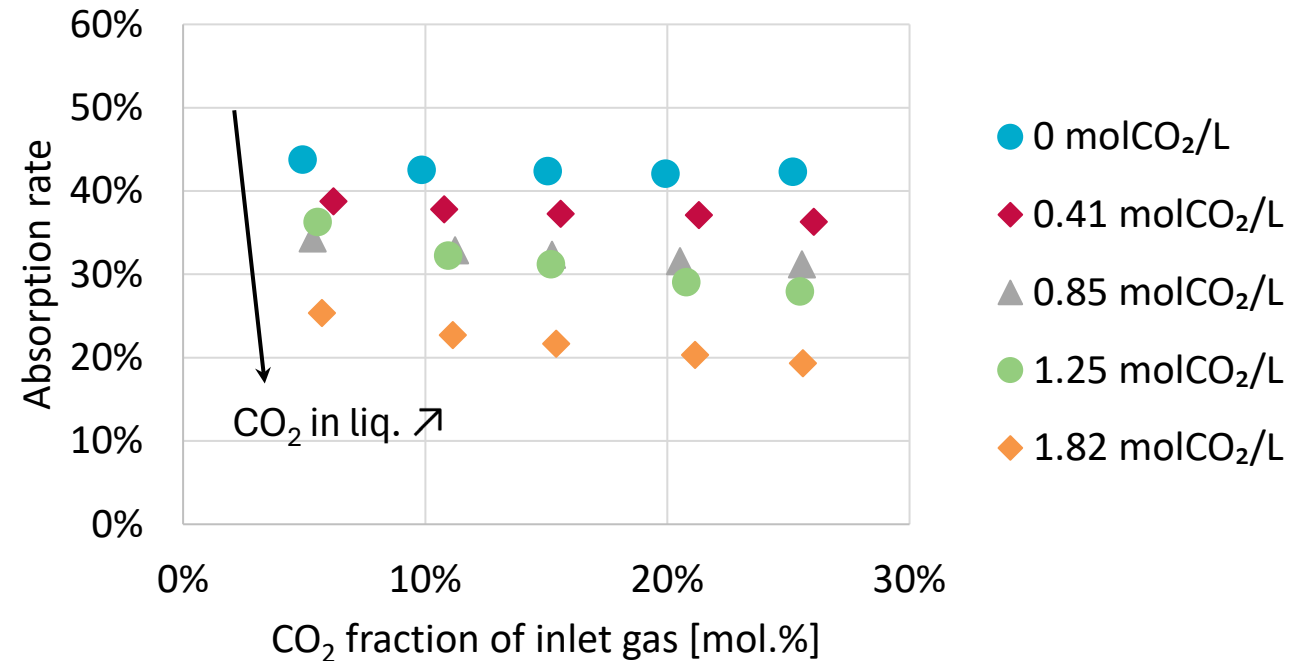


Height	54 cm
Number of cables	6
Diameter of a cable	1.6 mm

Continuous tests

$$A = \frac{G_{CO_2,in} - G_{CO_2,out}}{G_{CO_2,in}} = 1 - \frac{y_{CO_2,out}}{y_{CO_2,in}} * \frac{1 - y_{CO_2,in}}{1 - y_{CO_2,out}}$$

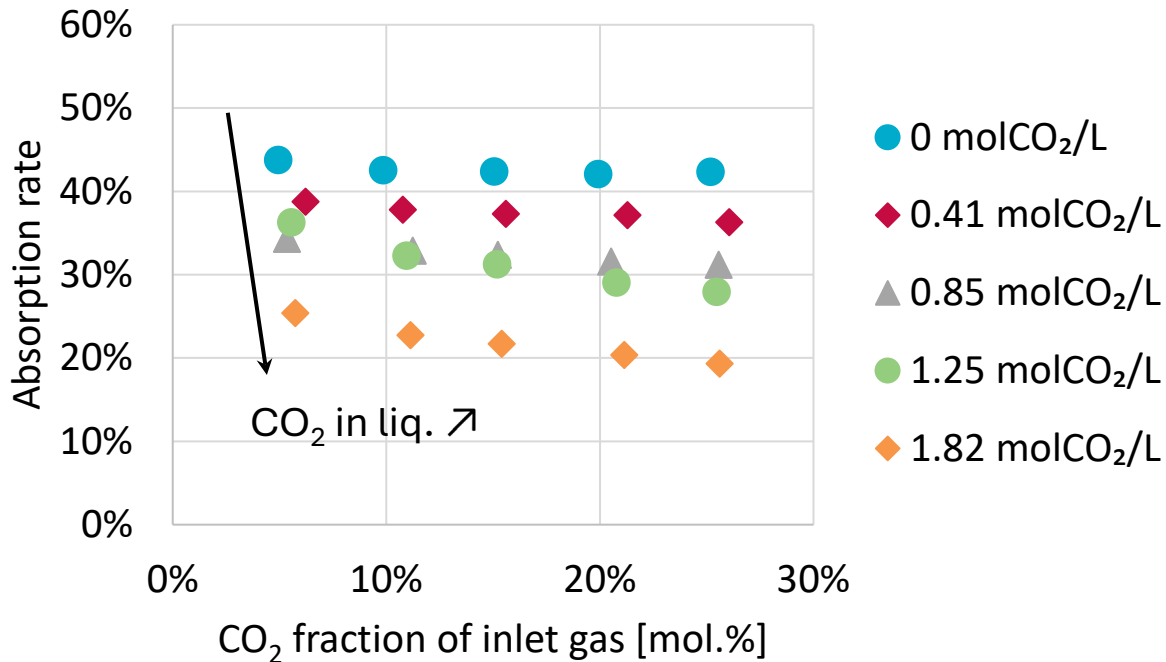
MEA 30 wt. %



Absorption performance on cable-bundle contactor

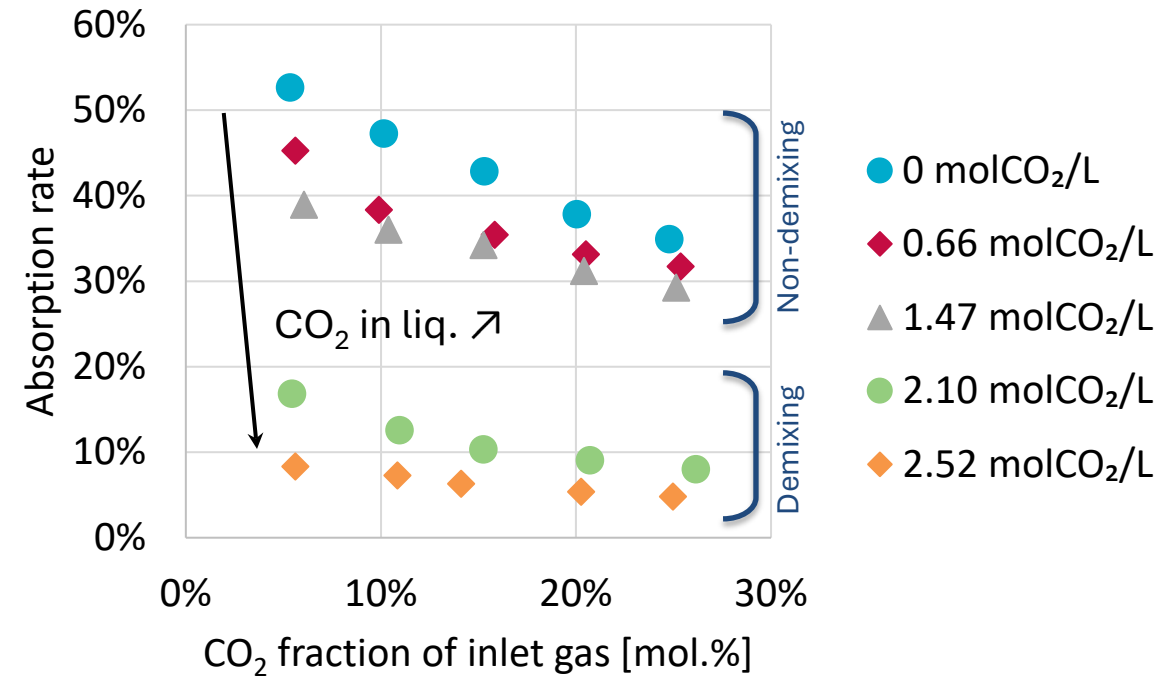
Continuous tests

MEA 30 wt. %



$$A = \frac{G_{CO_2,in} - G_{CO_2,out}}{G_{CO_2,in}} = 1 - \frac{y_{CO_2,out}}{y_{CO_2,in}} * \frac{1 - y_{CO_2,in}}{1 - y_{CO_2,out}}$$

MEA 30 wt. % - PROP 40 wt. %



Liquid-liquid equilibrium modelling

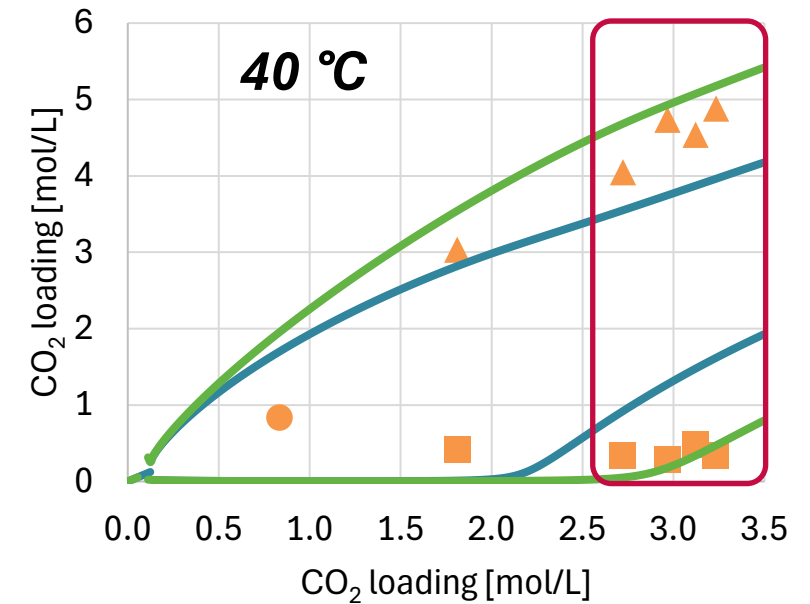
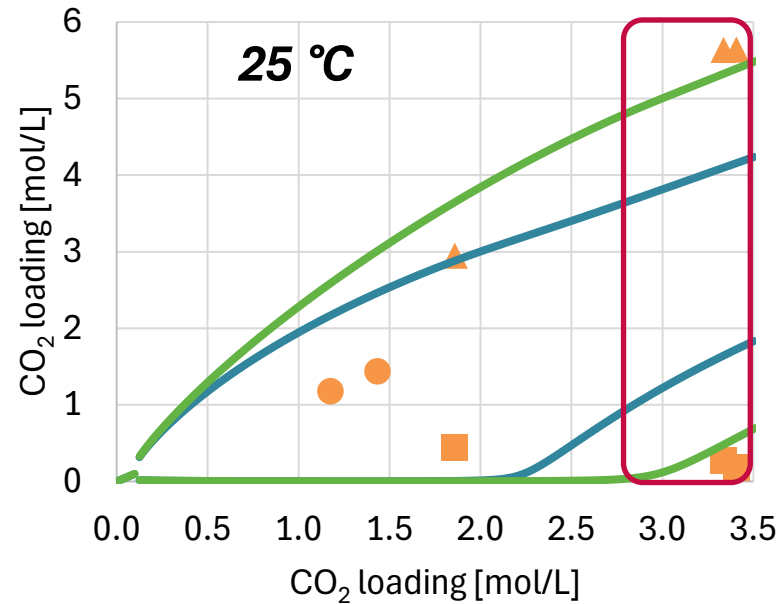
MEA (30 wt.%) – PROP (40 wt.%)

Modelling using
two different
thermodynamic models
for liquid phases:

— Electrolyte Non-Random
Two-Liquid (eNRTL) Wang et al., 2019

— Electrolyte Non-Random
Two-Liquid with the
Helgeson model (eNRTL-HG)

Tanger et al., 1988



Relative deviations between experiments and modelling

		25 °C	40 °C
CO ₂ -rich phase	eNRTL	27%	17%
	eNRTL-HG	5%	9%

Experiment :
● Non-demixing
▲ CO₂-rich phase
■ CO₂-lean phase

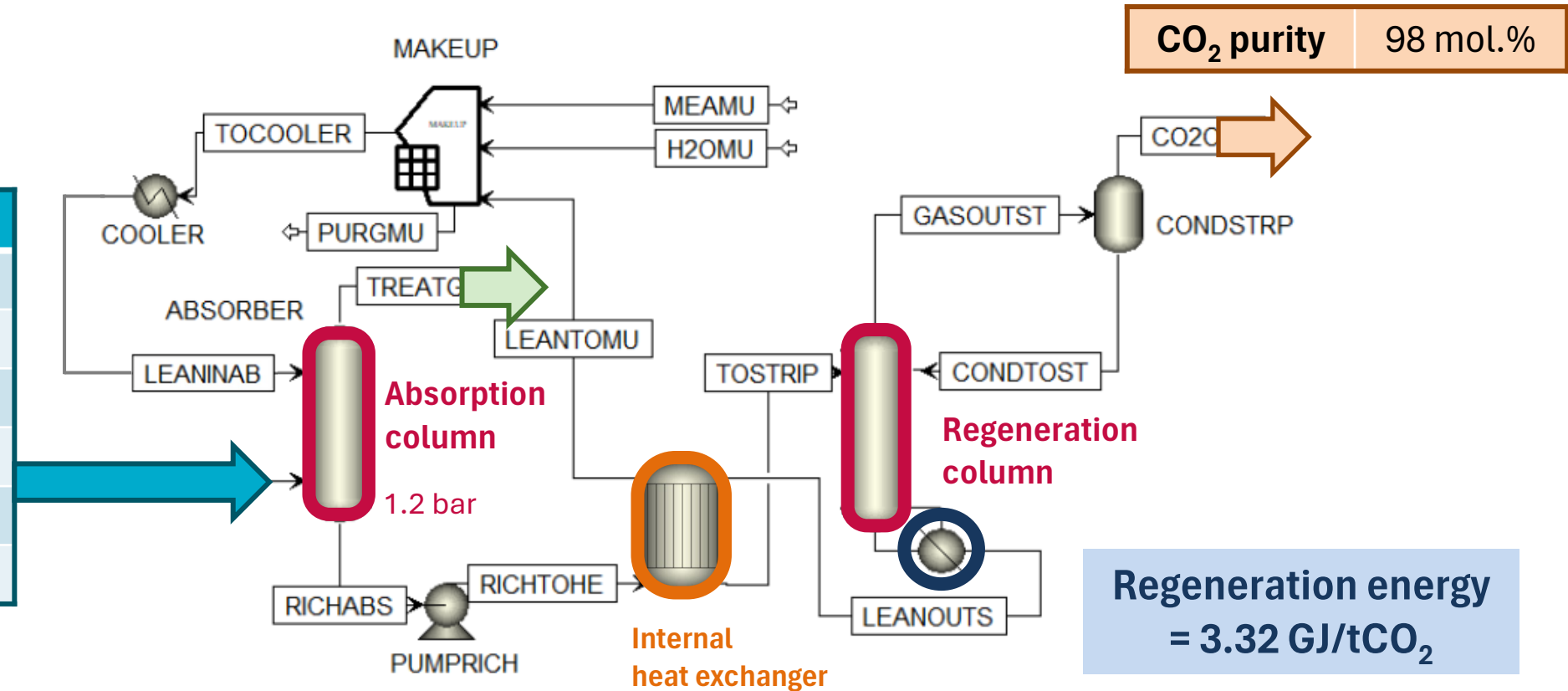
Absorption-Regeneration process modelling

MEA (30 wt.%)

Absorption rate 90%

CO₂ purity 98 mol.%

Flue gas from lime plant		
Flow	32 000 m ³ /h	
Temperature	50 °C	
Molar fractions	CO ₂	24%
	N ₂	63%
	O ₂	8%
	H ₂ O	5%



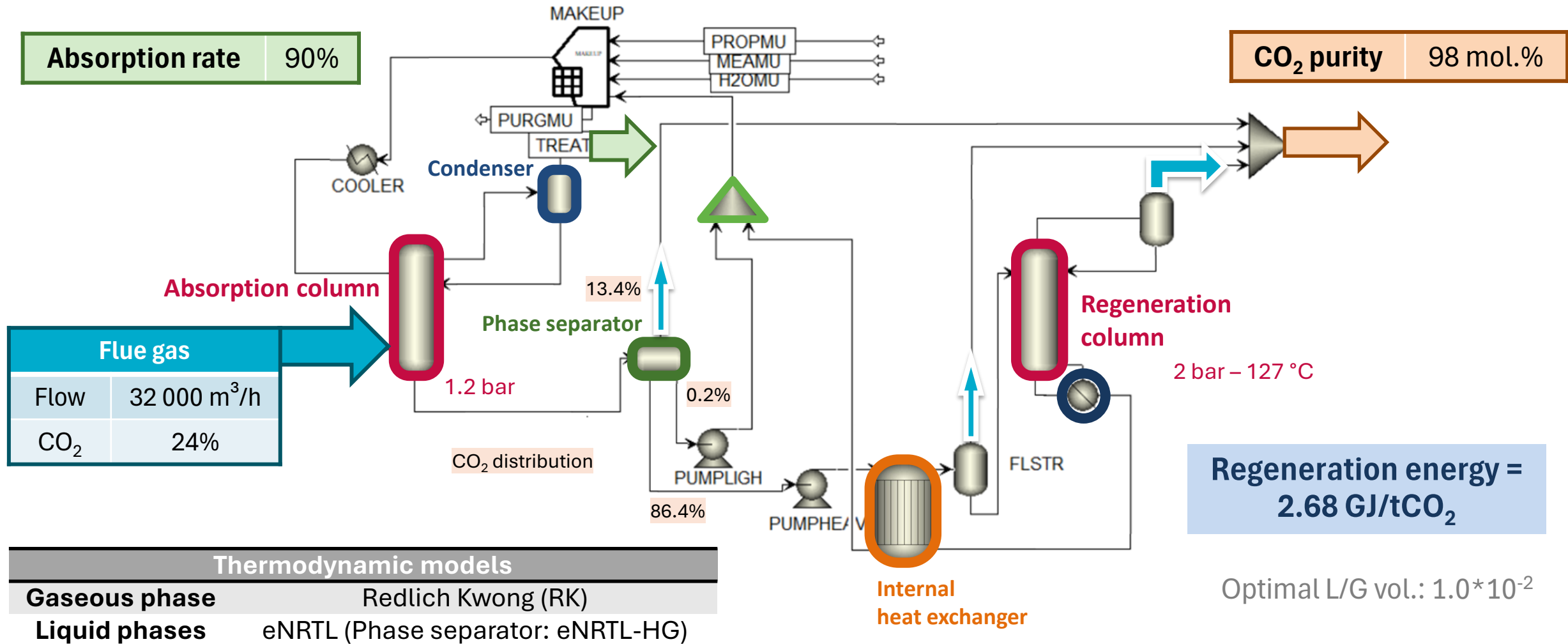
Thermodynamic models

Gaseous phase	Redlich Kwong (RK)
Liquid phase	Electrolyte Non-Random Two Liquid (eNRTL)

Optimal L/G vol.: 6.8×10^{-3}

Absorption-Regeneration process modelling

MEA (30 wt.%) – PROP (40 wt.%)



Conclusion

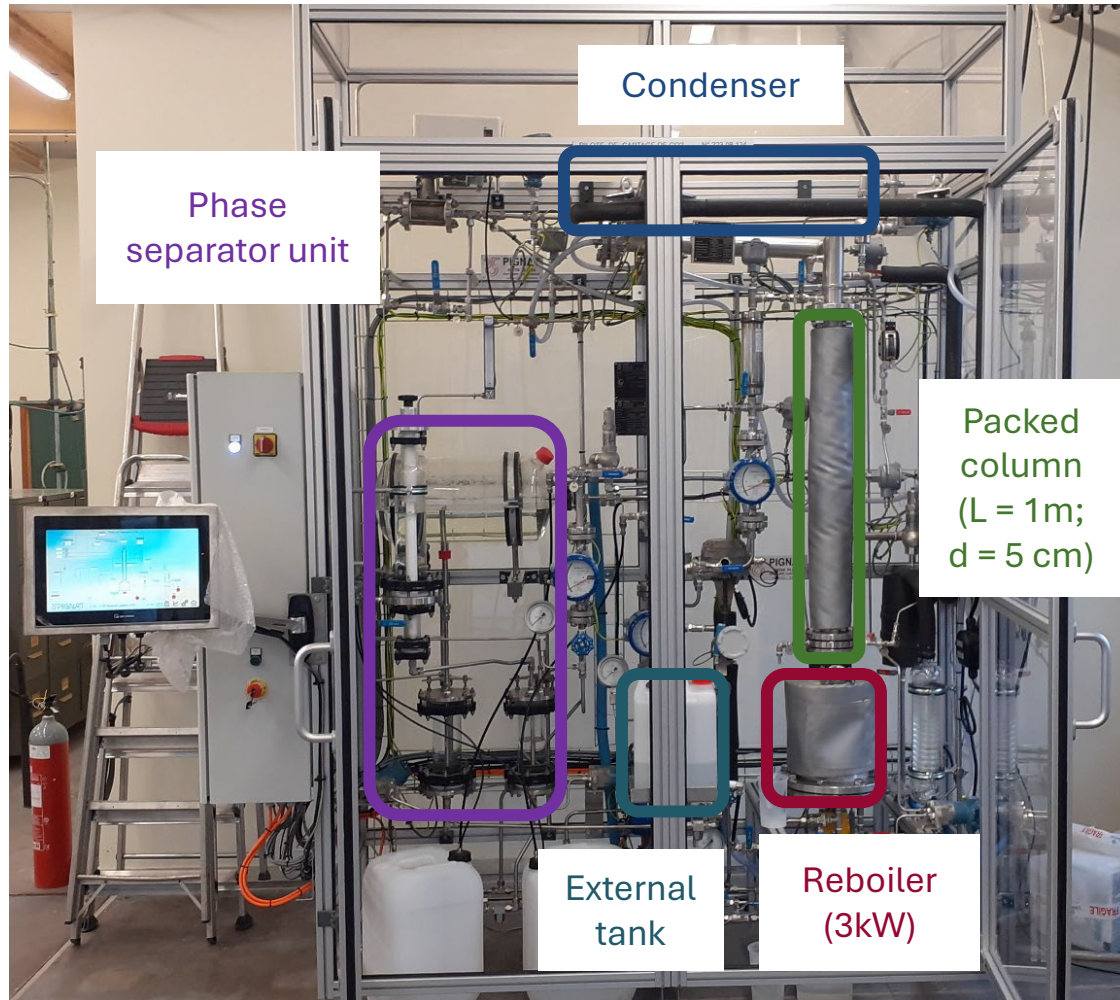
Aqueous-alcoholic MEA-based solution

- Same fast chemical reactions as for the MEA benchmark
- Propan-1-ol used as a demixing inducer
- Up to **97.9% of the CO₂ in the rich phase** (60% of the total volume)
- Challenge about the alcohol volatility (condenser / intercooling)
- 20%-reduction for regeneration energy >< aqueous MEA (30 wt.%) solvent (despite higher liquid flow rate)

Perspectives

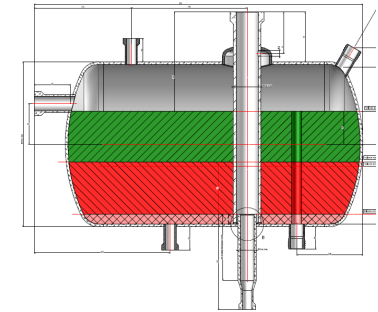
- Micro pilot Absorption-Regeneration unit tests + simulations

Micro pilot Absorption-Regeneration unit



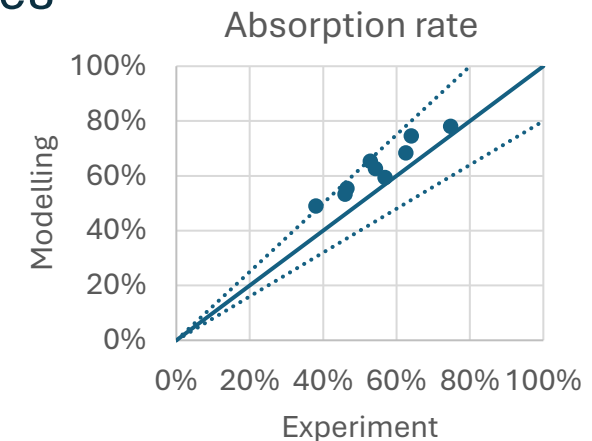
Multiple possibilities of use

- Two modes
 - ✓ Absorption
 - Continuous tests
 - Semi-continuous tests
 - ✓ Regeneration
- Use of **demixing** solvents (with phase separator unit)
- Regeneration under **pressure** (up to 3 barg)



Objectives

- **AspenPlus model validation**
 - ✓ experimental vs modelling on AspenPlus at this scale
 - First promising results with aq. MEA (30 wt.%)



Conclusion

Aqueous-alcoholic MEA-based solution

- Same fast chemical reactions as for the MEA benchmark
- Propan-1-ol used as a demixing inducer
- Up to **97.9% of the CO₂ in the rich phase** (60% of the total volume)
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Perspectives

- Micro pilot Absorption-Regeneration unit tests + simulations
- Other aqueous-alcoholic solvents

Thank you very much for your attention

Any QUESTIONS?

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