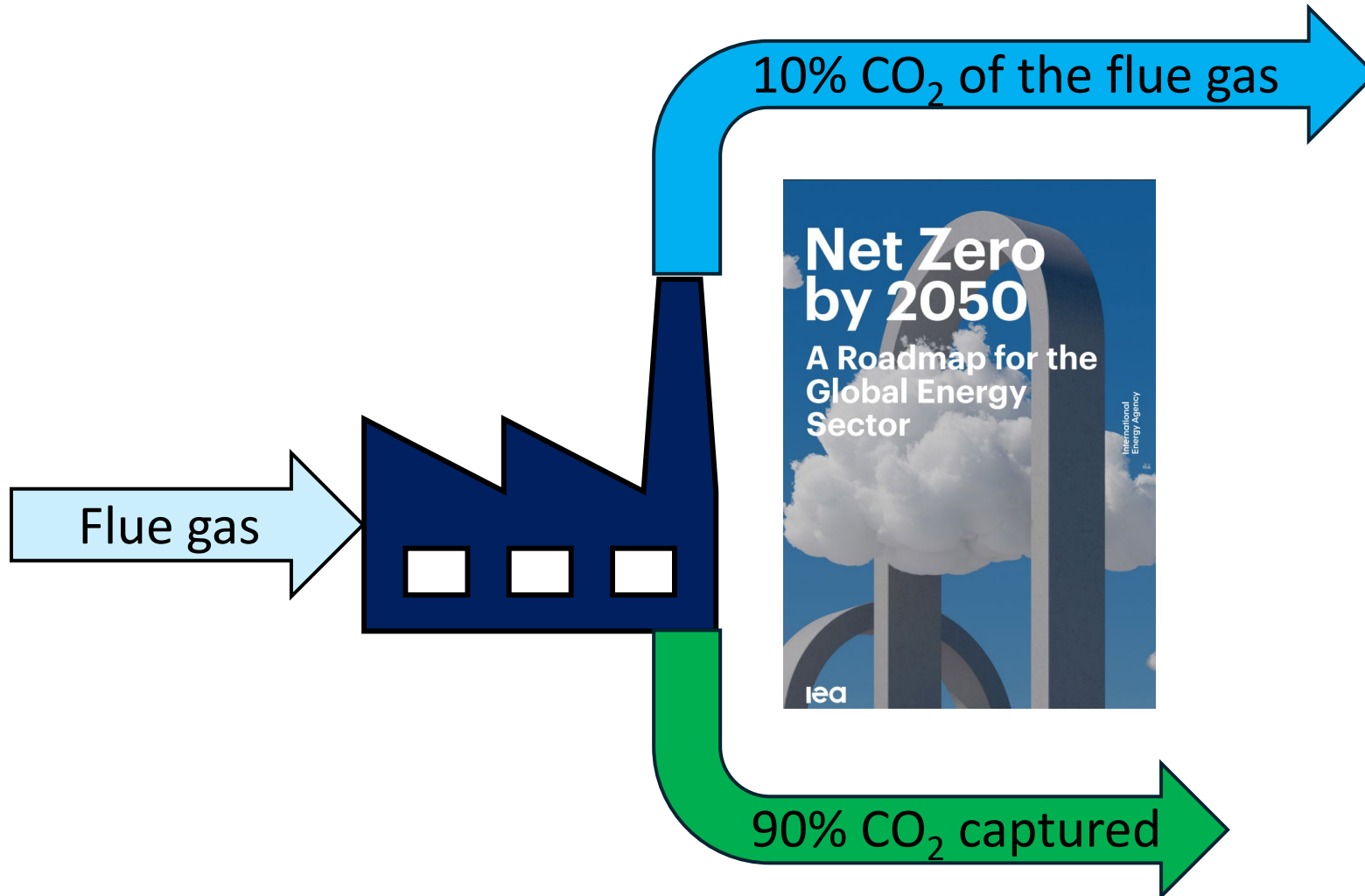




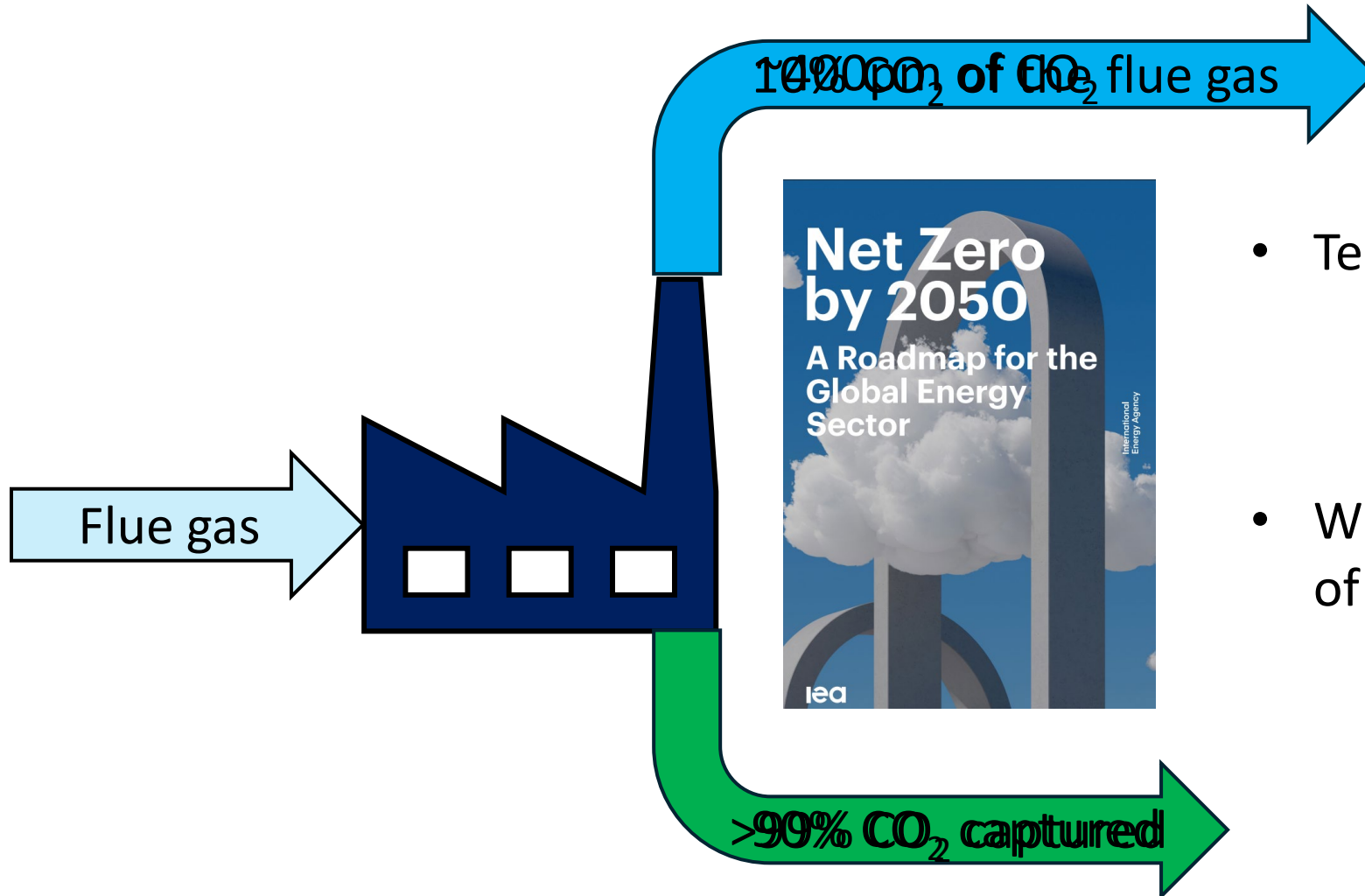
Reboiler duties at ultra-high CO₂ capture rates with MEA and CESAR1

Benas Mockus, Diego Morlando, Hanna K. Knuutila
Norwegian University of Science and Technology (NTNU)

Beyond 90% CO₂ capture



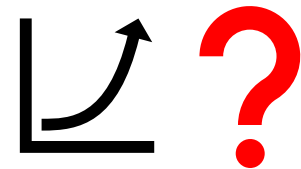
Beyond 90% CO₂ capture



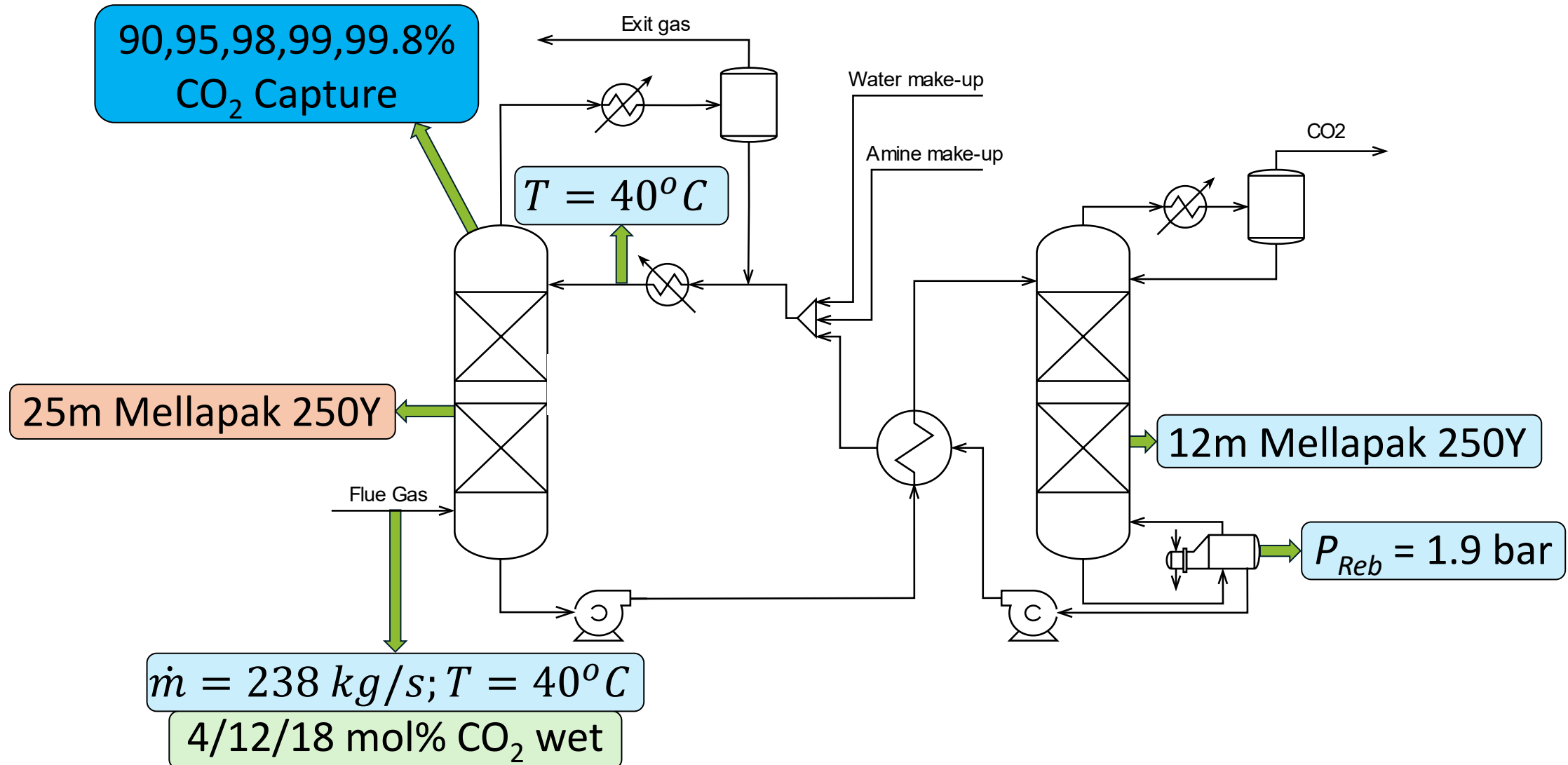
- Technically feasible



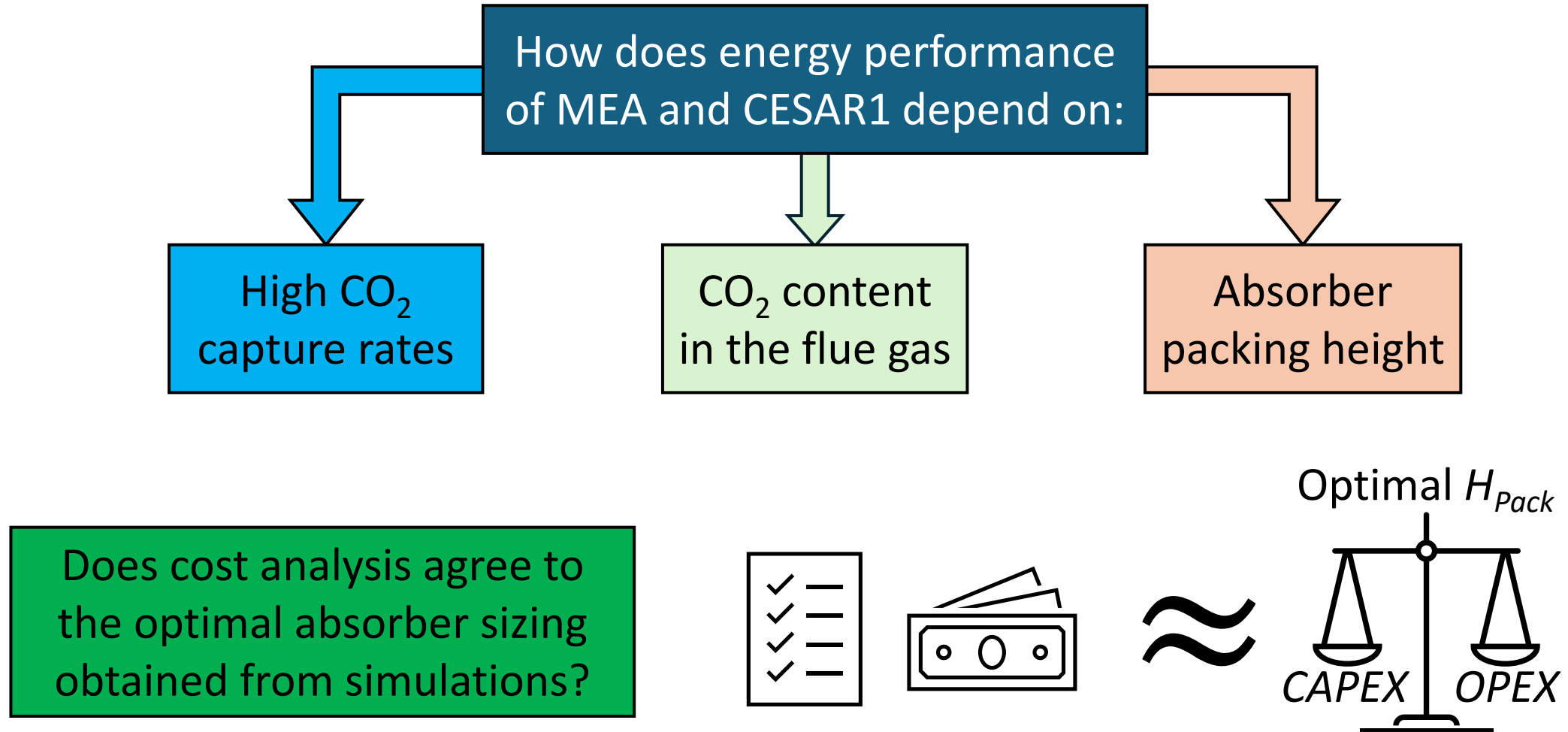
- What is energy performance of MEA and CESAR1?



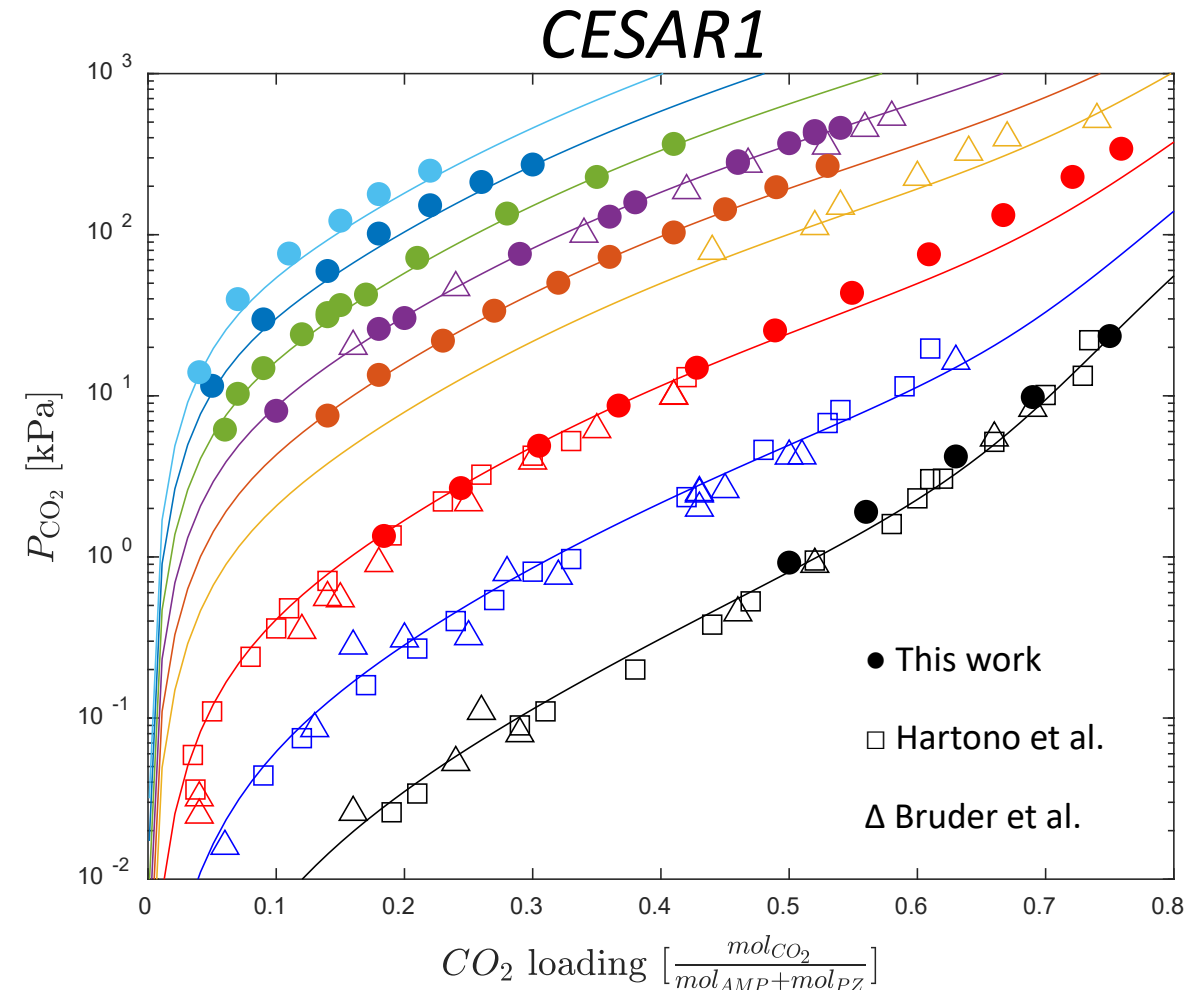
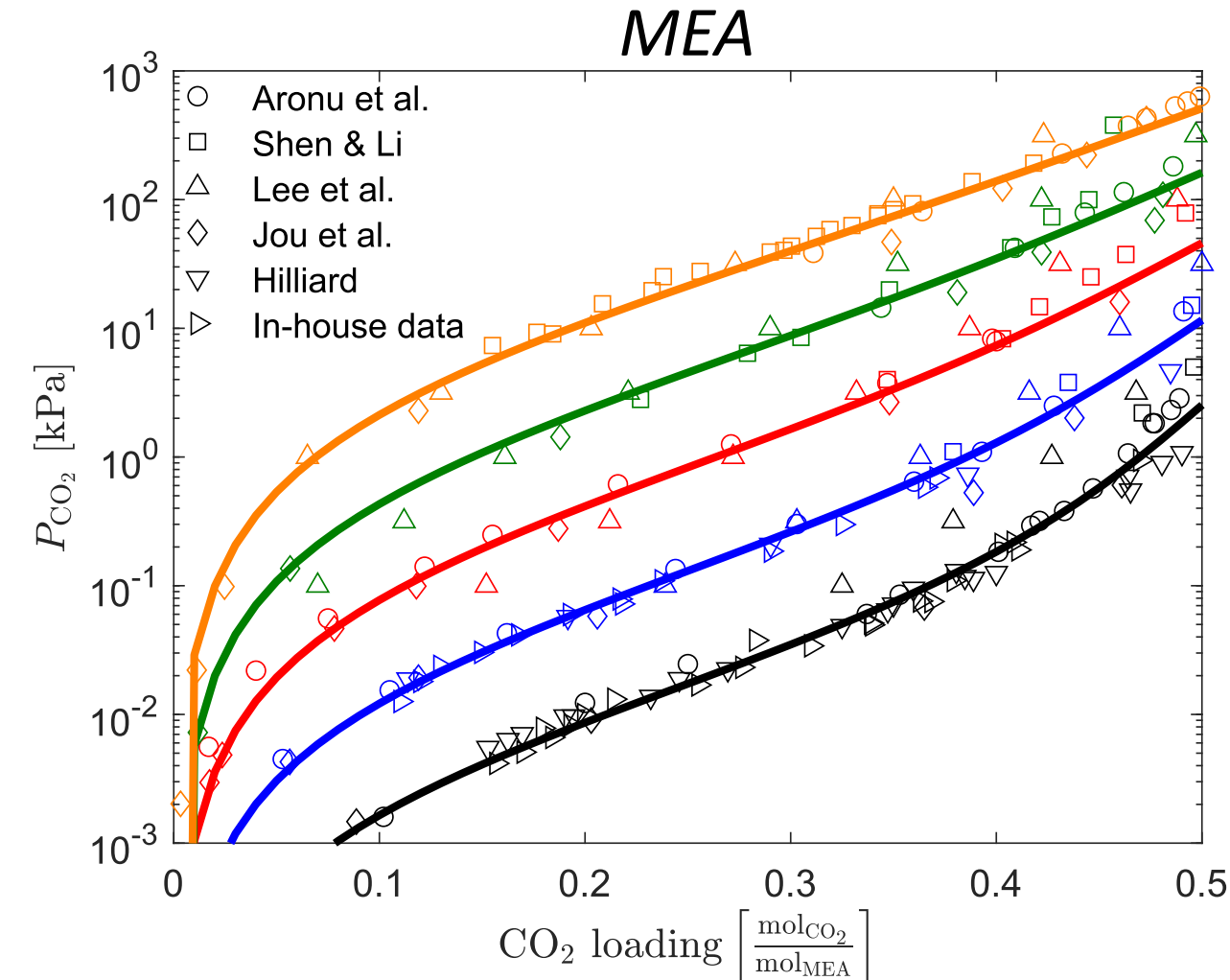
Design of this work



Scope of this work



Validation of MEA and CESAR1 models: VLE



Adapted from "Thermodynamics data for CO_2 absorption in aqueous 2-amino-2-methyl-1-propanol (AMP) and piperazine (PZ) solutions: CO_2 solubility, N_2O solubility, heat of absorption of CO_2 , pH and liquid speciation". Morlando et al. (2025)

Validation of models: pilot plant data

MEA



Experimental validation of a rigorous absorber model for CO₂ postcombustion capture

Experimental validation of a rigorous desorber model for CO₂ post-combustion capture



Tobiesen et al.
<https://doi.org/10.1002/aic.11133>

Tobiesen et al.
<https://doi.org/10.1016/j.ces.2008.02.011>



Post combustion CO₂ capture by reactive absorption: Pilot plant description and results of systematic studies with MEA

Notz et al. <https://doi.org/10.1016/j.ijggc.2011.11.004>

CESAR1



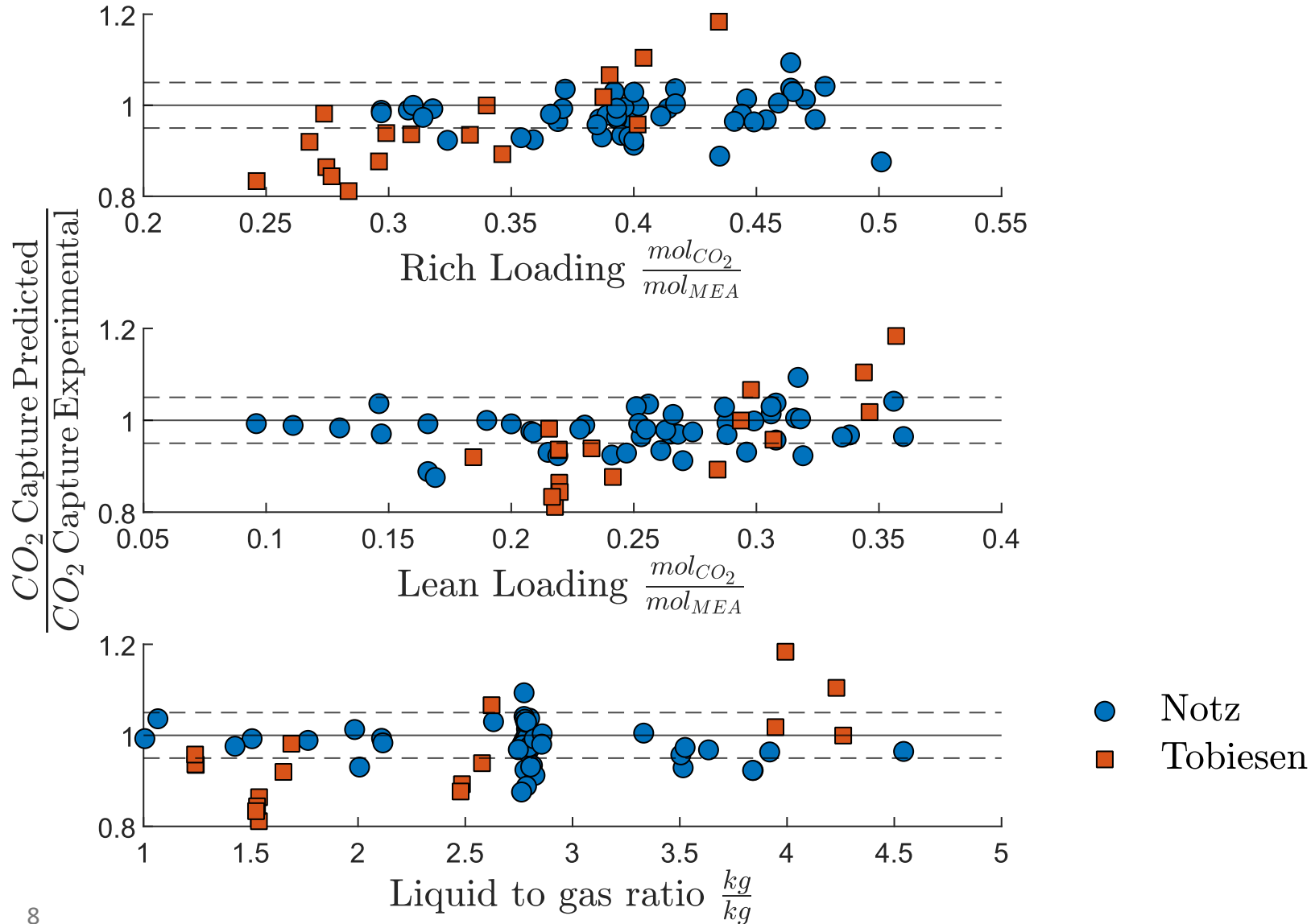
Development of process model of CESAR1 solvent system and validation with large pilot data.

Morgan et al. <http://dx.doi.org/10.2139/ssrn.4276820>

Pilot plant study of two new solvents for post-combustion carbon dioxide capture by reactive absorption and comparison to monoethanolamine.

Mangalapally et al. <https://doi.org/10.1016/j.ces.2011.06.054>

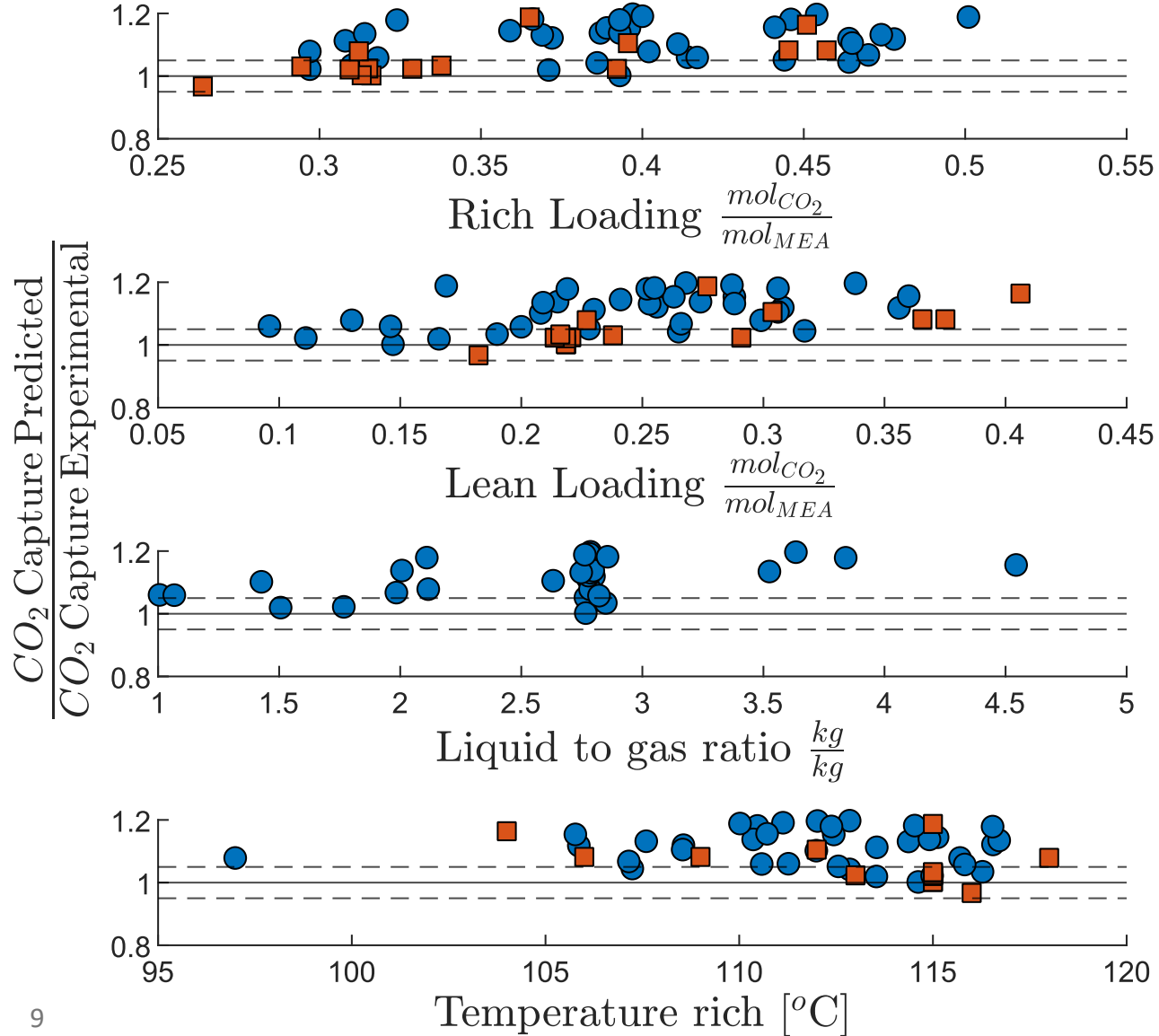
Absorber validation: MEA



$$AARD_{\alpha_{rich}} = 2.3\%$$

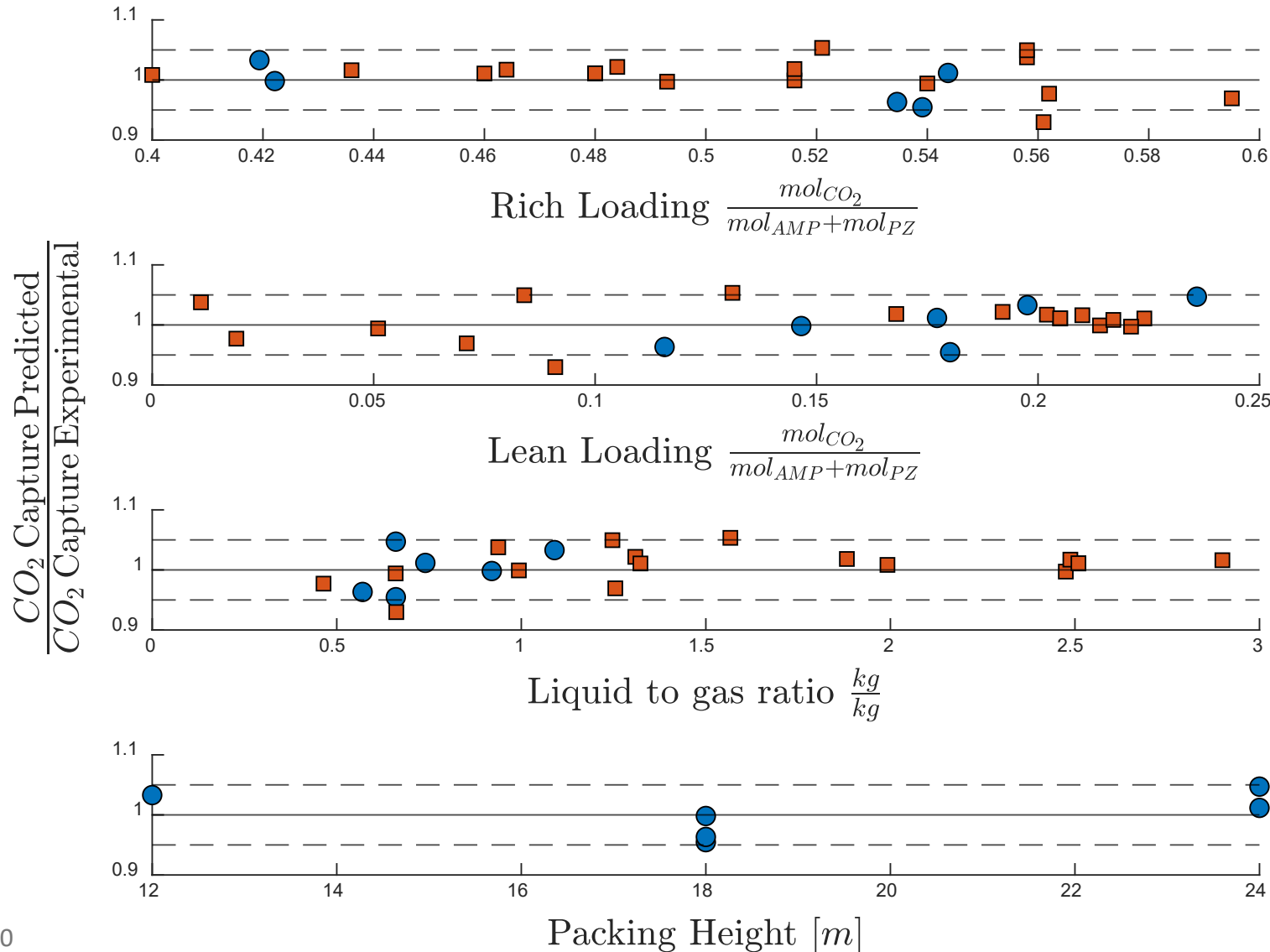
$$AARD_{\text{capture}} = 5.1\%$$

Stripper validation: MEA



$$AARD_{SRD} = 11.6\%$$

Absorber validation: CESAR1

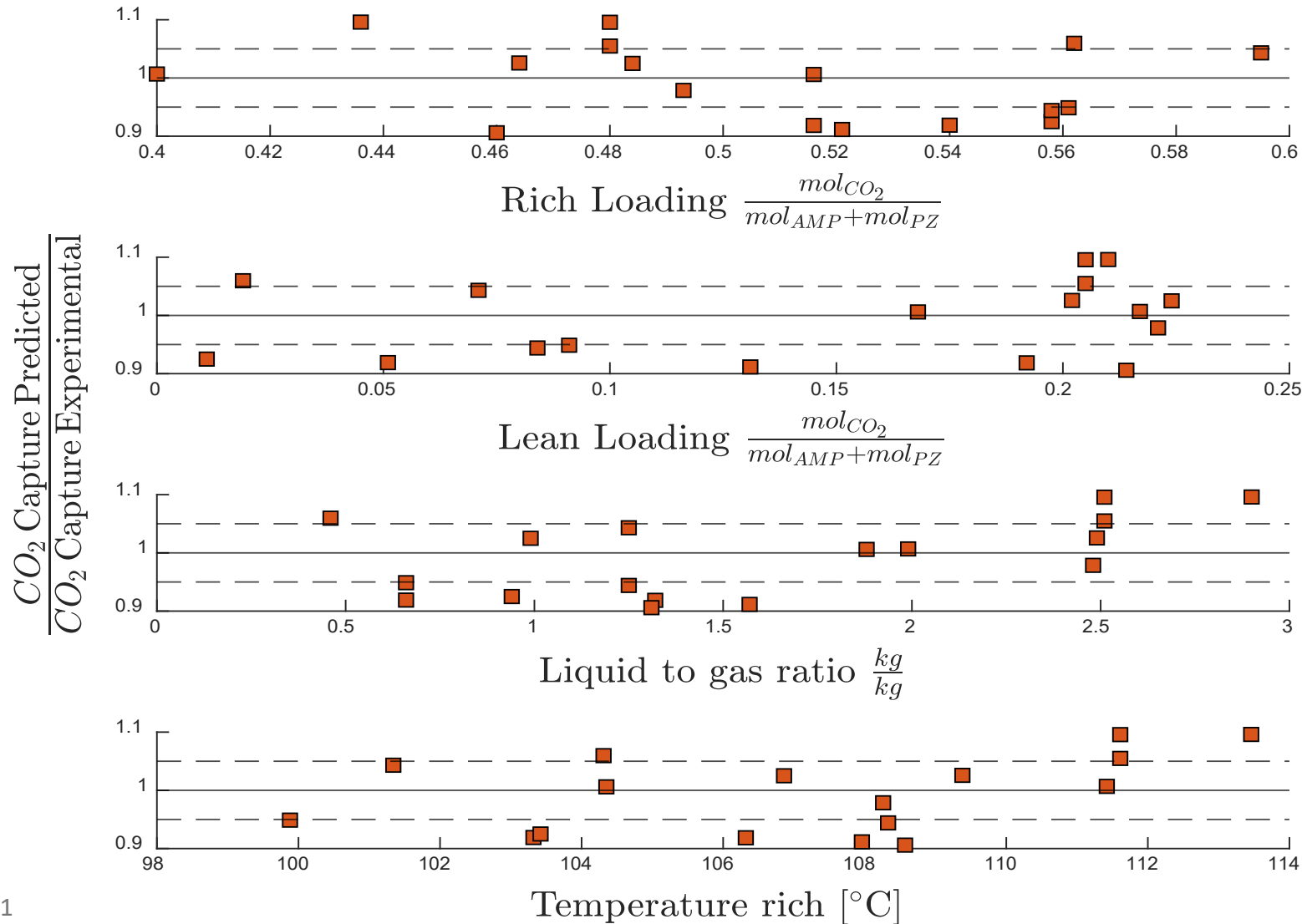


● TCM
■ Kaiserslautern

$$AARD_{\alpha_{rich}} = 2.3\%$$

$$AARD_{capture} = 2.7\%$$

Stripper validation: CESAR1



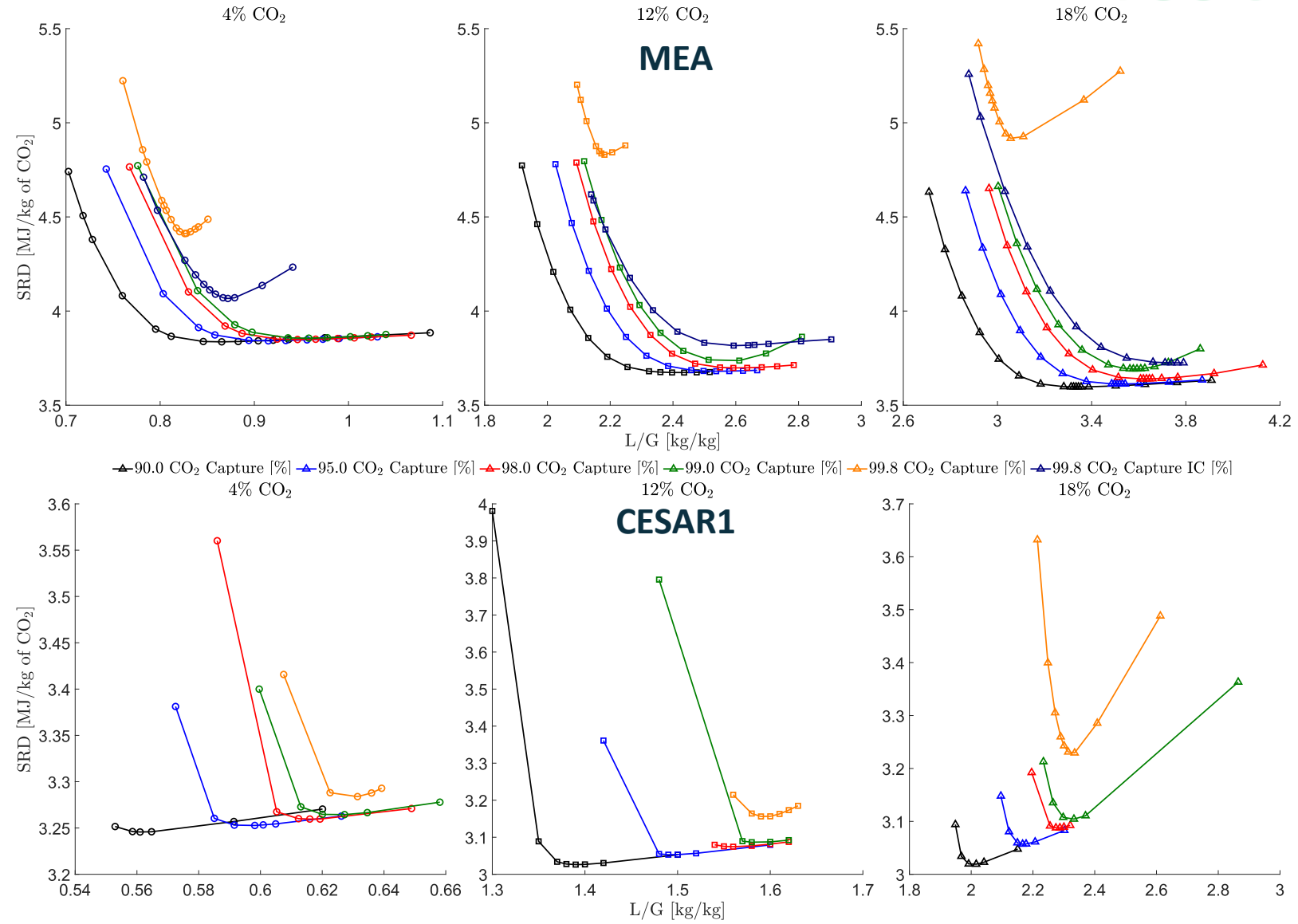
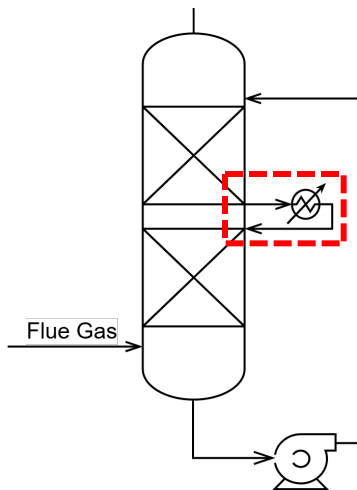
$$AARD_{SRD} = 4.8\%$$

SRD at 25m absorber: MEA & CESAR1

- SRD increases with increasing CO₂ capture



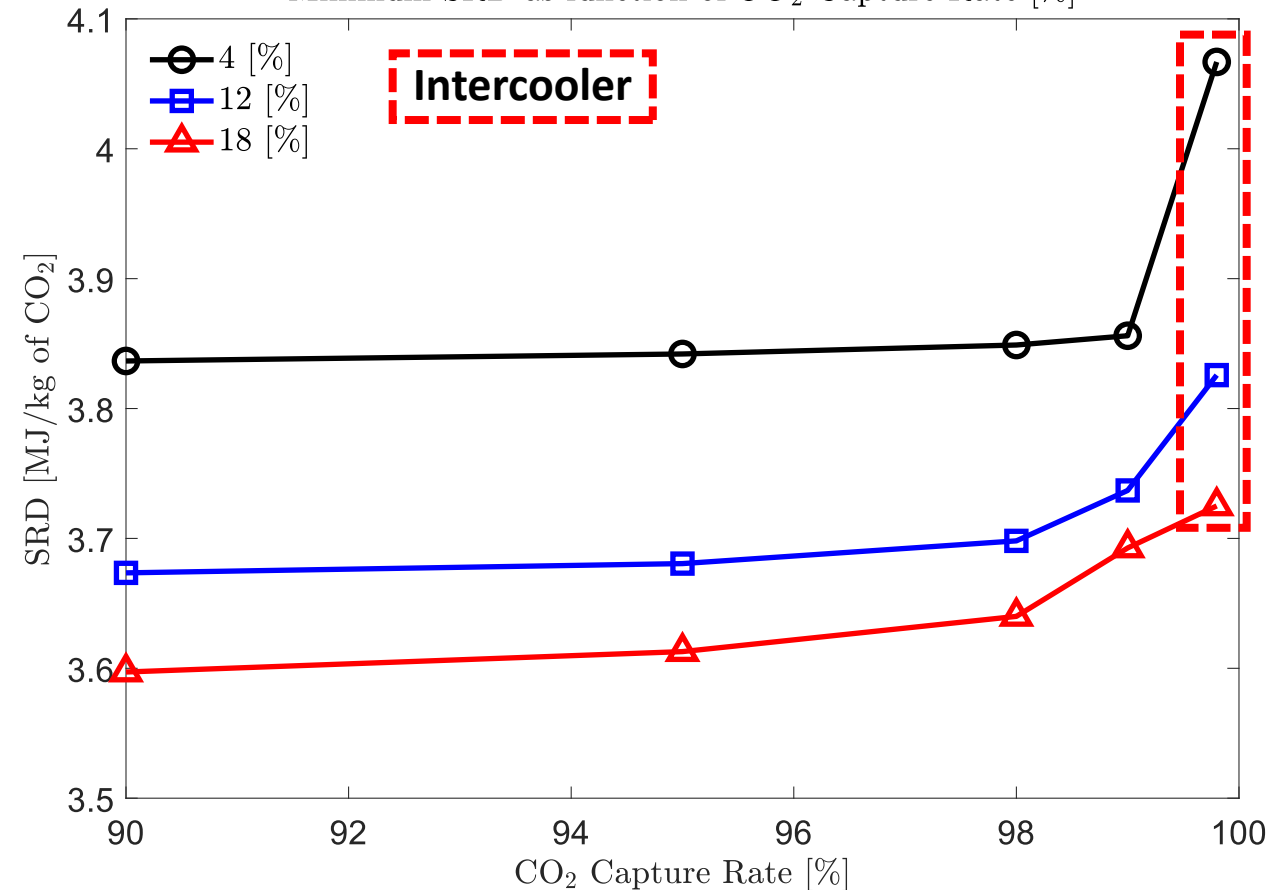
- MEA: intercooler needed to increase driving force at 99.8% CO₂ capture



CO₂ capture effect on MEA and CESAR1

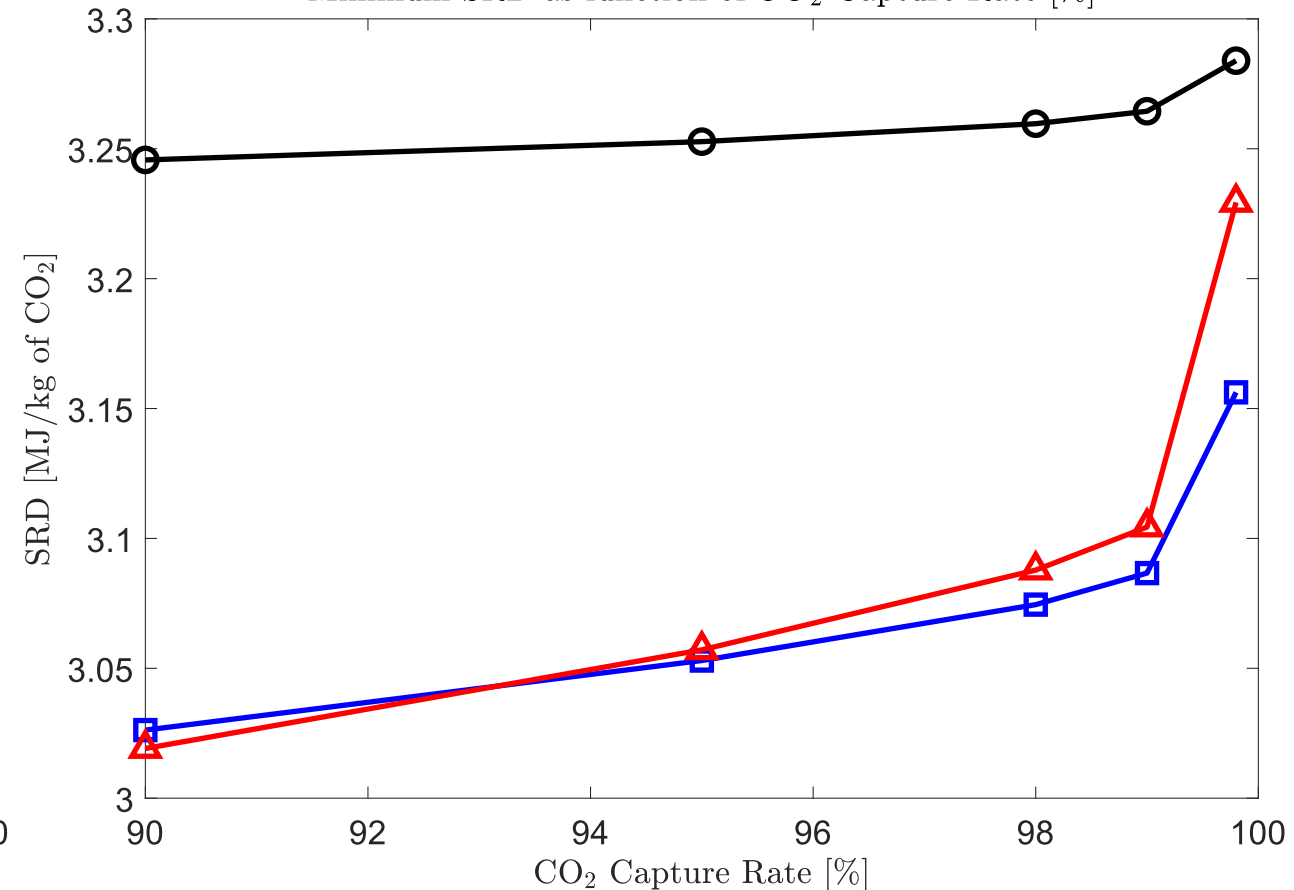
MEA

Minimum SRD as function of CO₂ Capture Rate [%]

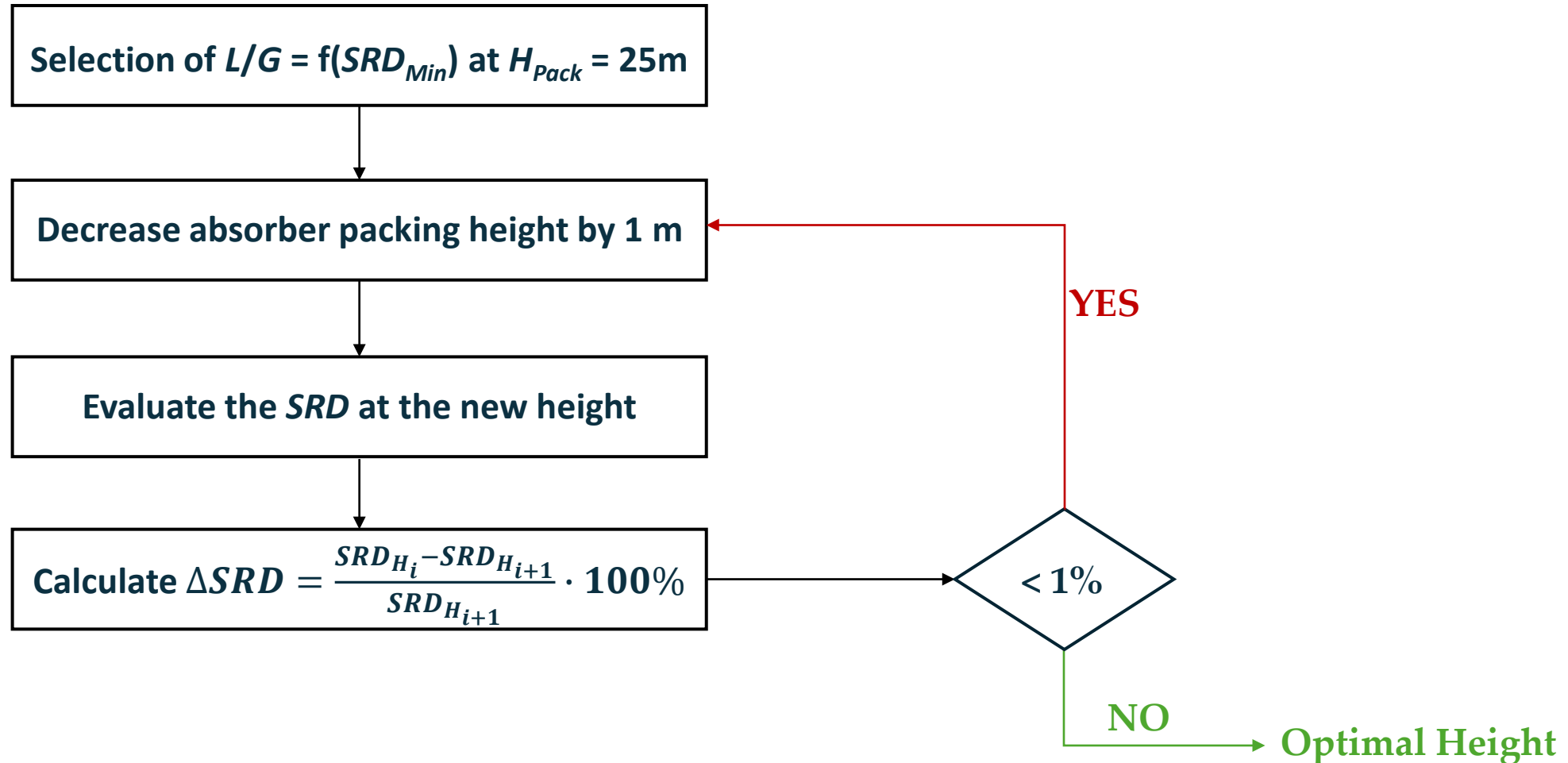


CESAR1

Minimum SRD as function of CO₂ Capture Rate [%]



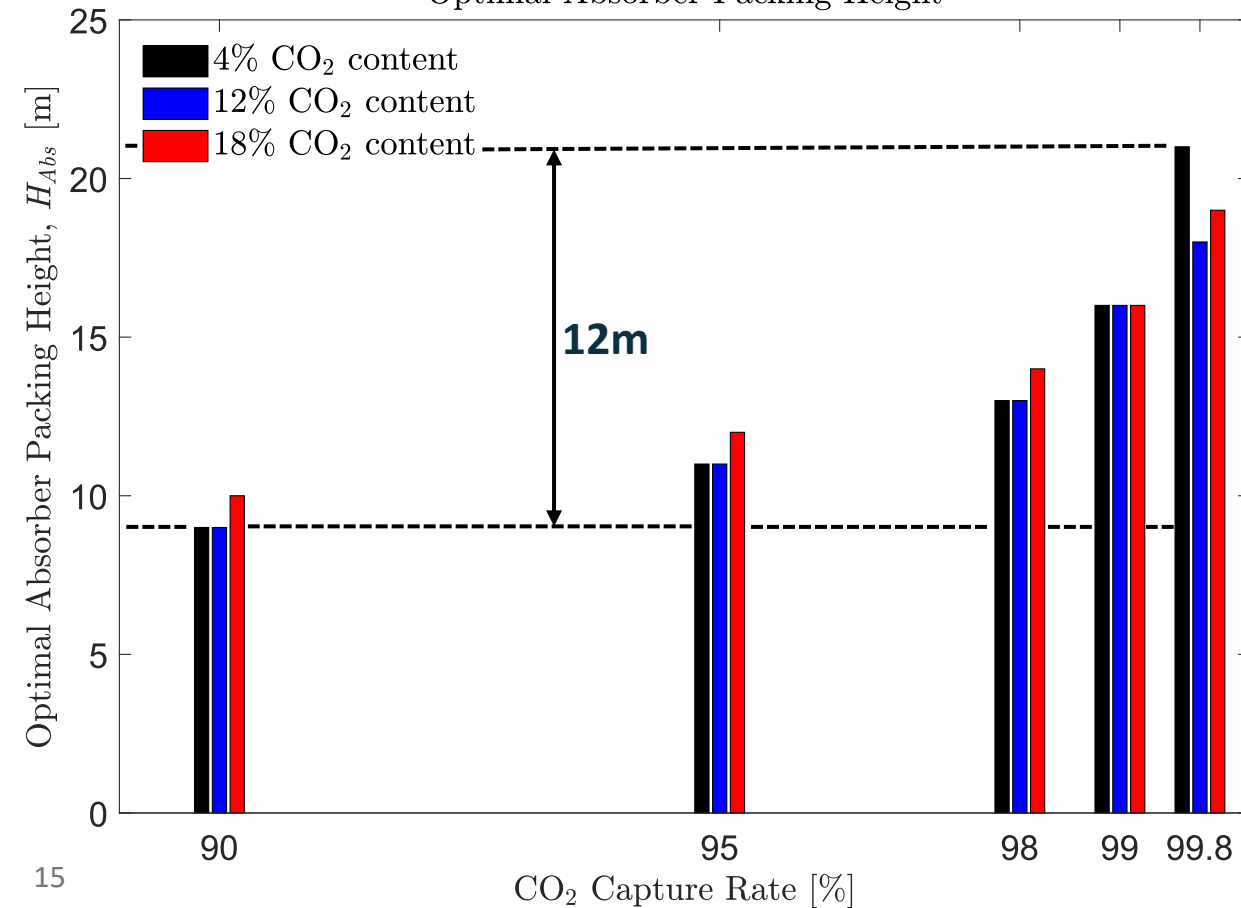
Absorber height reduction: Approach



Absorber height optimization:

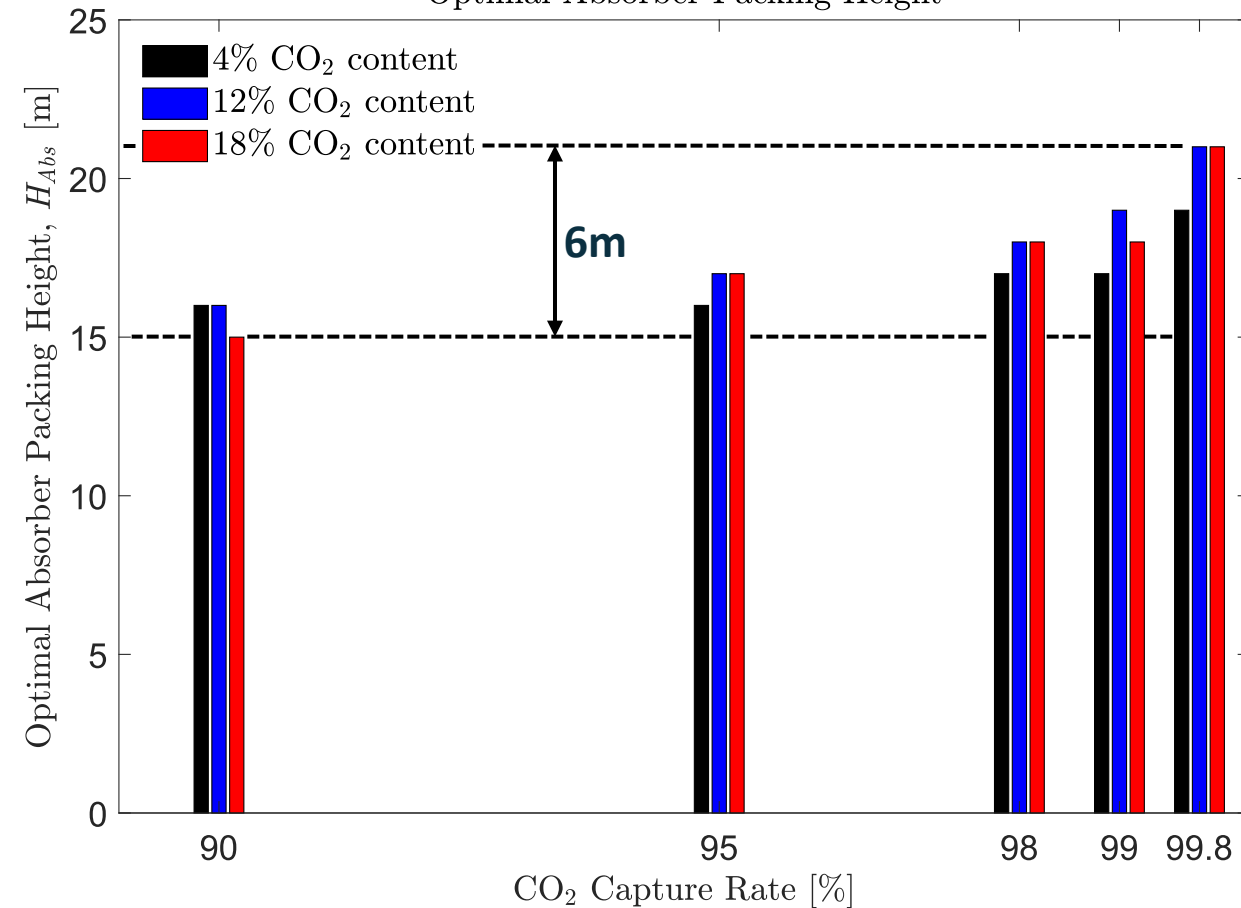
MEA

Optimal Absorber Packing Height



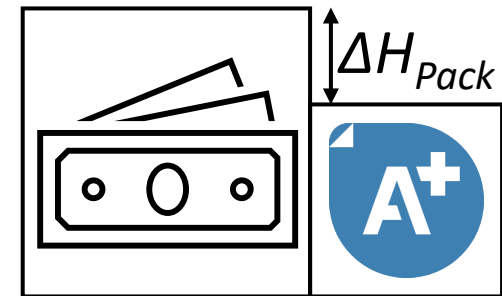
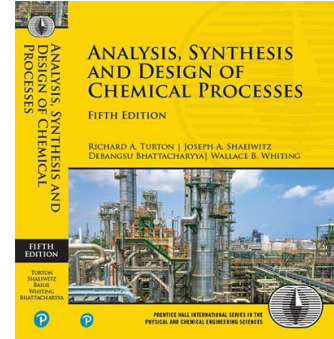
CESAR1

Optimal Absorber Packing Height



Does cost analysis agree with simulations?

- Techno-economic assessment based on the book by Turton et al.
- Analysis qualified as Class 3 (Accuracy of +40% & -25%)
- Based on techno-economic assessment for MEA:
 1. Economics suggested higher optimal absorber packing height than simulations
 2. Difference in absorber packing height becomes bigger at higher CO₂ content
- Choice of materials and cost of utilities (steam) affect optimal absorber design



Conclusions and future work

- MEA and CESAR1 can successfully operate up to 99.8% CO₂ capture
- Intercooler is needed for MEA
- CO₂ capture rates and CO₂ inlet concentration affected optimal absorber packing height
- MEA required lower absorber packing heights than CESAR1: by 6 to 2m for 90-99% CO₂ capture respectively
- Cost analysis for MEA suggested to use higher absorber packing heights than simulations

Future work will focus on techno-economic assessment for CESAR1 and comparison with MEA

Acknowledgements

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- This research has received funding from the European Union's Horizon Europe research and innovation programme under grant agreement No. 101096521 (the AURORA project).



Thank you for your attention!

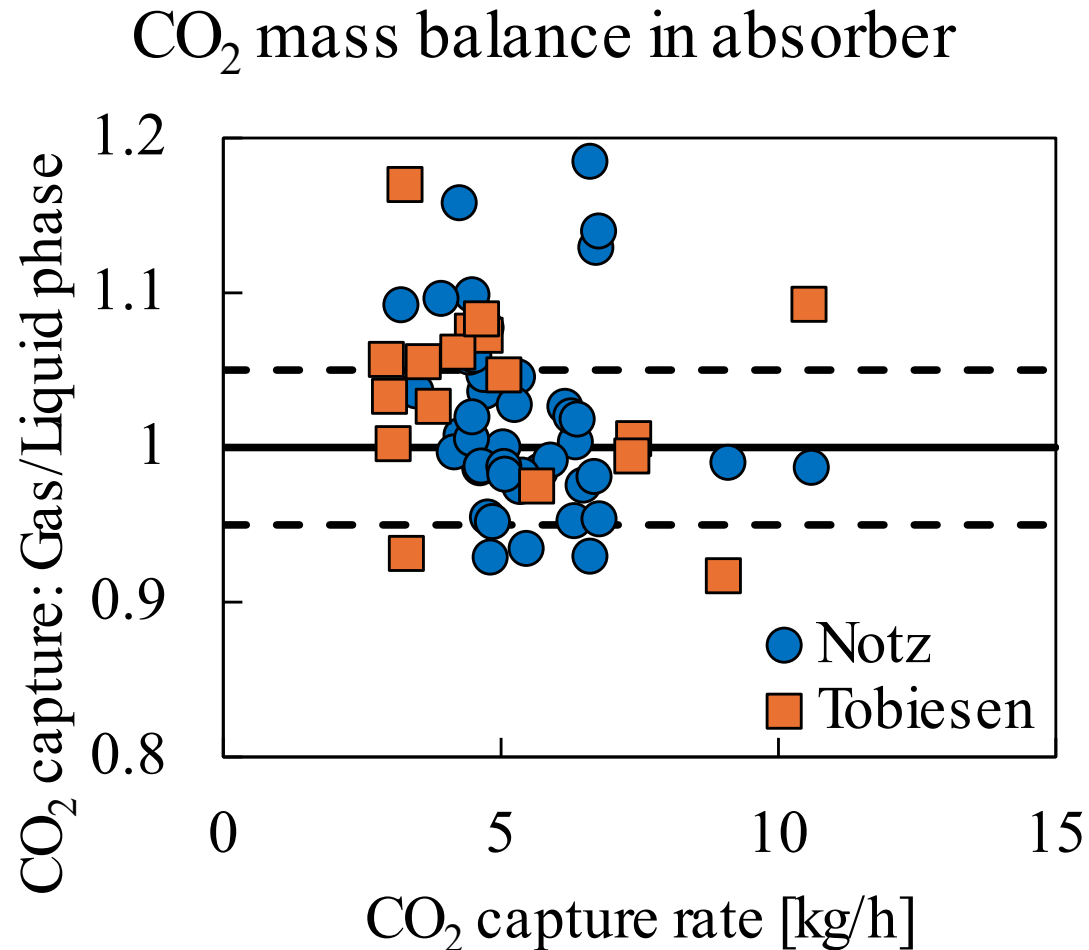
Benas Mockus | PhD student

✉ benas.mockus@ntnu.no

in [linkedin.com/in/benas-mockus-b5b38216b/](https://www.linkedin.com/in/benas-mockus-b5b38216b/)

Supplementary Slides

CO₂ mass balance in absorber pilot data: MEA



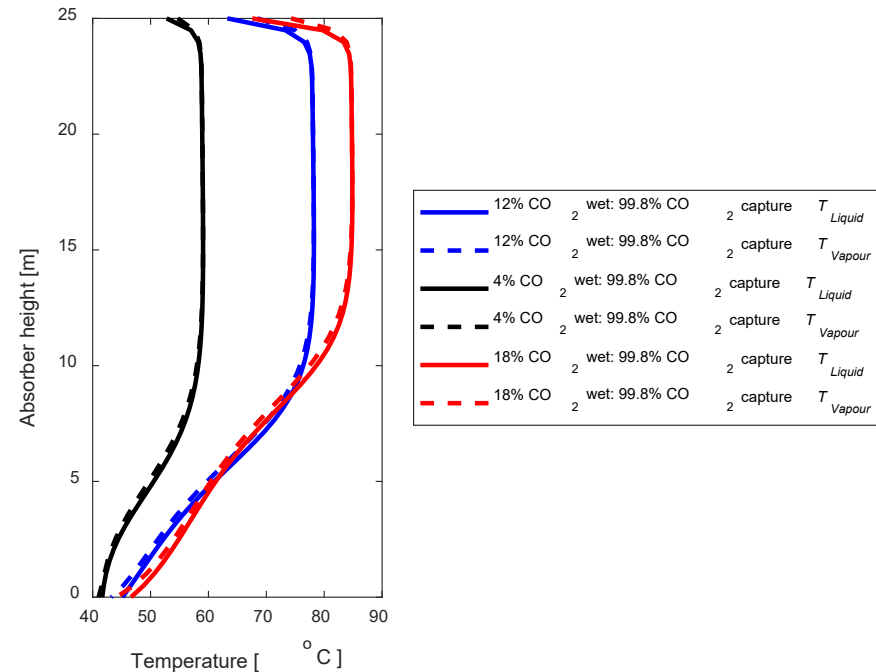
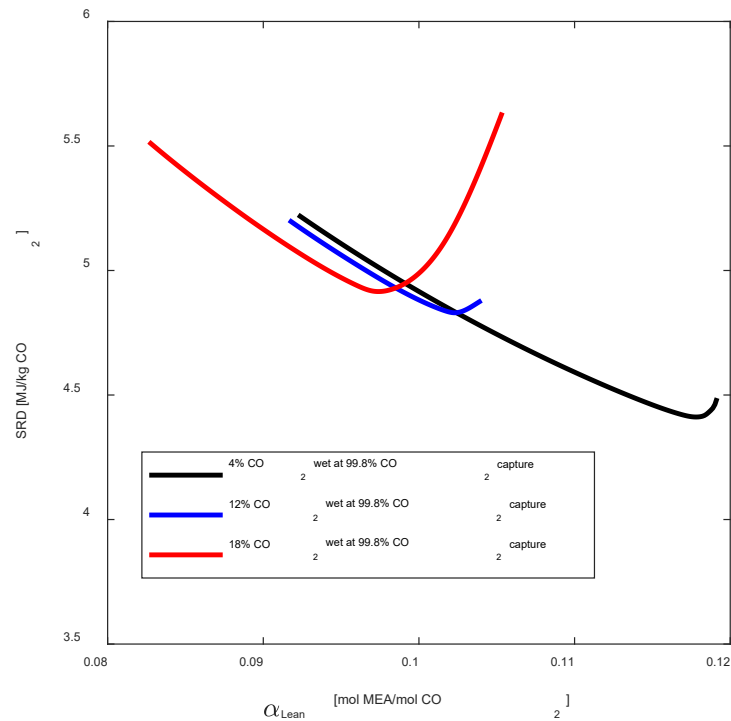
Loadings for MEA and CESAR1 at 25m

%CO ₂ wet in flue gas	MEA								
	Lean loading [mol CO ₂ / mol MEA]			Rich Loading [mol CO ₂ / mol MEA]			Cyclic capacity [mol CO ₂ / mol MEA]		
	4%	12%	18%	4%	12%	18%	4%	12%	18%
90% CO ₂ capture	0.171	0.183	0.175	0.483	0.502	0.512	0.312	0.320	0.337
95% CO ₂ capture	0.171	0.178	0.172	0.483	0.502	0.510	0.312	0.324	0.338
98% CO ₂ capture	0.171	0.173	0.168	0.482	0.500	0.507	0.311	0.327	0.339
99% CO ₂ capture	0.171	0.169	0.158	0.481	0.496	0.503	0.311	0.327	0.346
99.8% CO ₂ capture + IC	0.135	0.170	0.168	0.477	0.488	0.500	0.341	0.318	0.332

%CO ₂ wet in flue gas	CESAR1								
	Lean loading [mol CO ₂ / mol AMP + PZ]			Rich Loading [mol CO ₂ / mol AMP + PZ]			Cyclic capacity [mol CO ₂ / mol AMP + PZ]		
	4%	12%	18%	4%	12%	18%	4%	12%	18%
90% CO ₂ capture	0.057	0.055	0.055	0.573	0.653	0.654	0.516	0.598	0.599
95% CO ₂ capture	0.060	0.055	0.053	0.572	0.644	0.641	0.512	0.589	0.588
98% CO ₂ capture	0.060	0.055	0.053	0.570	0.636	0.631	0.510	0.580	0.578
99% CO ₂ capture	0.060	0.054	0.055	0.568	0.633	0.624	0.508	0.579	0.569
99.8% CO ₂ capture + IC	0.055	0.046	0.043	0.564	0.624	0.615	0.509	0.579	0.572

4%/12%/18% CO₂ wet concentration

- Temperature pinching at all CO₂ contents at 99.8% CO₂ capture
- Intercooler is needed for MEA



Partial pressures of CO₂ at the top of absorber

Results from simulation	P _{CO2} in exit gas [kPa]		
	4% CO ₂ inlet	12% CO ₂ inlet	18% CO ₂ inlet
90% CO ₂ capture	0.435	1.420	2.279
95% CO ₂ capture	0.218	0.715	1.152
98% CO ₂ capture	0.087	0.287	0.463
99% CO ₂ capture	0.044	0.143	0.231
99.8% CO ₂ capture + IC	0.009	0.029	0.046

VLE in Aspen Plus V14	P _{CO2} in VLE based on results loading [kPa]		
	4% CO ₂ inlet	12% CO ₂ inlet	18% CO ₂ inlet
90% CO ₂ capture	0.005	0.005	0.005
95% CO ₂ capture	0.005	0.005	0.005
98% CO ₂ capture	0.005	0.005	0.005
99% CO ₂ capture	0.005	0.004	0.004
99.8% CO ₂ capture + IC	0.003	0.005	0.005