



Development of a new CESAR1 carbon capture model across various scales and CO₂ contents

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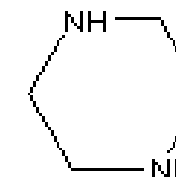
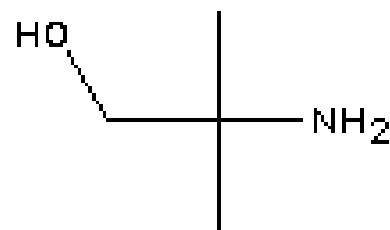


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CESAR1 is the new benchmark amine solvent

Aq. 27 wt.% 2-amino-2-methyl-1-propanol (**AMP**) + 13 wt.% piperazine (**PZ**)



Developed in the **CESAR European** funded-project

20-25% less energy consumption than MEA

Potential **higher stability** against **thermal** and **oxidative** degradation

Deploying CESAR1 systems requires robust models

Predicting performance for industrial applications

Design, optimisation and scale-up of CESAR1 plants

High-fidelity CESAR1 models are required in commercial softwares (Aspen Plus,...)

Limited information in the literature regarding comprehensive modelling of CESAR1

Objective

Develop and **validate** a comprehensive and robust **CESAR1 model** in **Aspen Plus** to predict performance for various industrial applications

Robust model over a **wide range** of **operating conditions**
(inlet CO₂ fraction, regeneration pressure)

Pilot plant scale **validation**: TCM Mongstad unit

Simulations at **varying** inlet **CO₂ contents** (from 4 to 20 vol.%)

Outline

Development of the model

Validation of the model

Application to industrial cases

Conclusions

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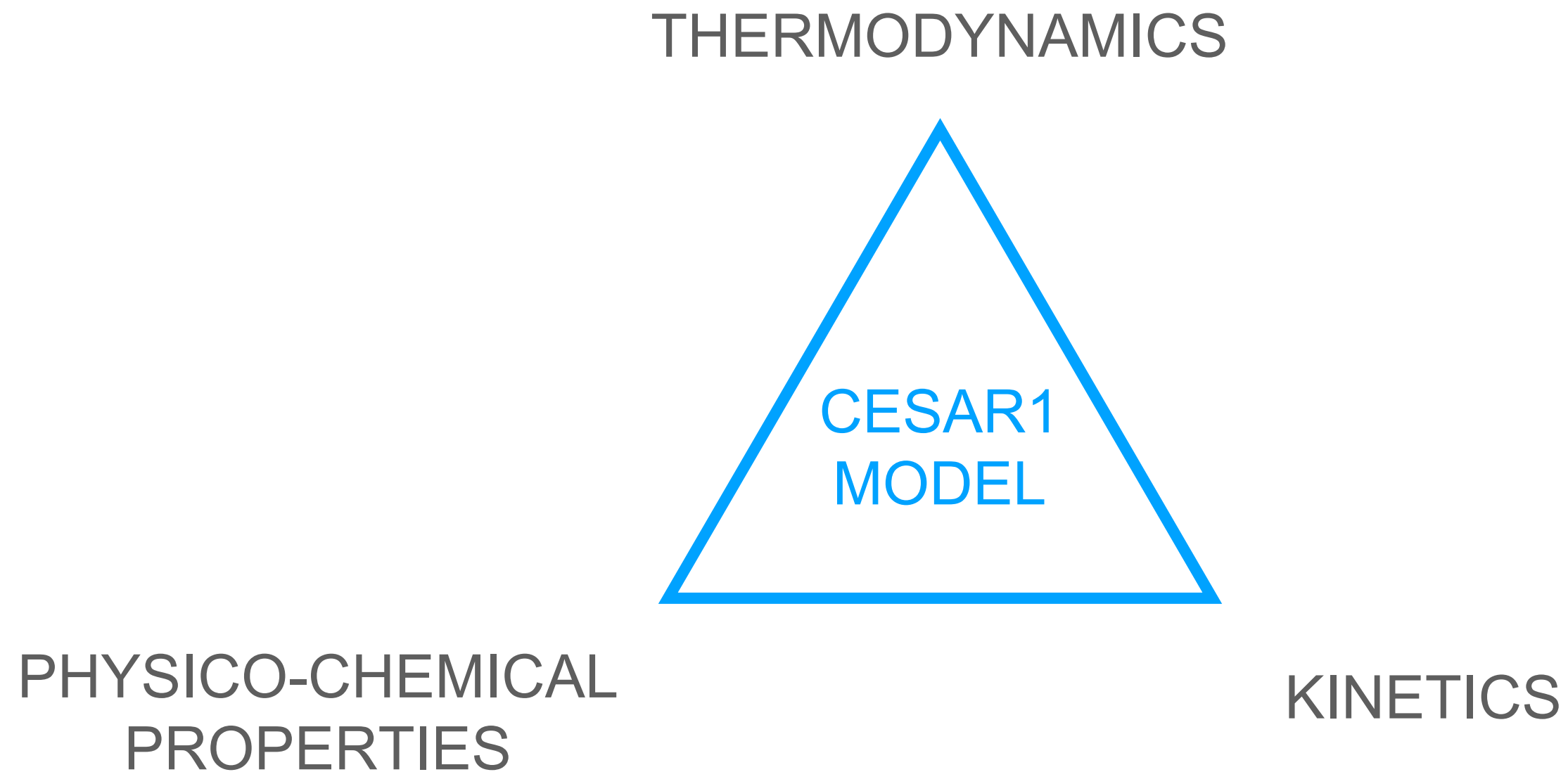
Development of the model

Validation of the model

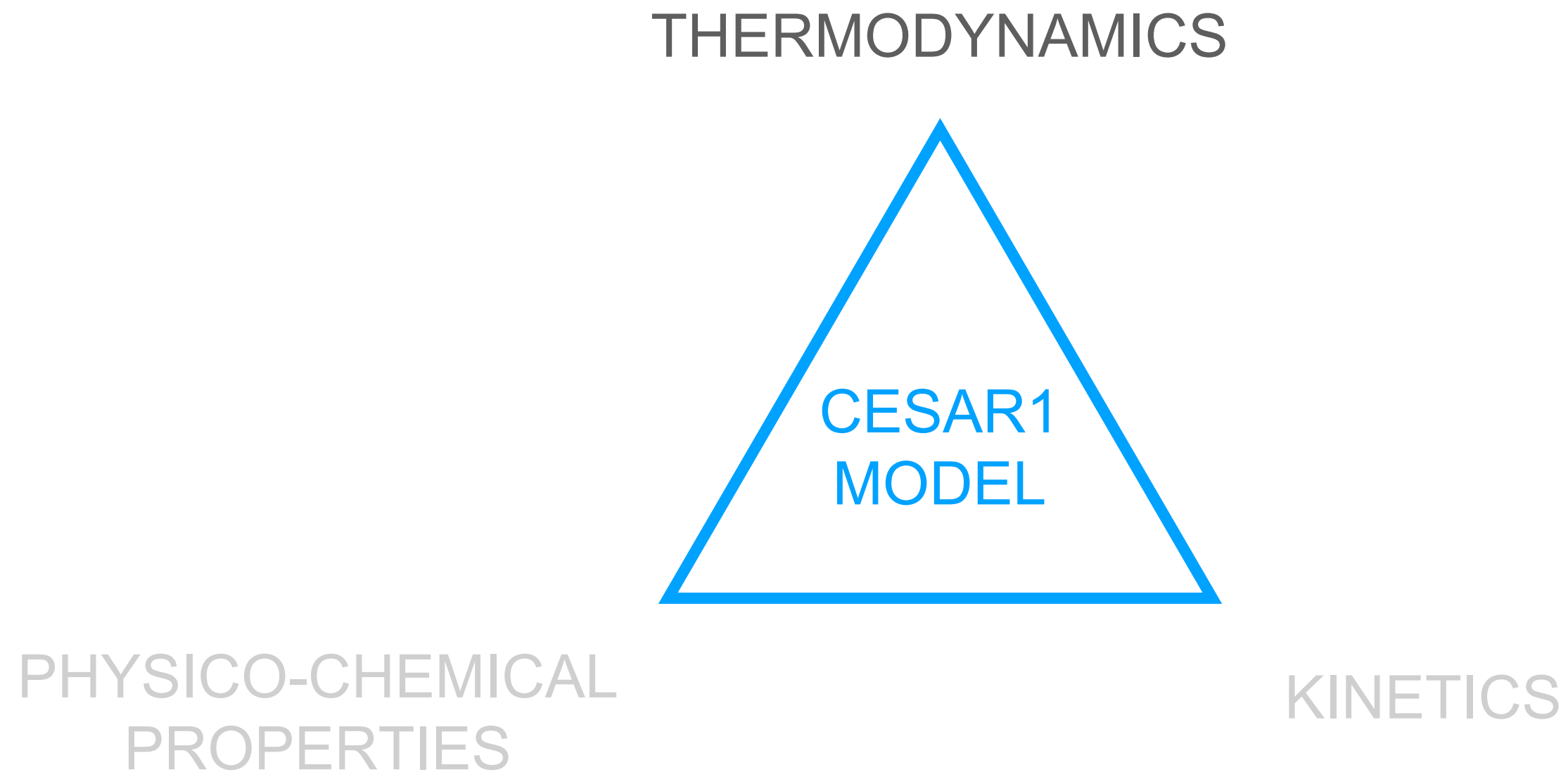
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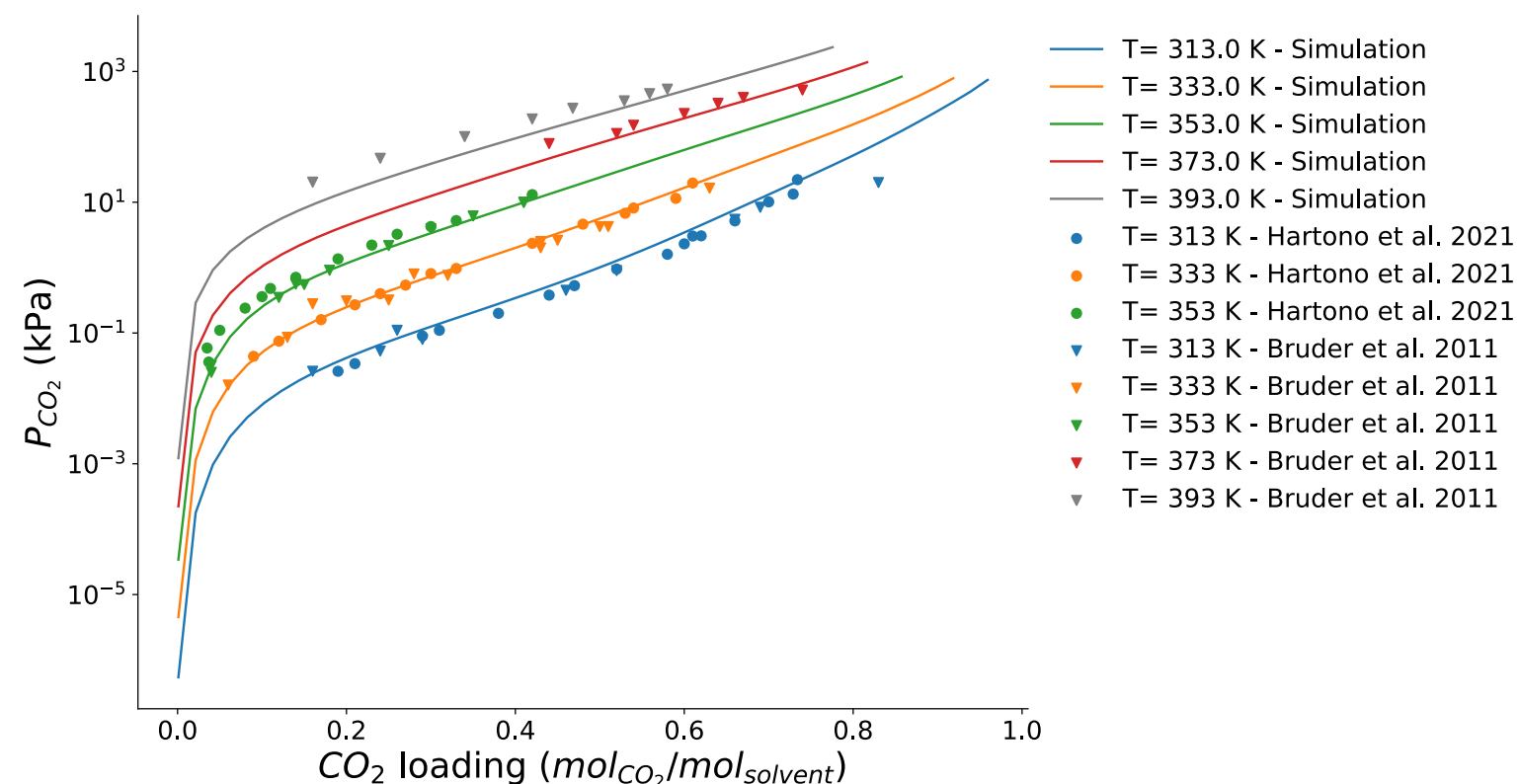
A robust model requires accurate sub-models



A robust model requires accurate sub-models



An open-access consistent Aspen Plus thermodynamic model is available in literature



ELECNRTL for liquid electrolyte

Redlich-Kwong-Soave for vapor phase

Sequential regression of model parameters using VLE and calorimetry data

Validated on a wide range of conditions:

AMP: 0-35.7 wt.% / PZ: 0-32.8 wt.%

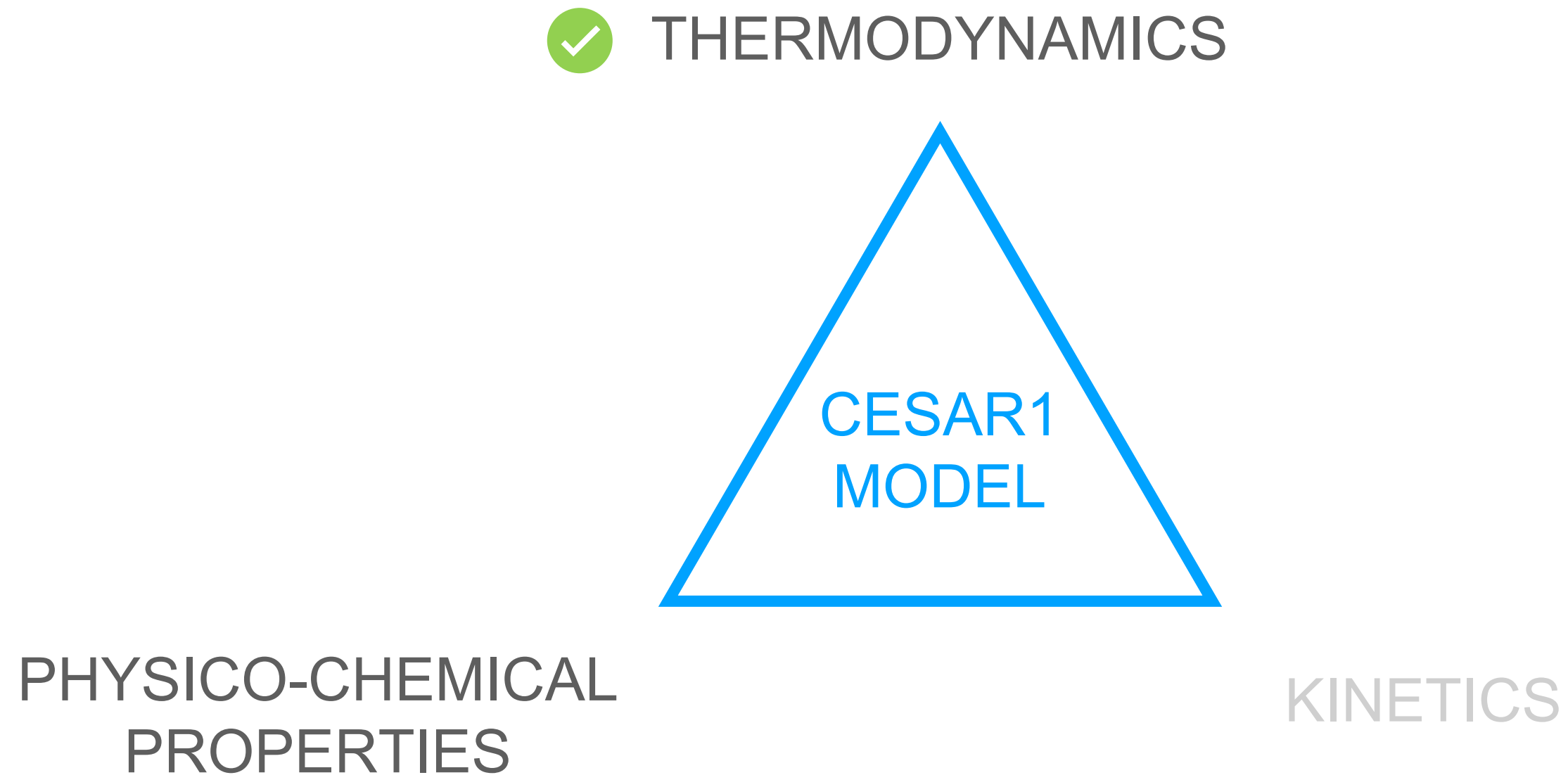
Temperature: 20-160°C

CO₂ loading: 0.04 – 1.07 mol_{CO₂}/mol_{amines}

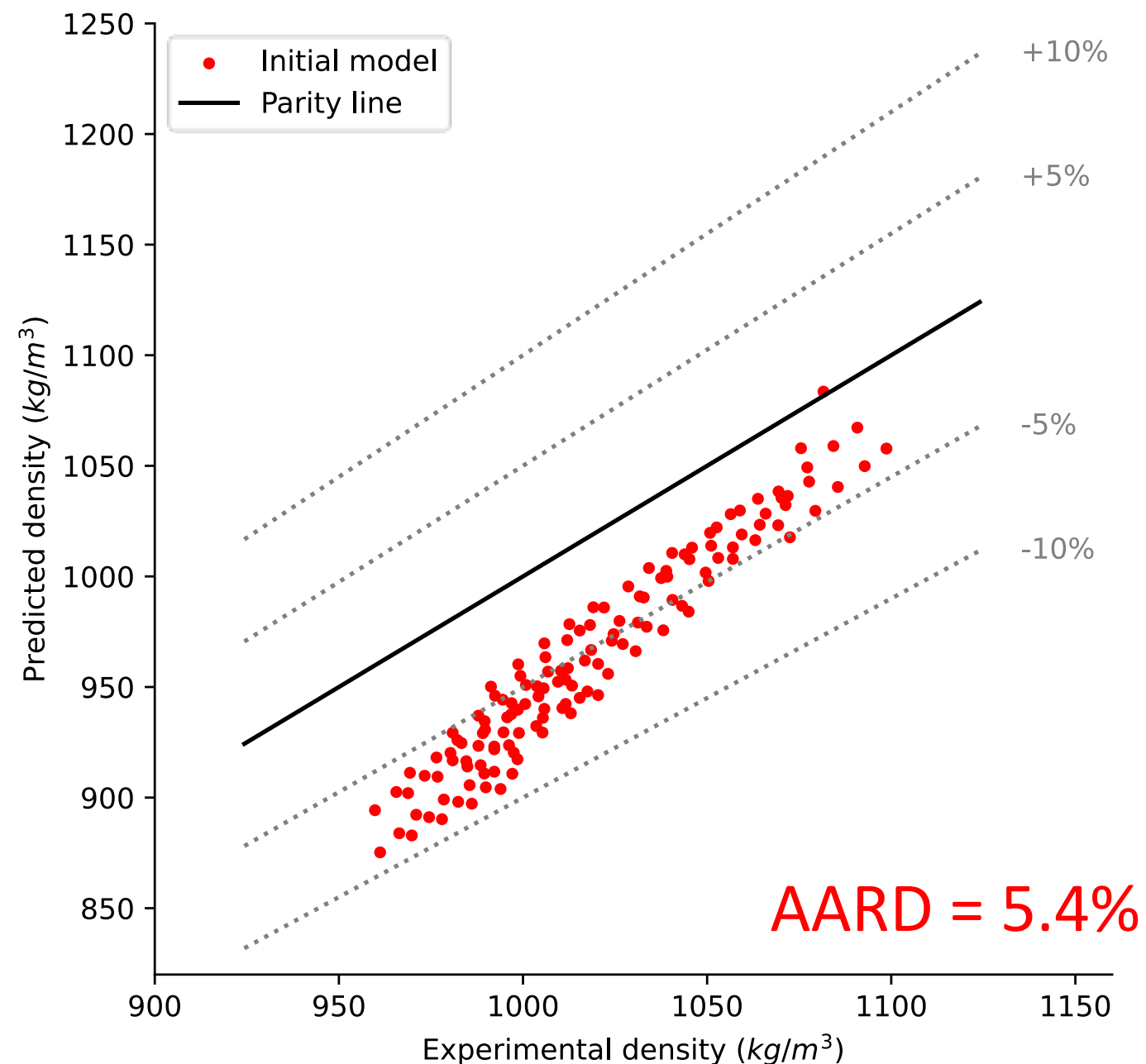
AARD = 22.3% for VLE

AARD = 6.3% for heat of CO₂ absorption

A robust model requires accurate sub-models



Initial density model with default parameters slightly underestimates predictions



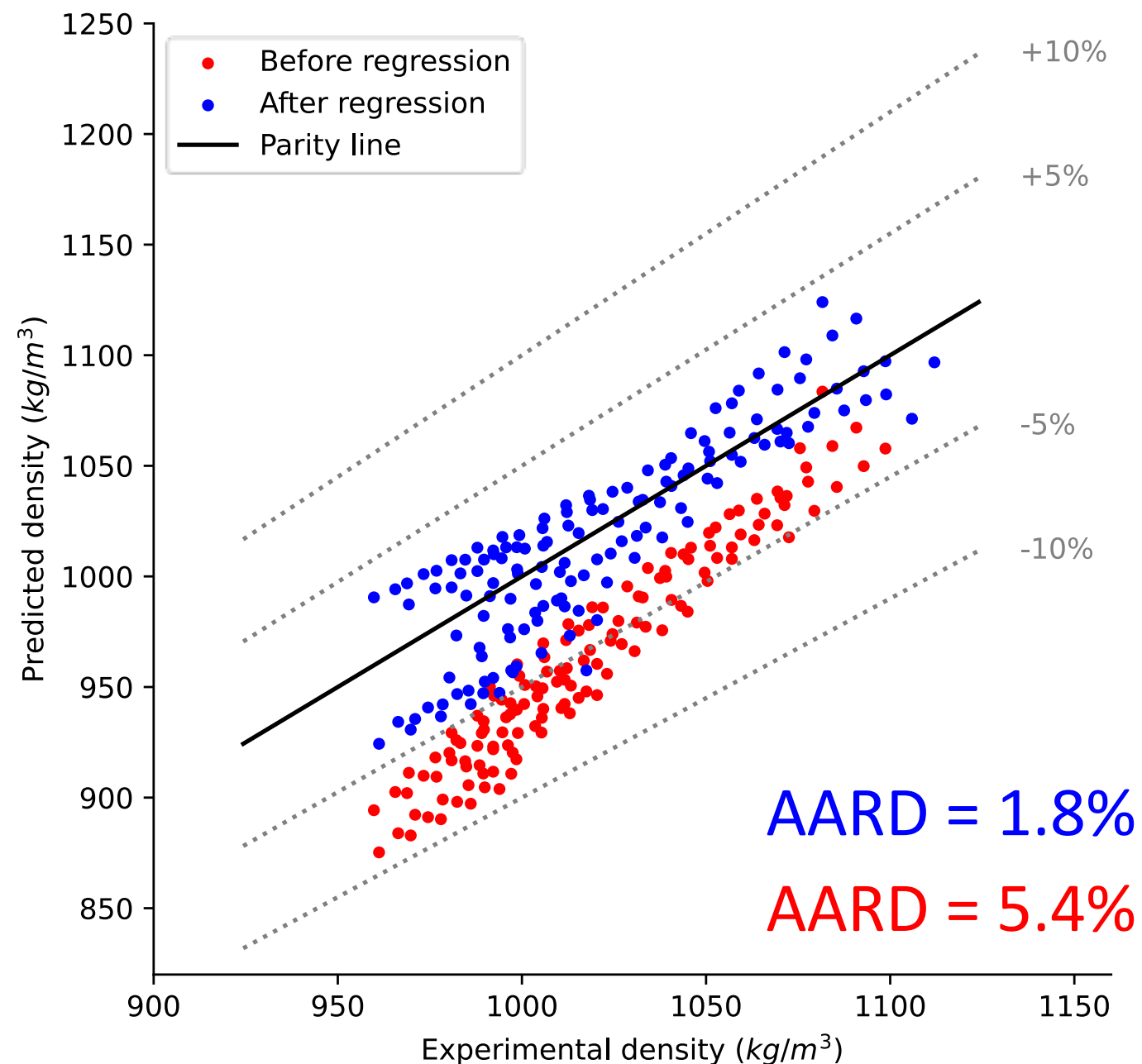
Clarke model: $V_{sol} = V_m + V_{el}$

$\swarrow$ $\searrow$

Rackett equation Redlich and Meyer

Missing parameters related to PZ and AMP ions
(default values)

Regressing ions related parameters allows to improve density prediction



Clarke model: $V_{sol} = V_m + V_{el}$

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Rackett equation Redlich and Meyer

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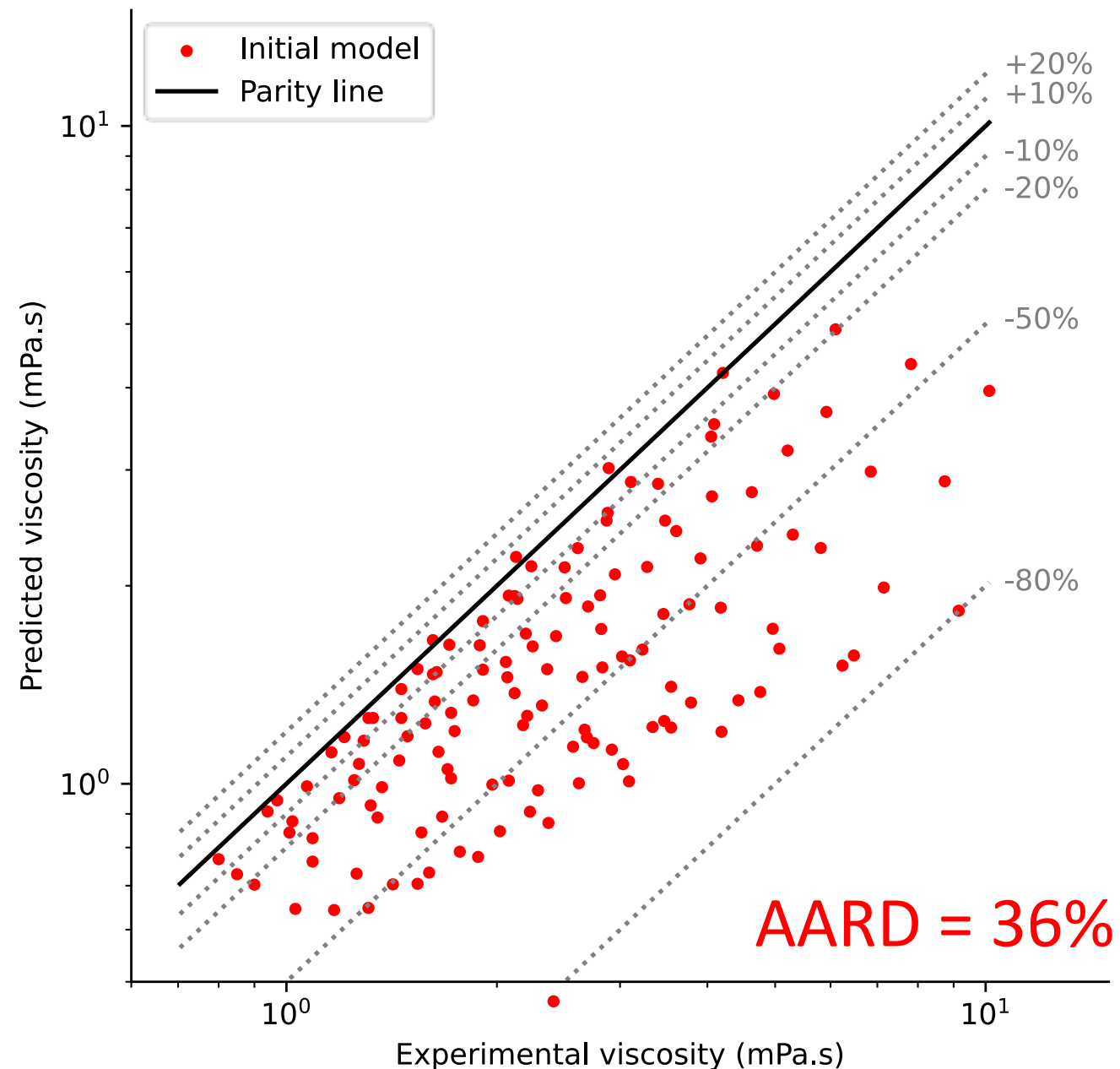
Regression of the missing parameters with
density data of *Morlando et al.*

AMP: 17.8-35.5 wt.% / PZ: 8.6–12.9 wt.%

Temperature: 20-80°C

CO₂ loading: 0 – 0.86 mol_{CO2}/mol_{amines}

Initial viscosity model with default parameters performs poorly



Jones-Dole model:

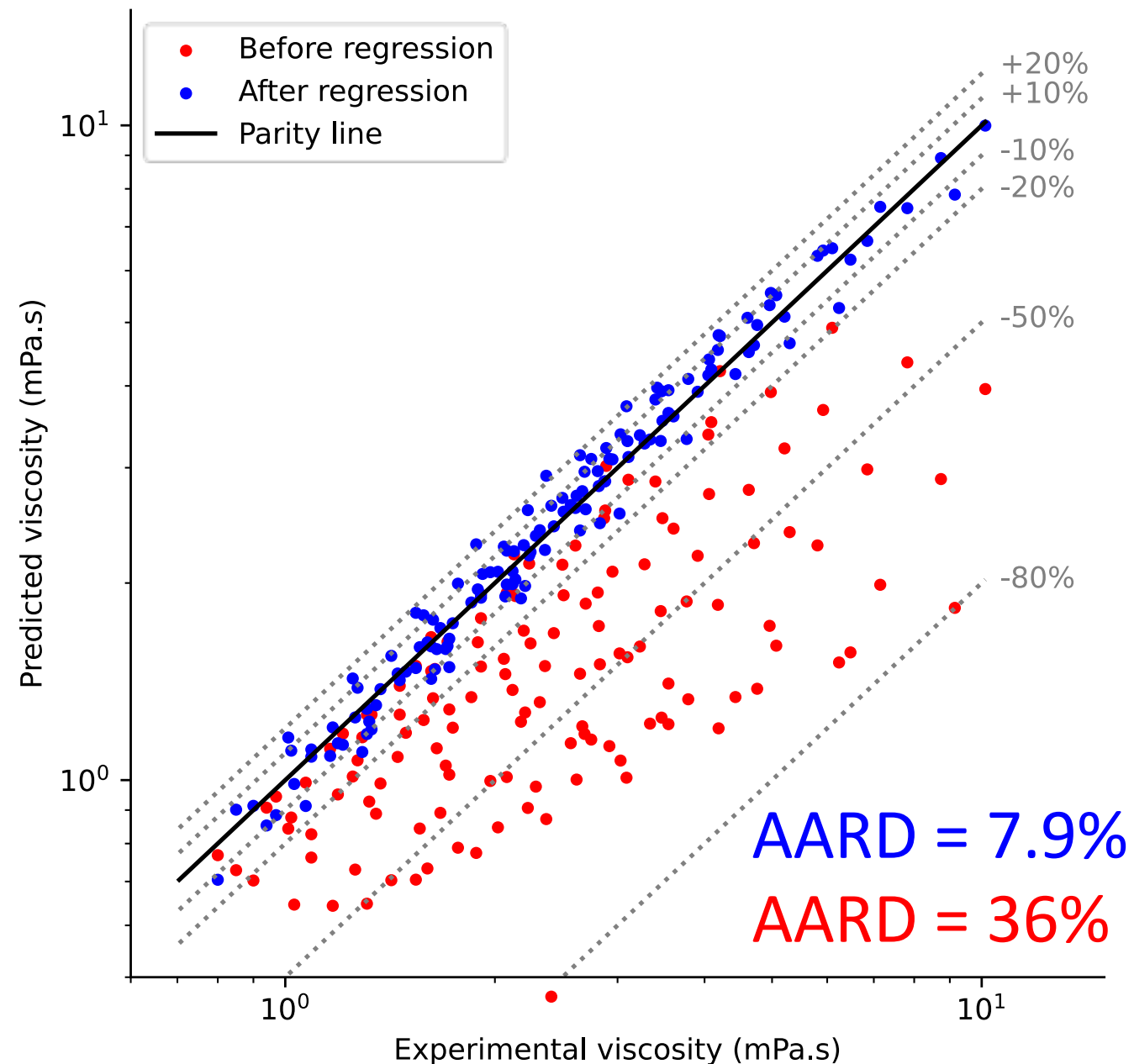
$$\eta_{sol} = \eta_m \left(1 + \sum_{ca} \Delta\eta_{ca} \right)$$

Aspen Liquid Mixture Viscosity model

Jones-Dole correction

Missing AMP interaction and AMP ions parameters (default values)

AMP-related parameters regression leads to significantly improved viscosity prediction



Jones-Dole model:

$$\eta_{sol} = \eta_m \left(1 + \sum_{ca} \Delta\eta_{ca} \right)$$

Aspen Liquid Mixture Viscosity model

Jones-Dole correction

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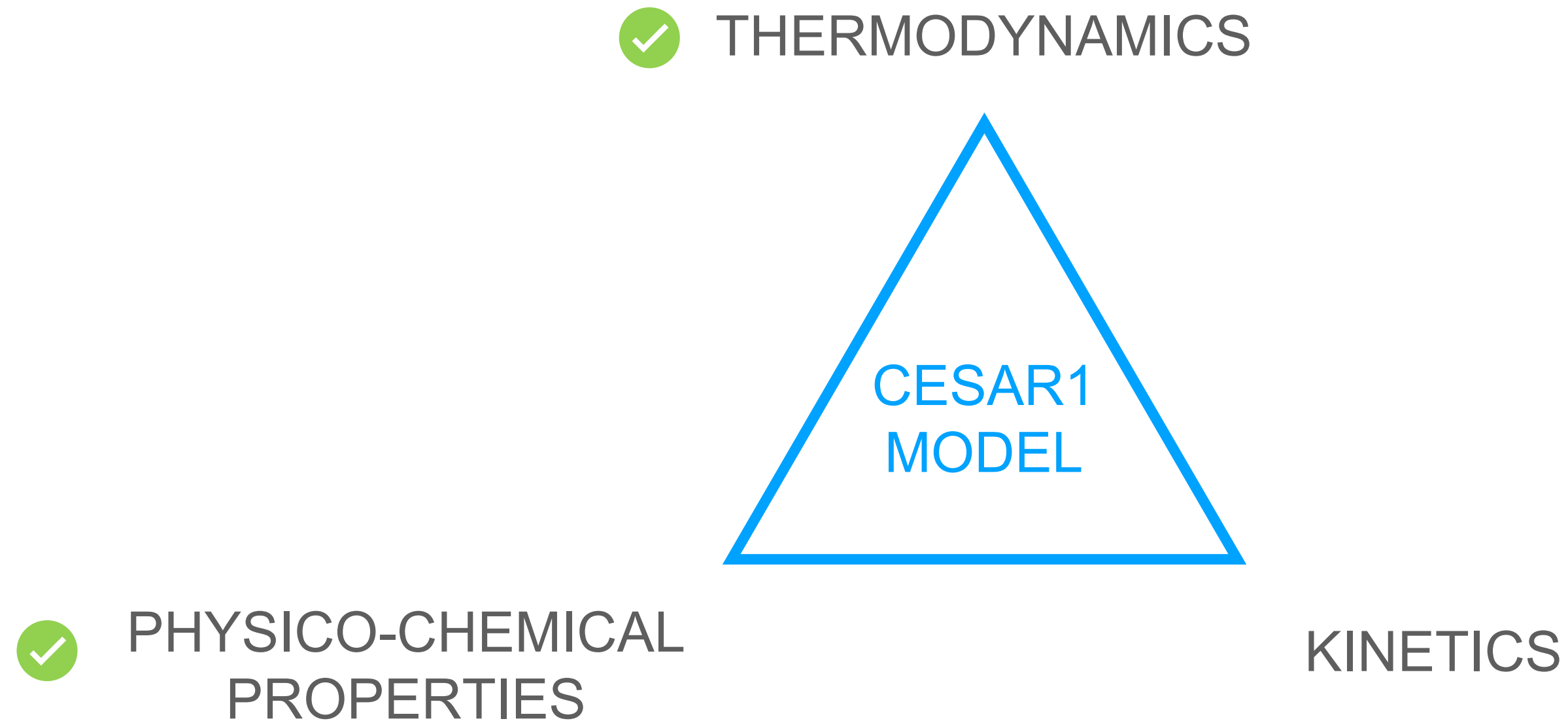
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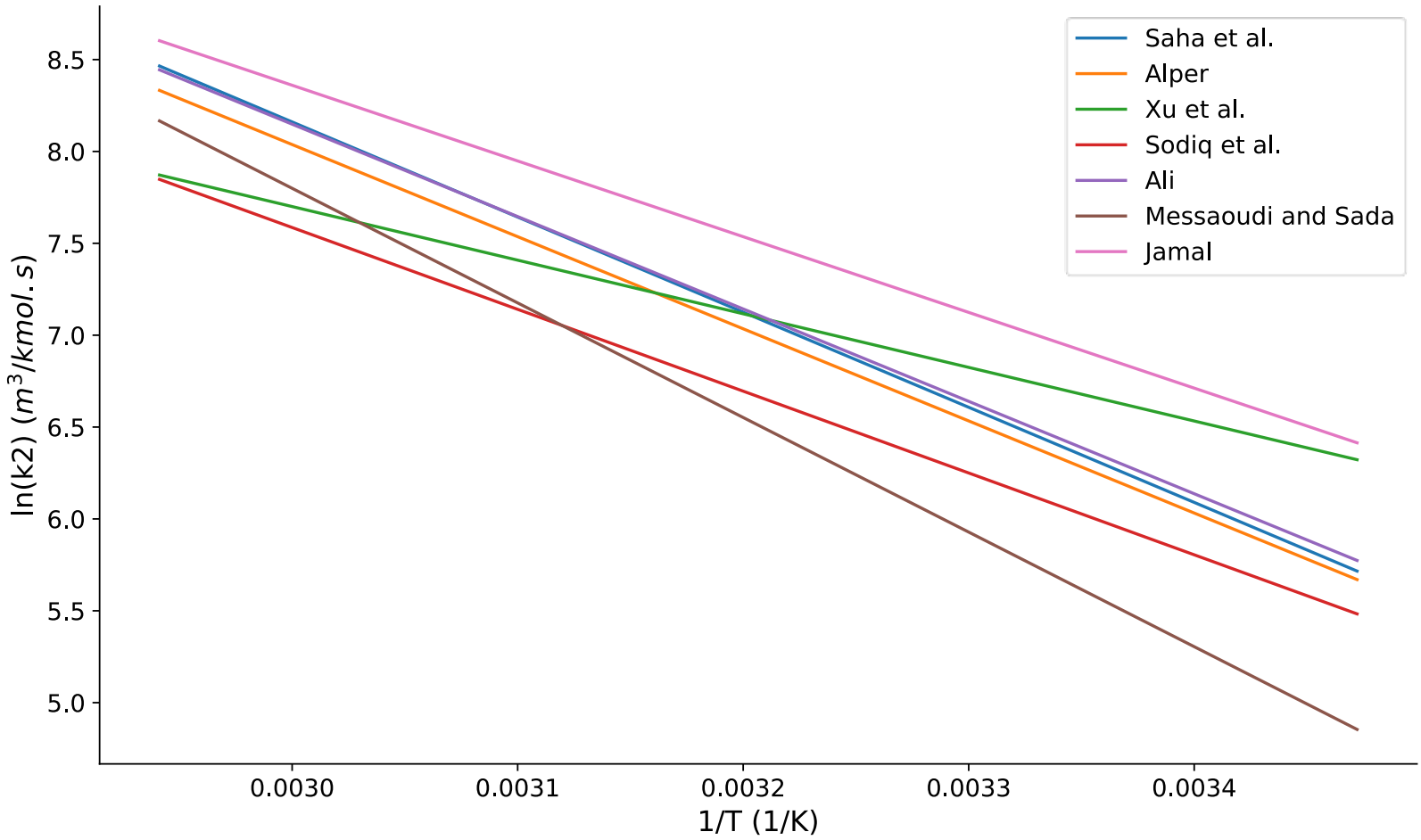
CO₂ loading: 0 – 0.86 mol_{CO2}/mol_{amines}

A robust model requires accurate sub-models



Significant differences exist among kinetics laws for AMP-CO₂ reaction in literature

REACTIONS	Kinetic laws
1) CO ₂ + OH ⁻ --> HCO ₃ ⁻	
2) HCO ₃ ⁻ --> CO ₂ + OH ⁻	
3) PZ + CO ₂ + H ₂ O --> PZCOO ⁻ + H ₃ O ⁺	
4) PZCOO ⁻ + H ₃ O ⁺ --> PZ + CO ₂ + H ₂ O	
5) PZCOO ⁻ + H ₂ O + CO ₂ --> PZCOO ⁻² + H ₃ O ⁺	
6) PZCOO ⁻² + H ₃ O ⁺ --> PZCOO ⁻ + H ₂ O + CO ₂	
7) AMP + CO ₂ + H ₂ O --> HCO ₃ ⁻ + AMPH ⁺	



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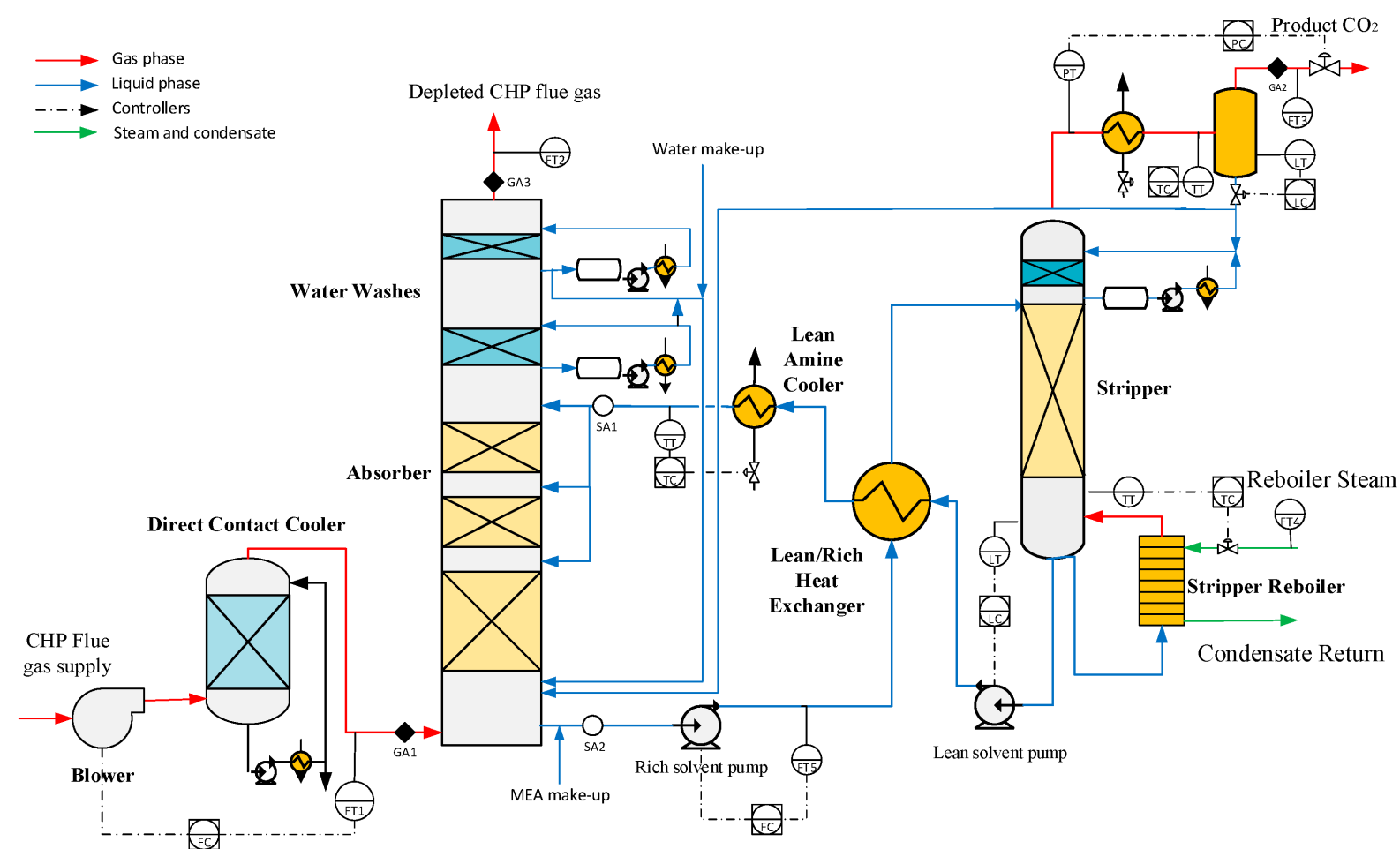
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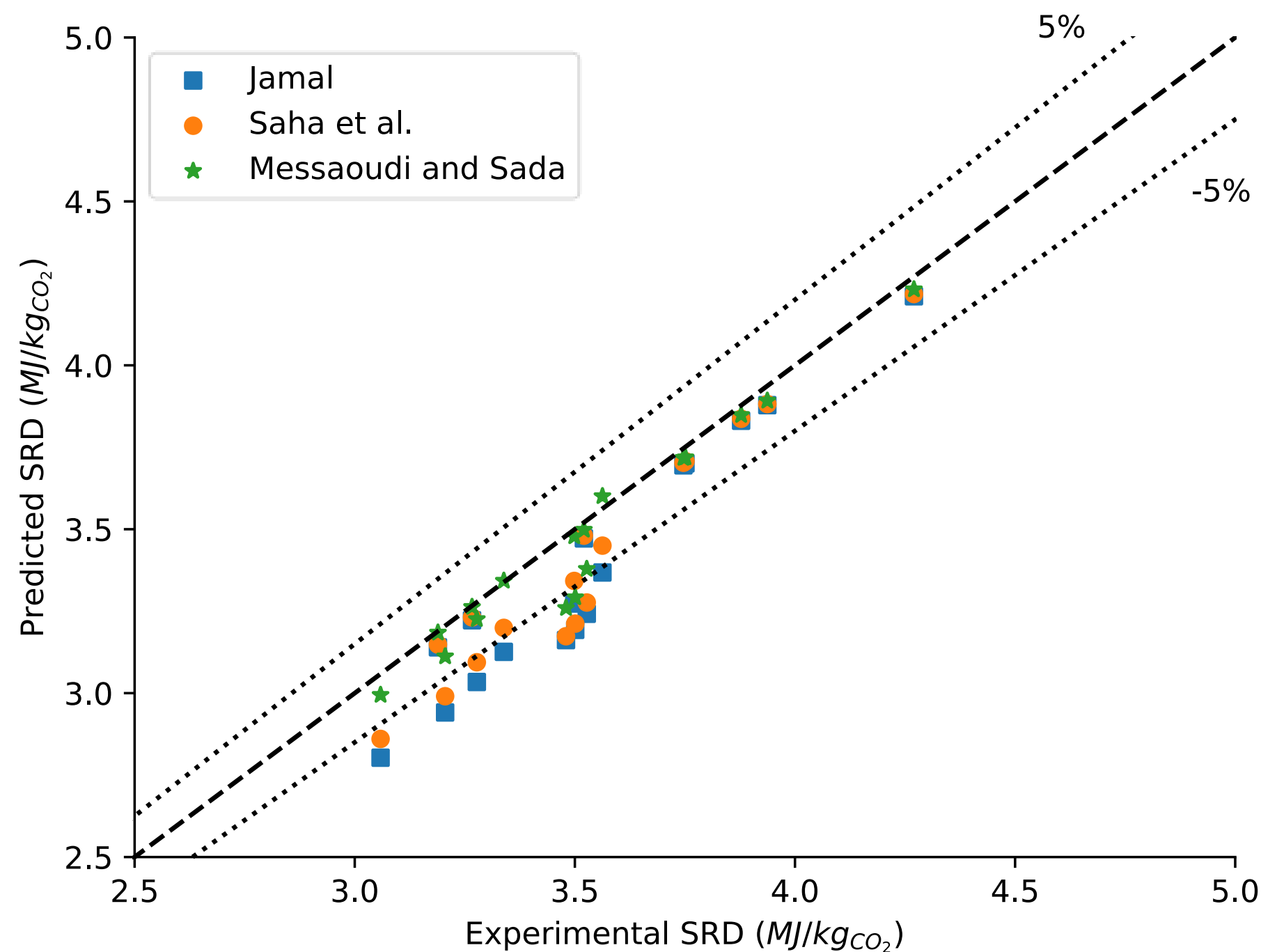
The amine plant unit at TCM Mongstad has been modelled in Aspen Plus



Absorber height	24 m
Stripper height	8 m
Absorber diameter	Rectangular 3.55*2 m
Stripper diameter	1.3 m
Packing type	Koch FLEXIPAC 2X
Stripper pressure	1.9 bar
CO ₂ content in gas	3.4 vol.%
Gas flow rate	50000 l/h
Solvent composition	27 wt.% AMP - 13 wt.% PZ
Capture rate	90-98%
L/G (kg/Sm ³)	0.6-1.2

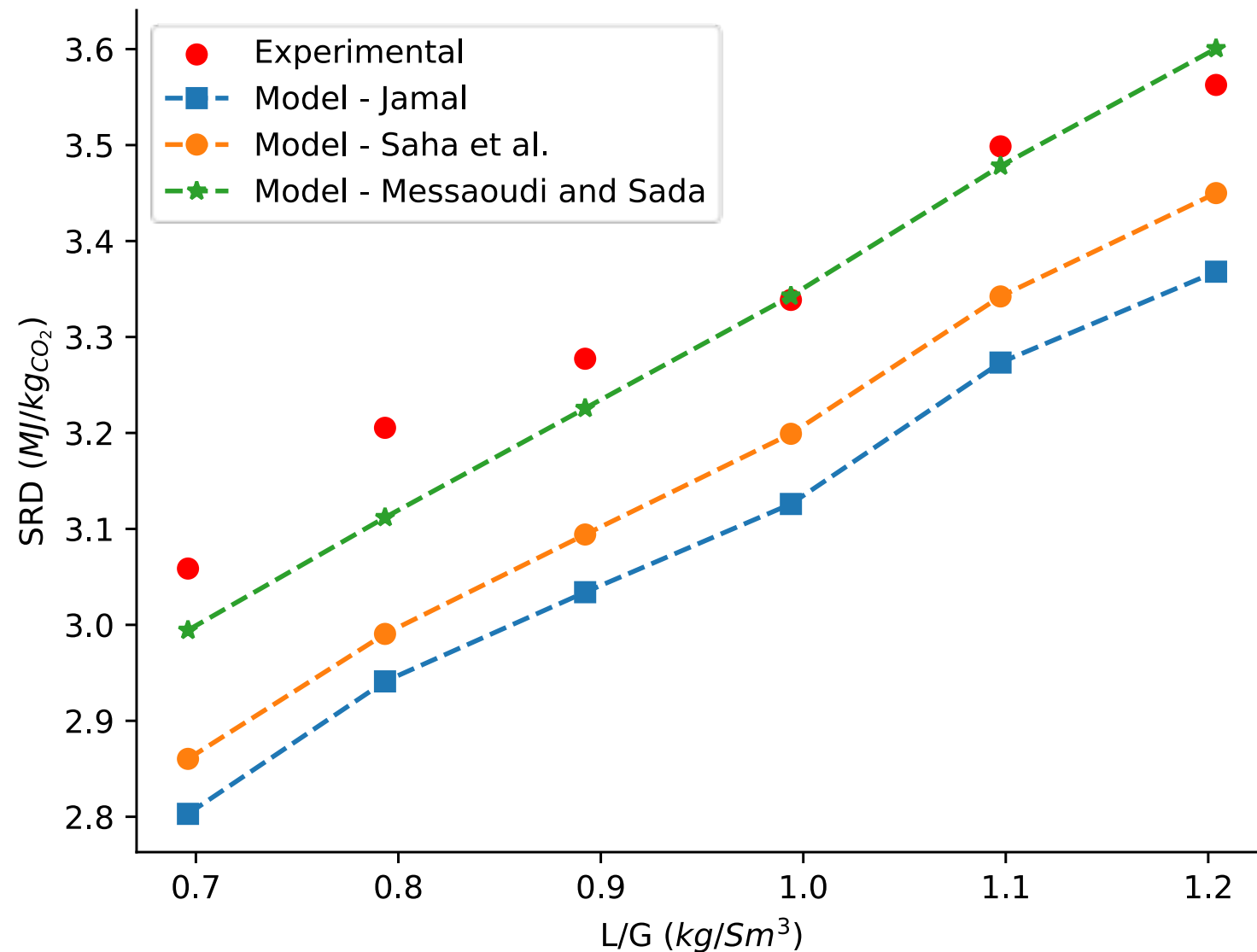
The CESAR1 model matches TCM Mongstad unit performance

Kinetic law AMP-CO ₂	AARD (%)
Jamal	4.62
Saha et al.	3.88
Messaoudi and Sada	2.08

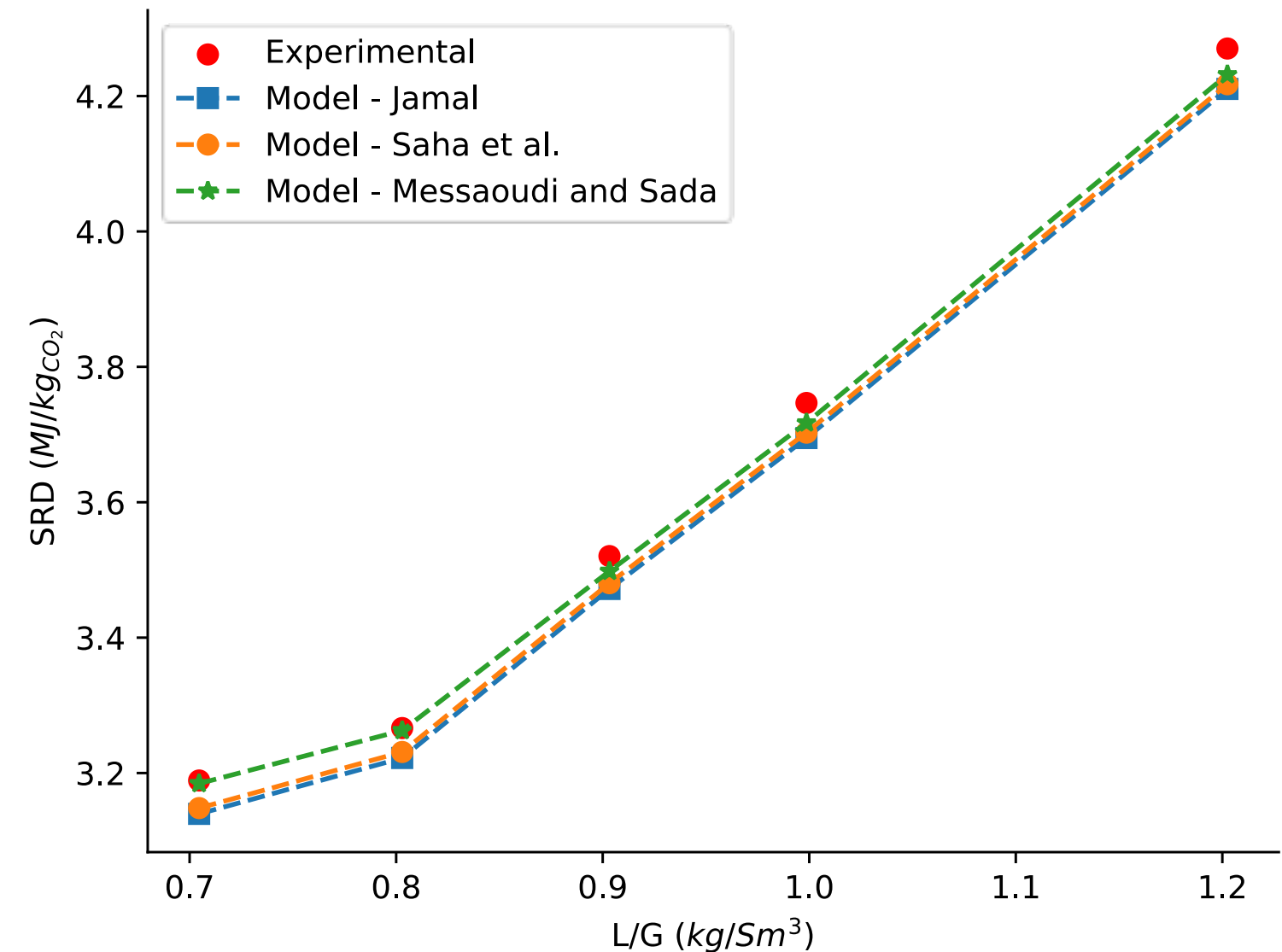


Messaoudi and Sada kinetic law best fits experimental data

capture rate $\approx 90\%$



capture rate $\approx 98\%$



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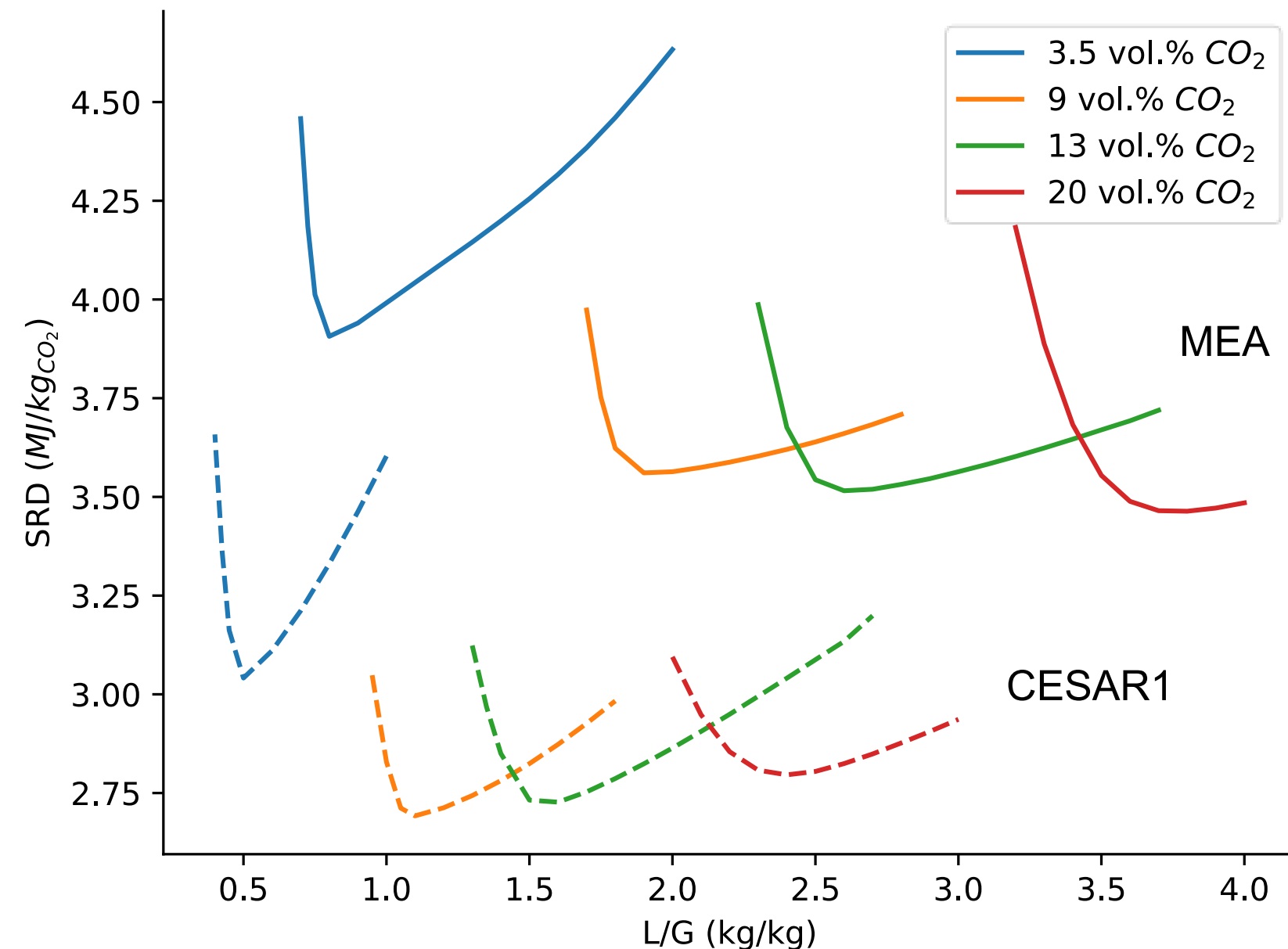
The model predicts a reduction in reboiler duty of 22% using CESAR1 instead of MEA

TCM Mongstad unit

90% capture rate

22% reduction in SRD with CESAR1

Results consistent with literature



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Development of a robust CESAR1 model in Aspen Plus

Extension of the CESAR1 thermodynamic model of Yi et al.

Accurate modelling of density and viscosity properties

Study of the impact of the kinetic laws for AMP-CO₂ reaction

Validation of the model with TCM Mongstad unit data (AARD=2%)

Simulations with variable inlet CO₂ contents, providing performance prediction with CESAR1 compared to MEA (22% SRD reduction)



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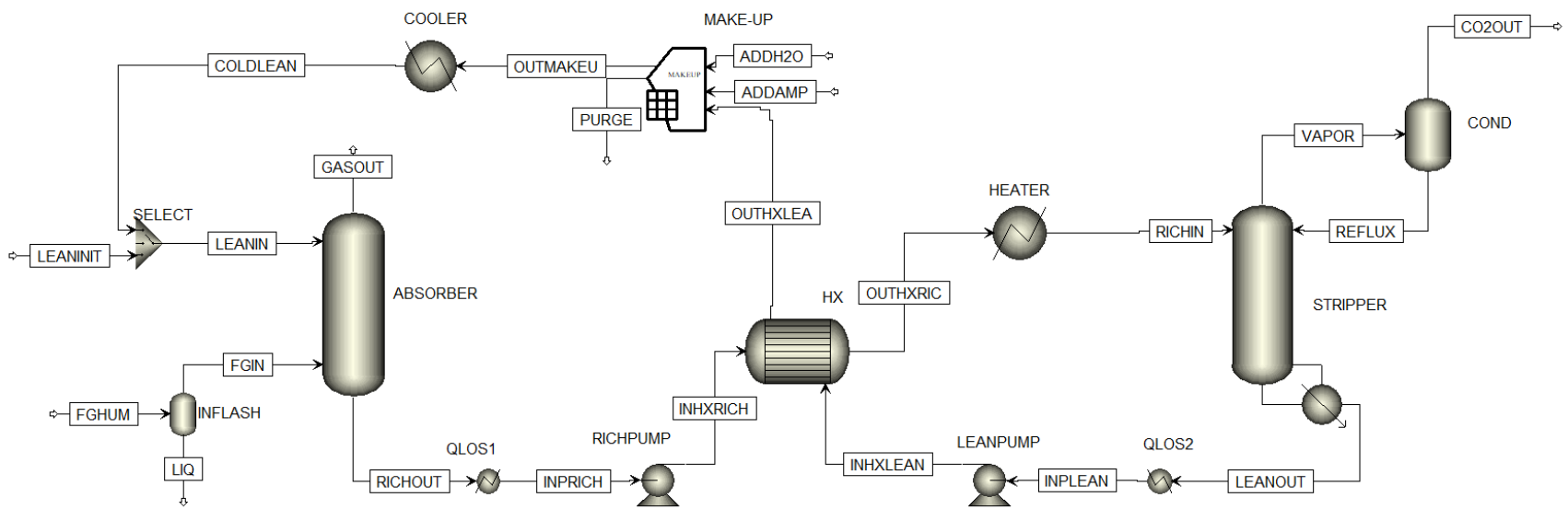


The UMONS lab-scale unit has been modelled in Aspen Plus

UMONS lab-scale unit



Aspen Plus model



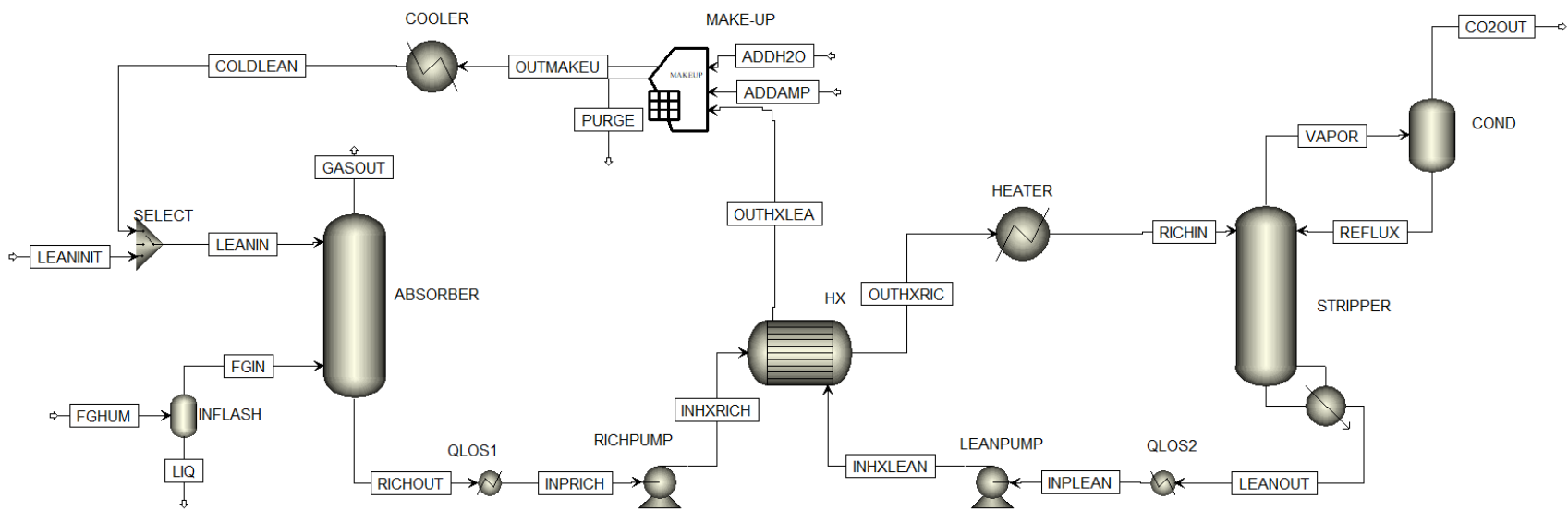
Absorber height	1 m
Stripper height	0.5 m
Columns diameter	0.06 m
Packing type	Glass Raschig Ring (6*6 mm)
Pressure	1 atm

The UMONS lab-scale unit has been modelled in Aspen Plus

UMONS lab-scale unit



Aspen Plus model



Absorber height	1 m
Stripper height	0.5 m
Columns diameter	0.06 m
Packing type	Glass Raschig Ring (6*6 mm)
Pressure	1 atm

Good agreement with lab-scale data, but validation remains limited

Inlet gas:

$$\dot{V} = 2701 \text{ l/h}$$

$$y_{CO_2} = 20 \text{ vol. \%}$$

(dry basis)

