





HEAT DUTY EVALUATION OF A NOVEL SOLVENT BLEND IN A CATALYST- AIDED CO₂ POST COMBUSTION CAPTURE PROCESS.

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Presentation outline

Introduction

- Background review & Solvent selection
- Process optimization & Objectives
- Experimental section
- Results and Discussion
- Conclusions
- References

Introduction



Background review

Amine Selection



Structure & Activity Relationship Studies (Singh et al., 2007, 2008, 2009)





(Chowdhury et al., 2013)

Solvent Selection Criteria



Absorption Parameter=Initial Absorption rate *pKa *Absorption capacity

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Desorption Parameter = <u>Initial Desorption rate* Cyclic Capacity</u> _{Heat Duty}

(Narku-Tetteh et al., 2017)

Selection Chart



Selection Chart for single amines

BMEA: Butylmonoethanolamine AMP: 2-Amino-2-methyl-1propanol Selection Chart for blended amines

5M triblend : 2M BEA:2M AMP:1M MEA 5M bi blend: 2.5 BEA:2.5AMP 4M biblend : 2M BEA:2M AMP 5

Process Optimisation

- The use of solid acid catalyst (HZSM-5) in reducing the heat of amine regeneration was first patented by Idem et al., 2017
- Srisang et al., 2017 and Decardi-Nelson et al. 2017 implemented the process for the first time in a pilot plant.
- The results showed a significant reduction in the heat duty and an overall improvement in the absorber efficiency and cyclic capacity.

Objectives

- Validate the criteria for selection of single and blended novel amine solvents developed from a batch process in an earlier work using a bench scale post combustion CO₂ capture plant.
- Evaluate any benefits provided by the improved new amine solvent blend using a bench scale post combustion CO₂ capture plant in terms of absorber efficiency, cyclic capacity and heat duty.
 - Evaluate the contribution of a solid acid catalyst in lowering the heat duty after introducing into the desorption column of a bench scale post combustion CO_2 capture plant.

Experimental Section

Schematic representation of the bench scale experimental set-up for CO₂ capture



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(Srisang et al., 2017)

Experimental Conditions

- ▶ 4M Bi blend (2:2 BEA:AMP)
- ► 7M MEA-MDEA (Base case)
- Base case better than 5M MEA (Decardi-Nelson et al., 2017)
- Operating conditions used in the pilot plant experiments

Condition	Value	
Solvent used	7M MEA/MDEA, 4M BEA/AMP	Absorber efficiency
Solvent flowrate	60 mL/min	$= \frac{G_{in * X_{CO_2in}} - G_{out} * X_{CO_2out}}{G_{in * X_{CO_2in}}} 100\%$
Feed Gas flow rate	15 SLPM	
CO ₂ in feed gas	15%	$\mathbf{q} = \frac{m_{hw*Cp_{hw}}*(T_{hw,in}-T_{hw,out})}{m_{CO_2}}$
Desorber amine inlet Temperature	87°C	*Absorber Efficiency
Desorber Catalyst	HZSM-5 (Si/Al =19)	 Heat duty Cyclic capacity
Desorber Catalyst weight	0g, 150 g	
Absorber inlet Temperature	28°C	9

Results and Discussion

Comparison of novel blend with base case



Results and Discussion (Cont'd)

Process Improvement (Catalytic Runs)

Absorber Efficiency

Cyclic Capacity

Catalytic Run



Catalytic run



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Heat Duty

Catalytic run



Results and Discussion (Cont'd)

Catalytic Effect



Role of Catalyst

Without catalyst, For carbamate forming amines like MEA and BEA, desorption reactions are shown:

Step 1: Carbamate breakdown

 $MEA/BEACOO^{-} + H_{3}O^{+} \leftrightarrow MEA/BEA + CO_{2} + H_{2}O$

Step 2: Amine Deprotonation

 $MEA/BEAH^{+} + H_{2}O \iff MEA/BEA + H_{3}O^{+}$

For sterically hindered amine like AMP the reaction mechanism is as shown below.

Step 1: Carbamate hydrolysis

 $AMPCOO^{-} + H_2O \leftrightarrow AMP + HCO_3^{-}$

Step 2: bicarbonate breakdown

 $AMPH^+ + H_2O \leftrightarrow AMP + H_3O^+$

 $\text{HCO}_{3^{-}} + \text{H}_{3}\text{O}^{+} \leftrightarrow \text{CO}_{2} + 2\text{H}_{2}\text{O}$

For bicarbonate forming amines like MDEA, the reaction is as follows:

 $MDEA + CO_2 + H_2O \leftrightarrow MDEAH^+ + HCO_3^-$



Heat Duty Terms

Heat Duty- $(H_{sens} + H_{vap}) = H_{des}$

Heat duty, q =
$$\frac{m_{hw*Cp_{hw}}^{*(T_{hw,in}-T_{hw,out})}}{m_{CO_2}}$$

- Heat of vaporisation, H_{vap} obtained from steam tables at the average operating temperature
- Sensible heat, H_{sens} obtained using energy balance of both liquid and gas phases.

Schematic Illustration for Calculation of Sensible Heat

m_{g1}

 m_{g2}

 m_{11}

 m_{12}

 T_1

 T_2

α

 α_1

 α_2



 CO_2 in gas phase in stream entering heater (kg/l.soltn) CO_2 in gas phase in stream leaving heater (kg/l.soltn) mass of liquid solution entering heater (kg/l.soltn) mass of liquid solution leaving heater (kg/l.soltn) amine solution temperature at heater inlet amine solution temperature at heater outlet loading of amine solution entering lean-rich heat exchanger loading of amine solution entering heater loading of amine solution exiting the heater

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Summary of Heat duty terms for the blends





- Thus, the role of catalyst is clearly manifested in the H_{des} for both systems.
- However, the values of H_{des} are apparent (a factor of amine cyclic capacity)

The catalytic effect on both the sensible heat and heat of vaporisation are negligible.



Conclusions

The pilot plant test validated the selection as well as the selection criterion of BEA and AMP as the components for formulation of a good solvent blend.

The novel 4M BEA-AMP bi-blend showed very attractive CO₂ capture performance, and as such is a good potential solvent for post combustion CO_2 capture.

Employing the use of a catalyst resulted in a tremendous improvement in the absorber efficiency, cyclic capacity and a significant reduction in the heat duty.

The results show that part of the energy needed for CO_2 desorption is contributed by the catalyst in proton donation thereby reducing the external energy required for CO₂ desorption from the amine solvent.

The heat duty for the novel blend with and without the desorption catalyst (HZSM-5) were 6.91 GJ/tonne CO₂ and 8.71 GJ/tonne CO₂ respectively.

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THANK YOU QUESTIONS?