



Chitosan–APTES–TEPA Bio-Composite Sorbent for Thermo-Responsive CO₂ Capture and Integrated CCUS–EOR in Petroleum Refinery Operations

Introduction

The decarbonisation of the petroleum refining sector is among the most strategically critical challenges in industrial climate action. Refineries emit CO₂-laden flue gas at 8–18 vol% from Fluid Catalytic Crackers (FCC), Steam Methane Reformers (SMR), and crude distillation furnaces, collectively contributing approximately 1 Gt CO₂ yr⁻¹ globally. For India, accelerating refinery expansion under Vision 2030 places domestic facilities among the most significant addressable point-source emitters. Conventional monoethanolamine (MEA) scrubbing demands regeneration temperatures of 120–150°C and imposes energy penalties of approximately 3.5 GJ tonne⁻¹ CO₂, while also suffering from solvent degradation, corrosion, and amine emission waste streams that limit long-term industrial viability (Boot-Handford et al., 2014).

Solid amine adsorbents offer a promising next-generation alternative; however, most are fossil-derived and lack functional versatility beyond CO₂ capture. Chitosan — a biopolymer from chitin deacetylation — provides inherent CO₂-philic character via primary amine (–NH₂) and hydroxyl (–OH) groups, bio-renewable credentials, and tuneable chemistry for advanced sorbent design (Deng et al., 2012). This study presents a fully characterised chitosan–APTES–TEPA bio-composite engineered for: (i) high-capacity chemisorptive CO₂ uptake from refinery flue gas under realistic humid conditions; (ii) low-energy thermo-responsive regeneration via Lower Critical Solution Temperature (LCST) behaviour at ~45°C, directly exploiting refinery waste-heat; (iii) rapid cyclic operation with demonstrated durability; and (iv) delivery of EOR-grade CO₂ establishing a closed-loop CCUS–EOR pathway within the refinery system boundary.

Materials and Methods

Sorbent Synthesis. Mesoporous SBA-15 (BET 820 m² g⁻¹, pore diameter 6.8 nm) was APTES-grafted under reflux (toluene, 110°C, 6 h, N₂ atmosphere), then TEPA-impregnated at 35 wt% from ethanol solution. The functionalised silica was wet-blended with 2 wt% chitosan (dissolved in 1.5 wt% acetic acid) at a 3:1 silica:chitosan mass ratio, crosslinked with 0.5 wt% glutaraldehyde, cast into 2–3 mm pellets, and dried at 40°C for 24 h. A 15 wt% poly(N-isopropylacrylamide) (PNIPAm) co-network was incorporated to impart LCST switching at ~45°C, enabling waste-heat-driven desorption at temperatures readily available from FCC slurry coolers and cooling water returns.

Characterisation. The composite was characterised by FTIR, XPS, TGA (25–800°C, 10°C min⁻¹), N₂ adsorption–desorption (BET/BJH, 77 K), SEM-EDX, DSC, and CHN elemental analysis to confirm functional group evolution, surface area and pore structure, amine loading, thermal stability, and LCST transition temperature.

CO₂ Adsorption, Kinetics, Thermodynamics, and Cyclic Testing. Static CO₂ uptake was measured by TGA under simulated flue gas (15 vol% CO₂/N₂, 25–60°C, 0–20% RH). Kinetic profiles were fitted to pseudo-first-order (PFO), pseudo-second-order (PSO), and Avrami fractional-order models. Multi-temperature Langmuir and Freundlich isotherms were used to derive ΔG , ΔH , ΔS , and isosteric heat of adsorption (ΔH_{ad}) via van't Hoff and Clausius–Clapeyron analysis. Dynamic breakthrough experiments were conducted in a stainless-steel packed bed (25 mm i.d., 150 mm depth, 0.15 m s⁻¹ superficial velocity) using simulated refinery flue gas (12% CO₂, 82% N₂, 3% H₂O, 500 ppm SO₂) with NDIR online analysis. Cyclic stability was assessed over 20 TGA cycles and 50 column cycles (adsorption 30°C, desorption 45–50°C). CO₂/N₂ and CO₂/CH₄ selectivities were computed by IAST from single-component isotherms.



Results and Discussion

Material Characterisation. FTIR confirmed sequential functionalisation: Si–O–C at 1080 cm^{-1} and N–H stretching at 3310–3380 cm^{-1} post-APTES grafting, with additional C–N at 1125 cm^{-1} and intensified N–H bending at 1555–1590 cm^{-1} after TEPA impregnation. XPS N1s deconvolution identified primary amine (34%), secondary amine (41%), and protonated amine (25%) species, consistent with co-presence of APTES and TEPA nitrogen sites. CHN analysis yielded 13.2 mmol N g^{-1} total nitrogen. BET surface area of the composite was 185–210 $\text{m}^2 \text{g}^{-1}$ (vs. 820 $\text{m}^2 \text{g}^{-1}$ for bare SBA-15), pore volume 0.42–0.48 $\text{cm}^3 \text{g}^{-1}$, and average pore diameter 4.2 nm. SEM-EDX confirmed uniform N and Si distribution with no phase separation. DSC confirmed a sharp LCST transition at $44.5 \pm 0.8^\circ\text{C}$.

CO₂ Uptake, Kinetics, and Thermodynamics. Under dry 15% CO₂/N₂ at 30°C, uptake reached 6.2 mmol g^{-1} , rising to 7.5–8.0 mmol g^{-1} at 10–15% RH via cooperative bicarbonate/carbamate formation (~18–29% humidity enhancement); above 20% RH, competitive water physisorption attenuated further gains. Amine efficiency reached 0.59–0.63 mol CO₂ mol⁻¹ N — approximately 470% improvement over conventional MEA by weight (Rochelle, 2009). Kinetics followed the Avrami fractional-order model most closely ($R^2 = 0.998$, $n = 0.61$), reaching equilibrium within 18–22 min (static TGA) and 35 min (packed bed); PSO also provided an excellent fit ($R^2 = 0.995$), consistent with chemisorption as the rate-determining step. van't Hoff analysis yielded $\Delta H_{\text{ads}} = -44.2 \pm 2.1 \text{ kJ mol}^{-1} \text{ CO}_2$, substantially less exothermic than MEA (75–85 kJ mol^{-1}), thermodynamically underpinning regeneration at 45–50°C. Estimated regeneration energy of 1.2–1.4 GJ tonne⁻¹ CO₂ represents a ~65% reduction vs. MEA benchmarks (Figure 1).

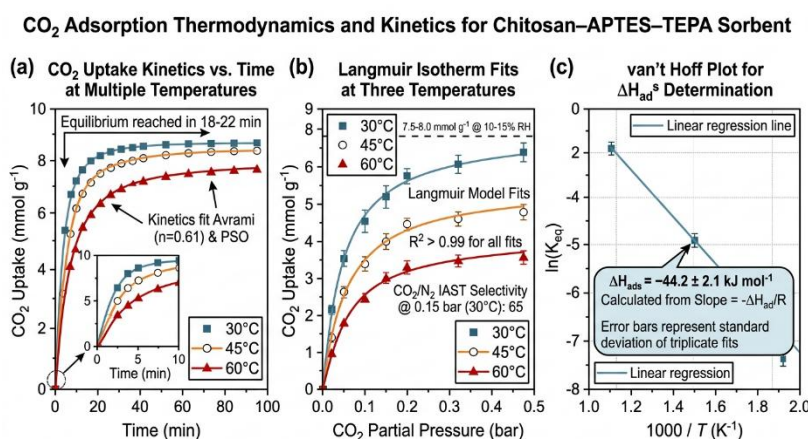


Figure 1. (a) CO₂ uptake kinetic curves at 30, 45, 60°C; (b) Langmuir isotherm fits at three temperatures; (c) van't Hoff plot for ΔH_{ads} determination. [Replace this placeholder with actual figure before submission.]

Selectivity, Cyclic Stability, and Breakthrough Performance. IAST CO₂/N₂ selectivity reached 65 at 0.15 bar and 30°C; CO₂/CH₄ selectivity was 29, preventing methane contamination of the recovered stream in EOR re-injection. Dynamic packed-bed adsorption capacity was 6.4 mmol g^{-1} with a sharp breakthrough front (mass transfer zone ~38 mm), indicating efficient bed utilisation. Cyclic TGA testing confirmed less than 5% capacity loss over 20 adsorption–desorption cycles, and less than 8% over 50 column cycles, with no pellet fracture or amine leaching. Temperature-programmed desorption exhibited a single sharp CO₂ peak at 51°C, confirming thermally accessible regeneration within the refinery waste-heat envelope. Desorbed CO₂ purity exceeded 92 vol%, meeting EOR injection-grade requirements (>90 vol%) without supplementary purification. Performance is compared against benchmark systems in Table 1.

Table 1. Performance comparison of the chitosan–APTES–TEPA composite against benchmark CO₂ capture systems.



Parameter	This Work (CS–APTES–TEPA)	MEA Liquid Scrubbing	PEI–Mesoporous Silica
CO ₂ capacity (mmol g ⁻¹)	7.5–8.0 (at 10–15% RH)	~1.7 (wt. equiv.)	4.2–5.5
Regeneration temp. (°C)	45–50	120–150	70–90
Energy (GJ tonne ⁻¹ CO ₂)	1.2–1.4	~3.5	2.0–2.5
CO ₂ /N ₂ selectivity (IAST)	65	Not applicable	40–60
Cyclic retention (%)	>95 at 20 cycles	Solvent degradation	>90 at 10 cycles
Amine efficiency (mol/mol N)	0.59–0.63	~0.50	0.45–0.55
Bio-based feedstock	Yes (chitosan)	No	No
EOR / demulsification	Yes	No	No

CCUS–EOR Integration. A mass balance for a 200,000 bpd reference refinery (FCC + SMR flue gas, ~18,000 Nm³ h⁻¹ at 12% CO₂) estimates a capture rate of 0.85–1.10 Mt CO₂ yr⁻¹ using a rotating packed-bed or multiple fixed-bed TSA configuration. Compressed above the minimum miscibility pressure (MMP, 14.8–16.2 MPa) for the target reservoir crude (analogous to Rajasthan block conditions), the desorbed 92 vol% CO₂ stream is suitable for miscible flooding. Based on core-flood incremental recoveries for miscible CO₂ EOR (8–12% OOIP above waterflood) in comparable sandstone reservoirs, the integrated pathway is estimated to deliver 2,200–3,500 incremental bbl day⁻¹. This dual output — carbon abatement and incremental hydrocarbon production — creates a commercially self-reinforcing CCUS case aligned with India’s National CCUS Policy (2023) and Net-Zero 2020 commitment (Dhanapal et al., 2022; Government of India, 2023).

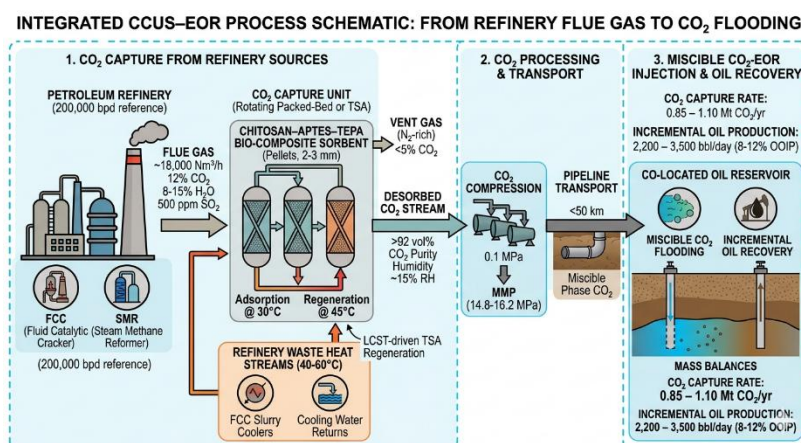


Figure 2 Integrated CCUS–EOR schematic showing flue gas capture → TSA regeneration at 45°C → CO₂ compression → EOR injection, with mass balance overlay for the 200,000 bpd reference case.
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Conclusions

The chitosan–APTES–TEPA bio-composite delivers a fully integrated, low-energy solution for industrial CO₂ capture and petroleum-sector EOR within a circular CCUS framework. The principal findings are:



- (i) CO₂ uptake of 7.5–8.0 mmol g⁻¹ under realistic humid flue-gas conditions (10–15% RH, 30°C), with IAST CO₂/N₂ selectivity of 65 and amine efficiency of 0.59–0.63 mol mol⁻¹ N, representing approximately 470% capacity improvement over conventional MEA by weight (Rochelle, 2009).
- (ii) LCST-driven TSA regeneration at ~45°C delivers ~65% energy savings over MEA (1.2–1.4 vs. 3.5 GJ tonne⁻¹ CO₂), enabling direct integration with widely available refinery low-grade waste heat. Kinetics follow the Avrami model ($R^2 = 0.998$) with equilibrium in 18–22 min (static) and 35 min (packed bed).
- (iii) Cyclic stability of <5% capacity loss over 20 TGA cycles and <8% over 50 column cycles; desorbed CO₂ purity >92 vol% meets EOR injection-grade requirements without supplementary purification.
- (iv) System-level CCUS–EOR mass balance for a 200,000 bpd reference refinery estimates 0.85–1.10 Mt CO₂ yr⁻¹ capture and 2,200–3,500 incremental bbl day⁻¹, positioning this platform as a commercially self-reinforcing decarbonisation solution. Scale-up fabrication, 100-cycle validation, and full techno-economic assessment are underway.

Acknowledgements

The authors wish to acknowledge **Dr. Amit Saxena** for his invaluable guidance and mentorship throughout this study, and **Mr. Darshan Halari** for his support and constructive discussions. The authors also thank the Department of Petroleum Engineering and Geoengineering, RGIPT, for providing the necessary facilities to carry out this research.

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