ABSTRACT

Ensuring safety for the aircraft and spacecraft is utmost, especially in detecting damage or defects before they compromise structural integrity during operation. Thermography emerges as a cost-effective, reliable, and practical method for monitoring structural health as it can provide damage or defect related information within a matter of time. This research aims to explore the efficacy of active flash thermography in assessing impact damage in structural components. The experiments simulated composite plates of quasi-isotropic material properties and analyzed the nodal temperature variation at different delamination locations. Additionally, thermography experiments were conducted on different composite plates, including a demonstrator used in NASA's "Civil Vertical Lift Vehicles" project, to assess impact damage. Furthermore, damage progression in tensile specimens was evaluated under increasing loads, with all areas measured using a pixel counting method. The obtained results were extensively analyzed and compared with Ultrasonic C-scan.

BACKGROUND



 \succ Due to the introduction of Thermographic signal reconstruction (TSR) data processing, thermography has become the most established NDE technique like ultrasonics, X-rays, eddy currents, etc.

 $\geq \log_{10}(\Delta T) = a_0 + a_1 \log_{10}(t) + a_2 [\log_{10}(t)]^2 + a_2 [\log$ $\dots + a_n [log_{10}(t)]^n$

OBJECTIVE

Depth and area measurement of impact damage in composite plates

- > Processing of numerical and experimental data
- Generation of T-t plots
- Generation of impact damage related images with noise reduction.
- Setting up a calibration profile.
- Comparison of data with Ultrasonic C-scan.





Assessing Impact Damage in Composite Aircraft Structures using Thermographic NDE

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METHODOLOGY



Numerical Analysis

Experimental Analysis



 \blacktriangleright Material : Quasi-isotropic: 48 ply with lay-up sequence [45/0/-45/90]_{2s} and thickness of 2.286 mm > Instrument: Thermoscope II equipped with IR camera (FLIR SC 5000) and two xenon lamps for pulse heating

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TS				
		Vergeseture 2536-02 2537-02 2536-02 2536-02 2536-02 2312-02 2356-02 2356-02 2356-02<	Temperature 9006-03 9706-03 8506-03 8506-03 7706-03 7706-03 7706-03 8506-03	Temperature 5:00+43 4:500+43 4
	Time: 0.02 s	Time: 0.11 + 5	Time of the formation o	744 S
ation at	Thermographic profiles of delamination's at different times			
.689 [D] 1.70 .689 [D] 1.55 1.40 1.25 1.10 0.95	Front side		Rear side	
0.547 [C]	No load (front)	0.1072 <i>in</i> ²	No load (rear)	0.0541 <i>in</i> ²
0.50 0.35				
• 100	5000 Ib (front)	0.1079 <i>in</i> ²	5000 Ib (rear)	0.0599 <i>in</i> ²
50				
		C.		
graphic of impact	10000 Ib (front)	0.1137 in ²	10000 Ib (rear)	0.1072 in ²
graphic of impact ge on	10000 Ib (front) Damage	0.1137 in ²	10000 Ib (rear) sile specimen as	0.1072 <i>in</i> ²
graphic of impact ge on strator	10000 Ib (front) Damage	0.1137 in ² growth in ten	10000 Ib (rear) sile specimen as	0.1072 <i>in</i> ² s load is

CALCULATIONS

 \succ Using Break time t^{*} = 4.511 sec (thickness L=0.002184 m)

 $\geq \alpha_z = 3.37 \text{e} - 7 \text{ m}^2/\text{sec}$

> $t^* = 0.1915$ sec (deviation of temperature curve related to 'B' from sound zone temperature curve 'A')

- Depth Calculation $L = \sqrt{(t^* \pi \alpha_z)}$
- > Depth of location 'B' = 0.450 m

CONCLUSIONS

 \succ T-t plots are useful for setting the threshold value. \succ Calibration profile (established with the R^2 value of 0.976) determined the depth values close to the those measured by temperature variation curve. ► Damage assessment using thermography is effective and timesaving in comparison with Ultrasonic C-scan.

Future Work

► Determination of smaller defect or damage beneath larger damage using heat conductive material.

References

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Acknowledgement

I would like to thank Dr. Mannur Sundaresan for helping, guiding and supporting me in this research. I would also like to thanks Manoj Rijal and David Amoateng Mensah for their help and guidance in this research.