

Enhancing Pavement Design Life

Back to Basics

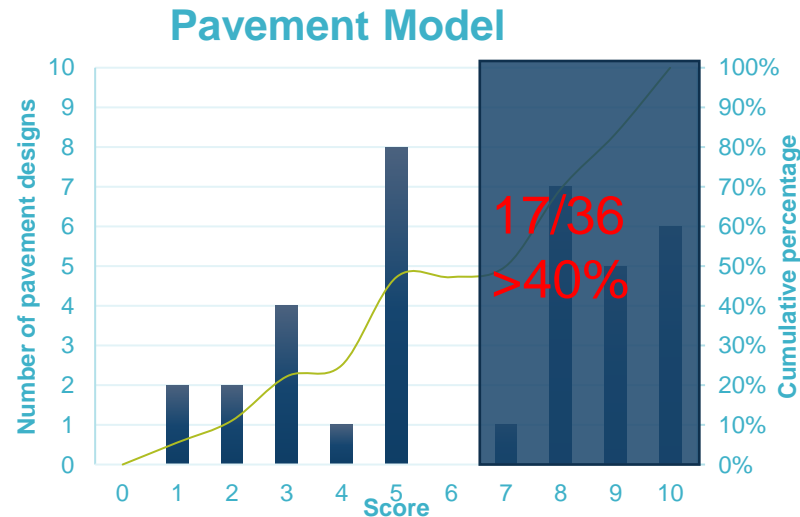
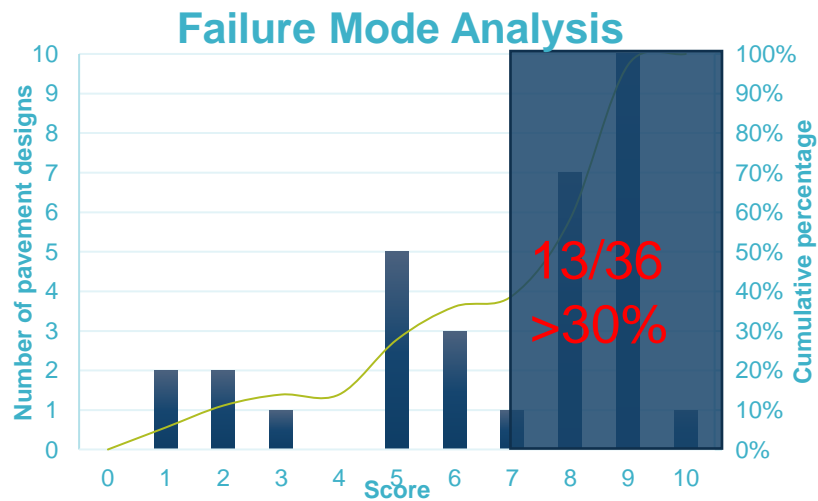
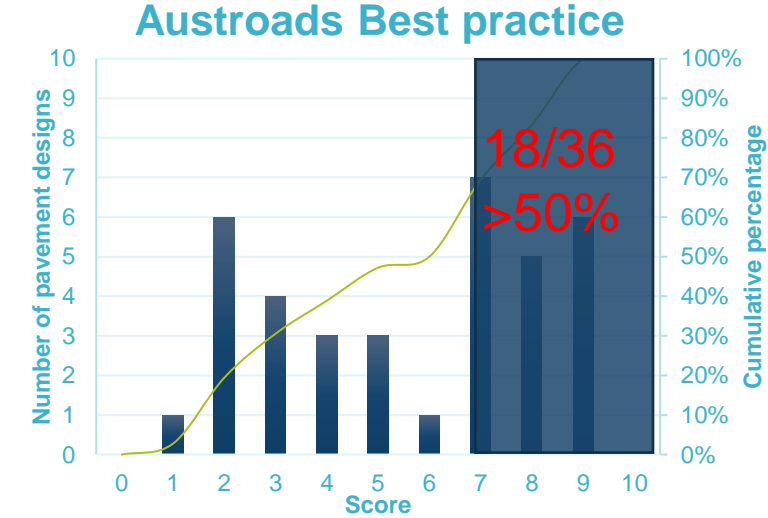
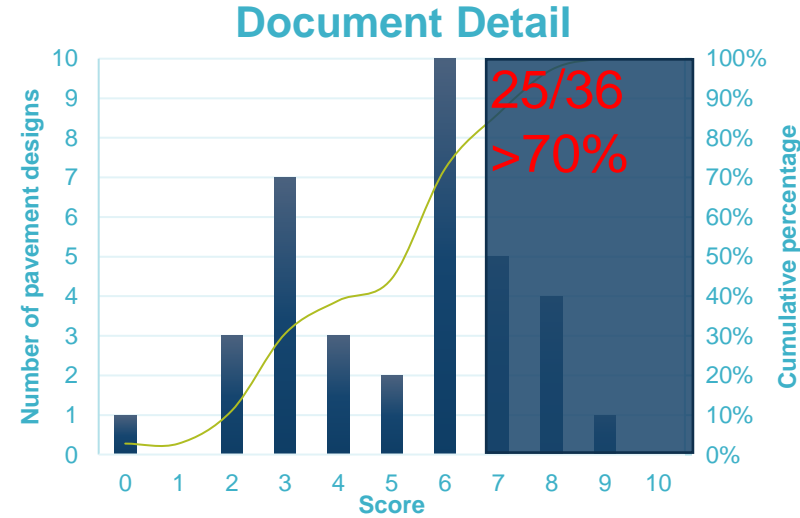
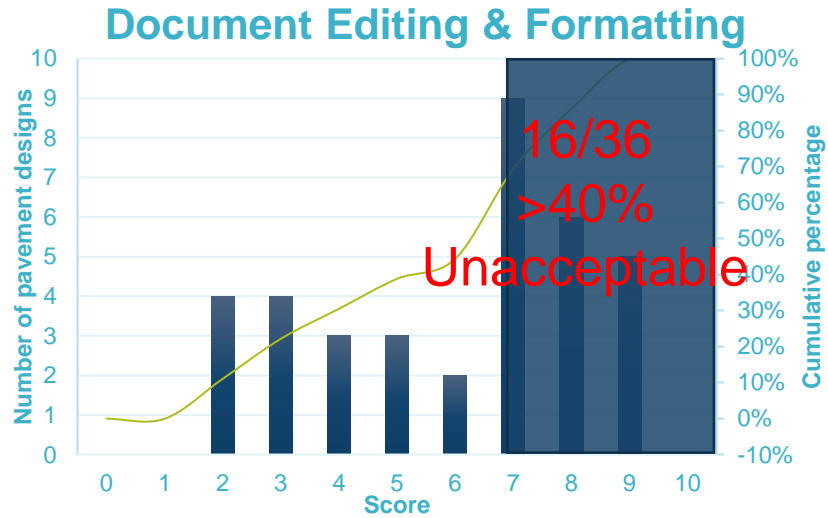
Rob Damhuis

Principle Pavement Engineer
Waka Kotahi - NZTA

Life of pavements....



Analysis of NOC pavement designs across NZ



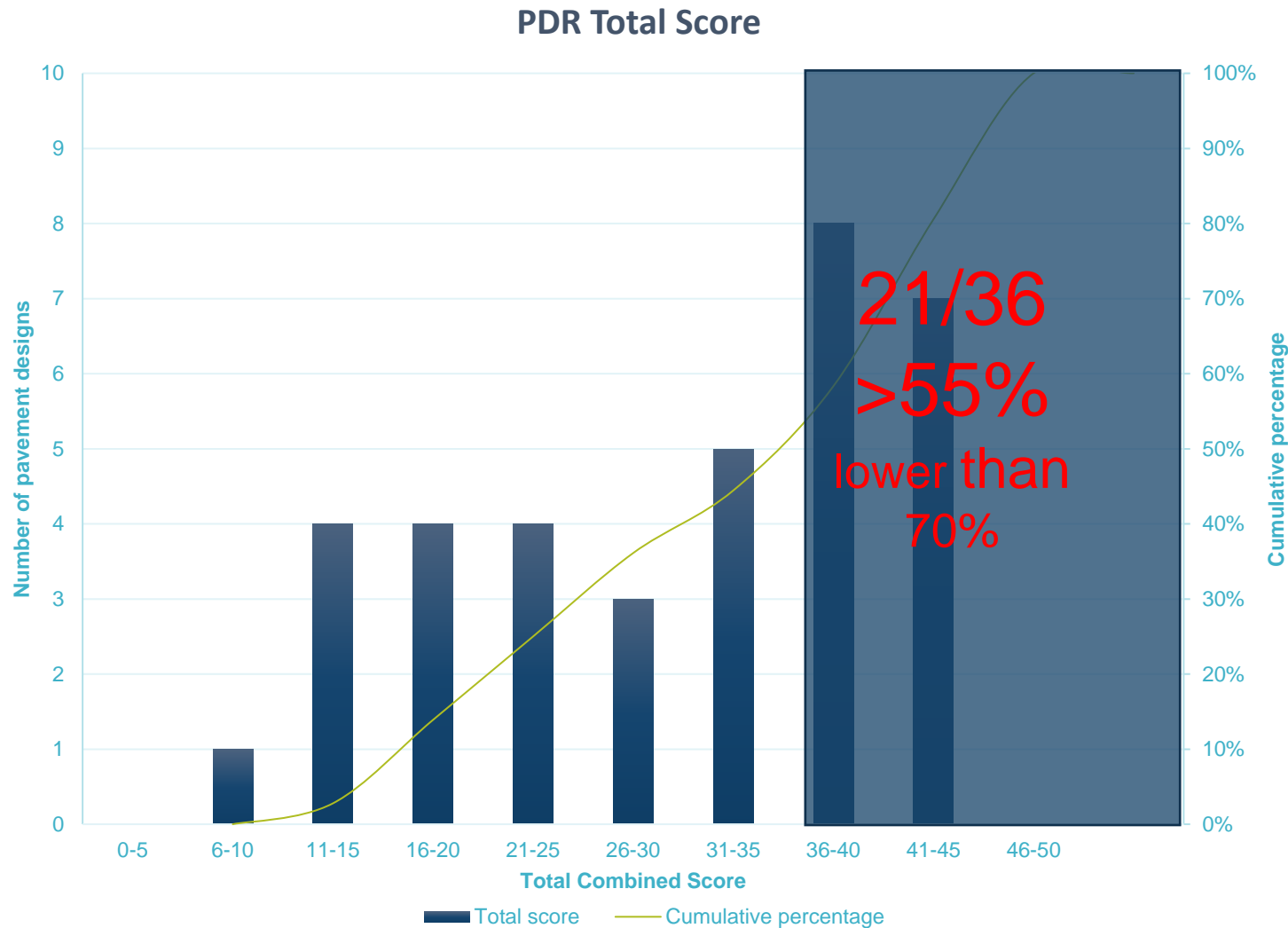
Study Representation

- Small sample size (36 PDRs)
- Most NOCs but all NOC contractors.
- Most Consultants
- Unbound, FBS, Cement and SAC

Reviews

- 36 x PDRs reviewed by Reviewer
- 10 x PDR reviewed by Moderator
- 5 x PDRs compared by 3 Principle Pavement Engineers

Analysis of NOC pavement designs across NZ



Significant portion of the PDRs have *not* carried out in accordance with NZ / Austroads good practice.



Pavement Life

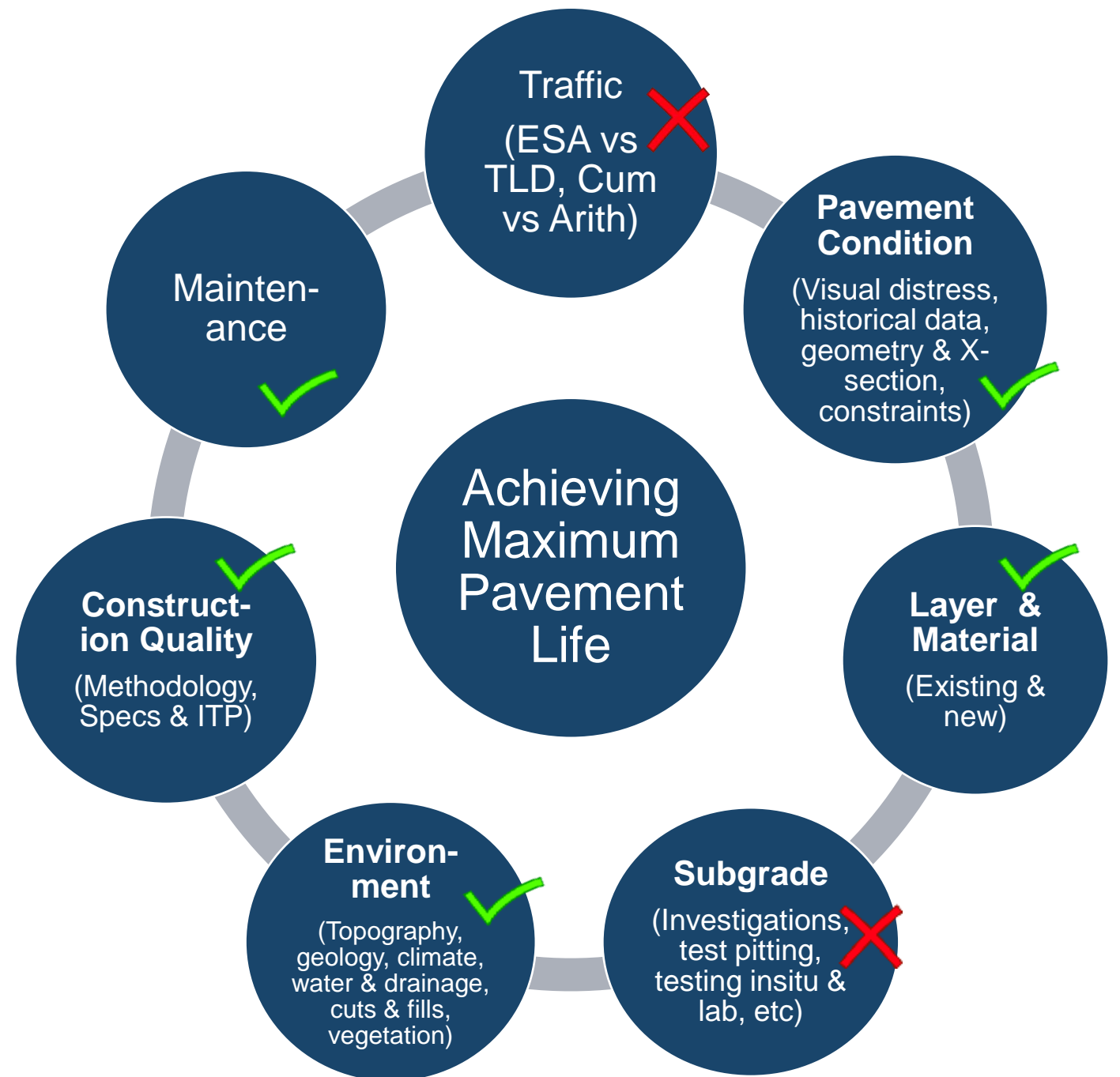
Most significant design-related factors affecting quality of roads:

"Nature and type of subgrade soil investigation"

Rahul R. Minde Dr. Anil N. Ghadge Analysing the factors influencing quality throughout the lifecycle of a road project.

Ahmed Ebrahim Abu El-Maaty, Ahmed Yousry Akal, Saad El-Hamrawy, "Management of Highway Projects in Egypt through Identifying Factors Influencing Quality Performance

And several other papers



Importance of good Sub-Grade Characterisation has been well understood for many years!

Austroads (1992) Procedures for Design of Flexible Pavements
Austroads (1992) procedure with thin bituminous surface design chart shown in Figure 10.1.1 designed to provide sufficient subbase course.

U.S. Department of Transportation
Aviation Administration
IRC:37
1.1 The first guide to the importance of pavement evaluation and evaluation of pavement should be emphasized, publish based on (i) subgrade Bearing Ratio) and (ii) of number of commercial weight of 3 tonnes or more) per day.

There's little new in this presentation



"I want you to find a bold and innovative way to do everything exactly the same way it's been done for 25 years."

Fed Highway Administration: General Pavement Design Considerations (23 CFR 626) April 8, 1999.

stiff, moisture and frost important aspect of attention needs to be stiffness and the elements on the NHS. When clay or silt materials, 10 mm should be stiffness, is the most design thickness, composition and the less the layer thicknesses and shrinkage and changes in be separately treated to avoid reflecting through to the surface (38). Such materials include reater al and replacement with non-(%) of depths up to 1 metre has such poor subgrade materials. high performance surfacings, Adelaide, IMENTS OF AN UNBOUND GRANULAR PAVEMENT FOR A SUCCESSFUL SPRAYED SEAL,

Subgrade

Support provided by subgrade is *one of most important factors* in determining pavement design thickness, composition and performance.

Support is dependent on *soil type, density and moisture content* at construction and in service!

Table 5.1: Use of subgrade support measures

Pavement type	Measure of subgrade support	
	CBR	Elastic parameters
Flexible	✓	✓
Rigid	✓	

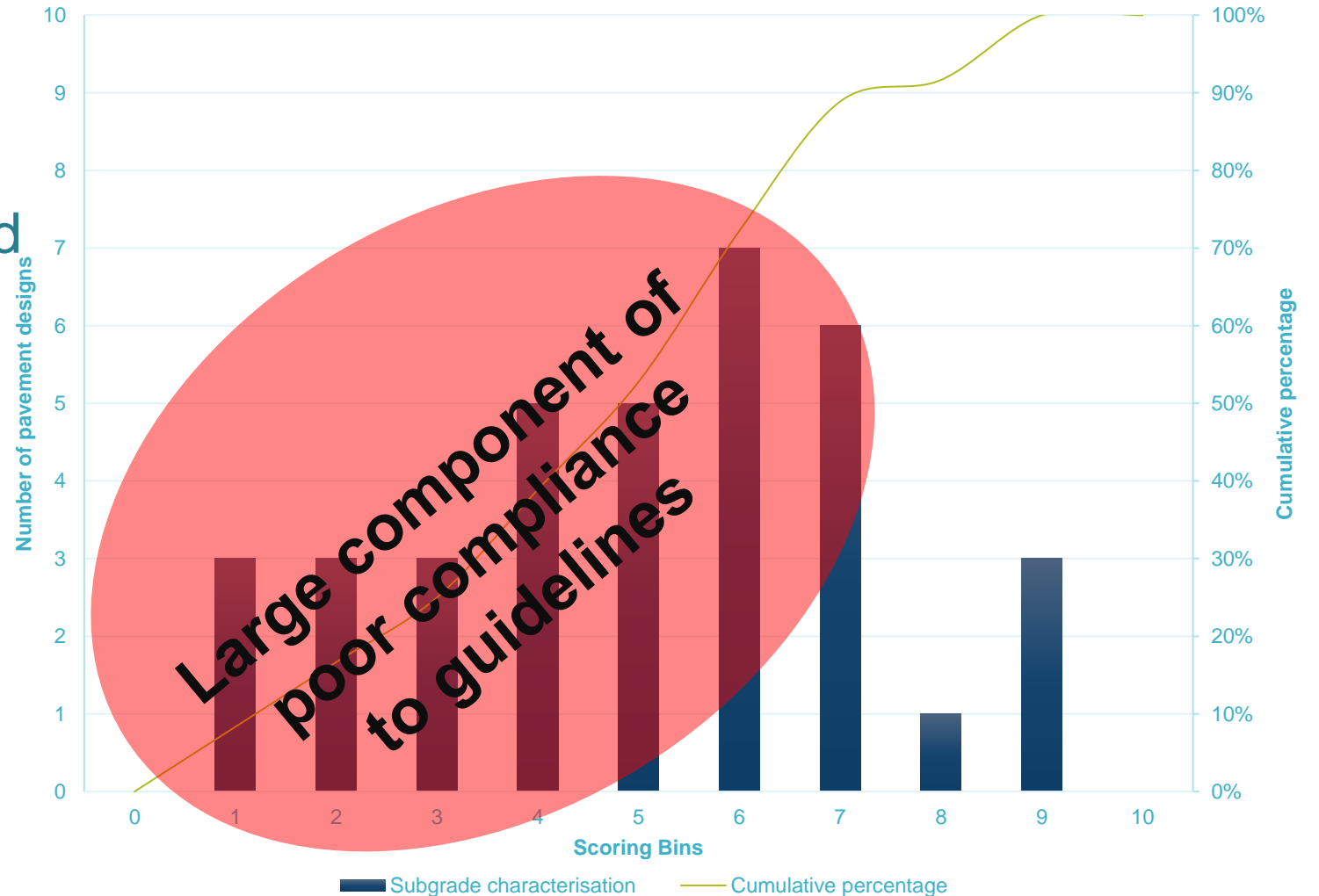
Guide to Pavement Technology Part 2: Pavement Structural Design, Ch 05

NZ / Austroads Best Practice

CH 05 Subgrade characterisation

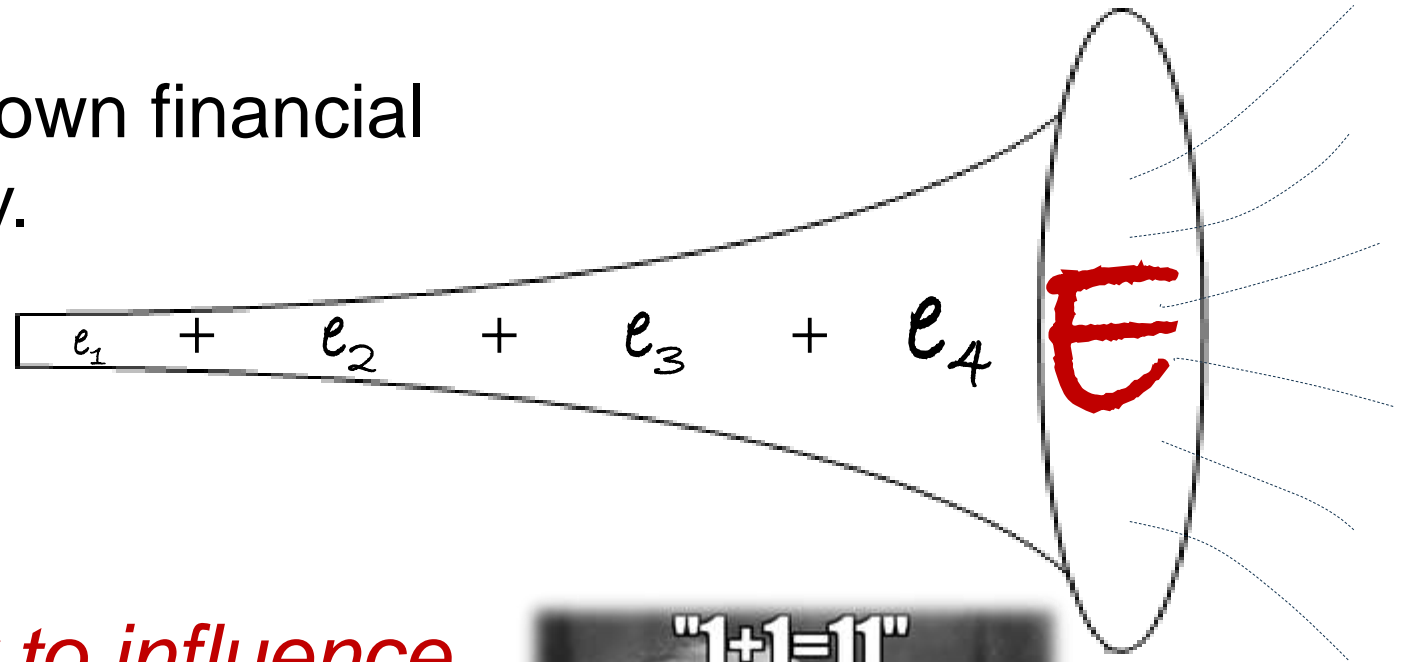
Depends on:

- HSD & FWD data analysis.
- Identification of TP sites and testing.
- Visual inspection.
- Site investigation.
- Insitu testing.
- Laboratory testing.
- Assignment of design modulus.

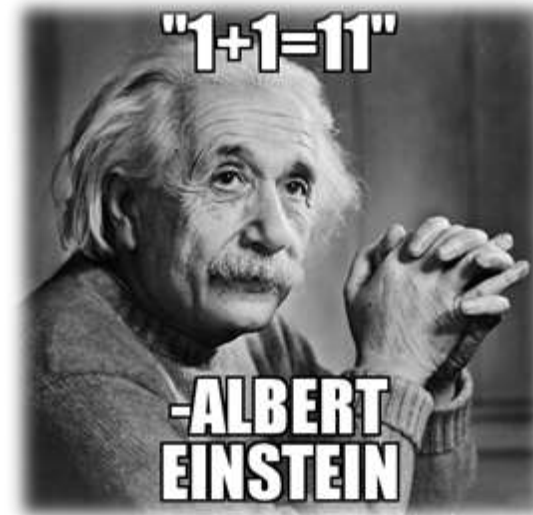


“Multiplier” Effect

Multiplier effect is a well known financial principle and in error theory.



The *ability of one factor to influence a whole number of factors*, creating a *total much bigger than the sum* of the individuals.



“Multiplier effect”

SCALA DCP subgrade strength inaccurately tested



Estimation of CBR from DCP



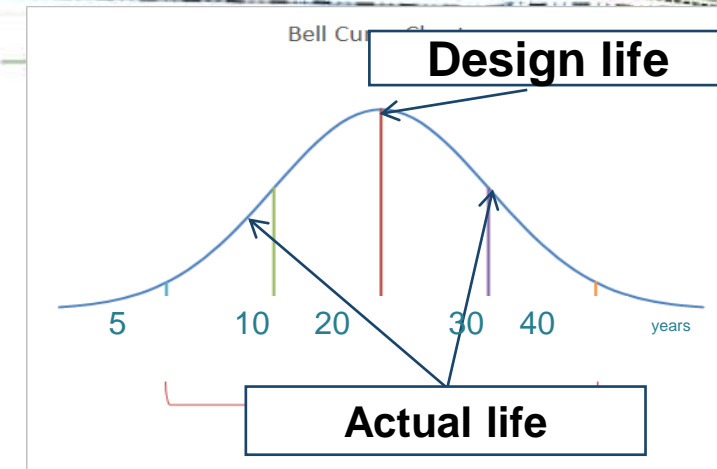
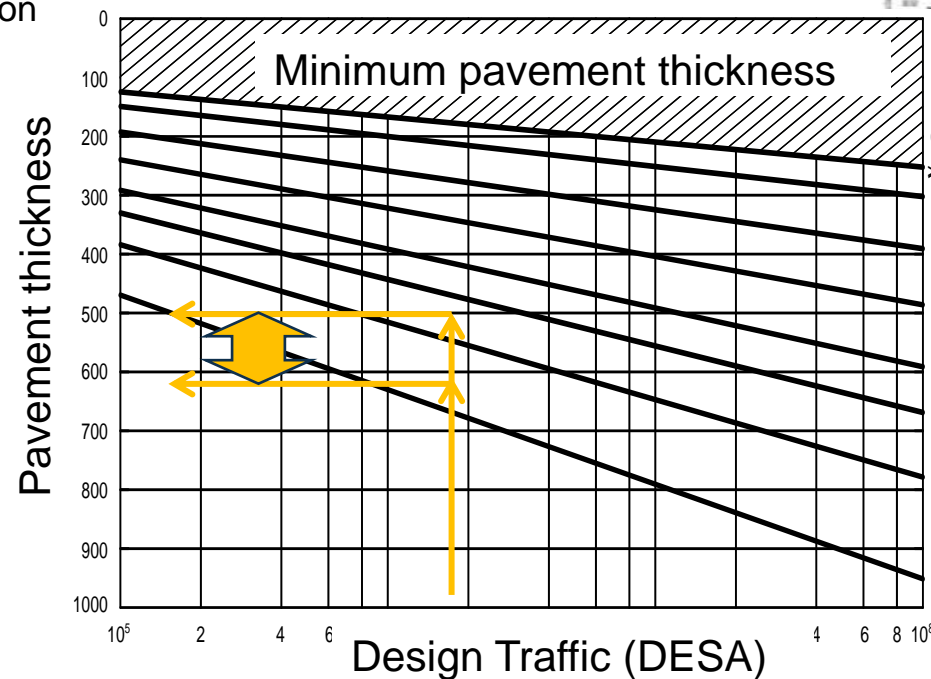
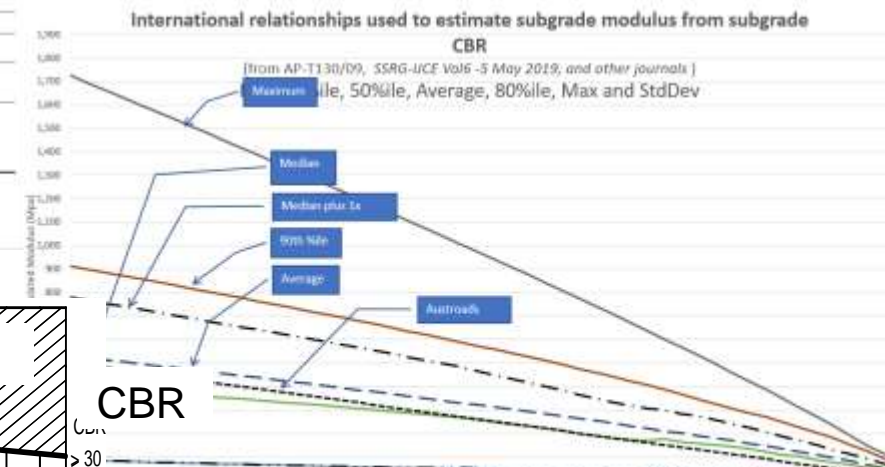
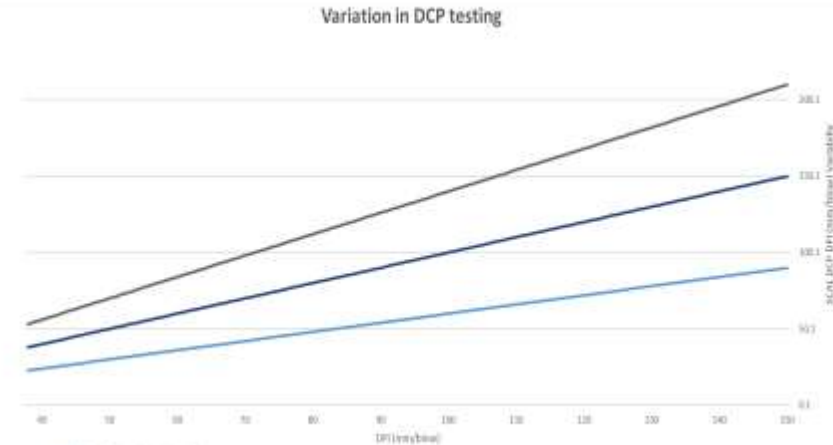
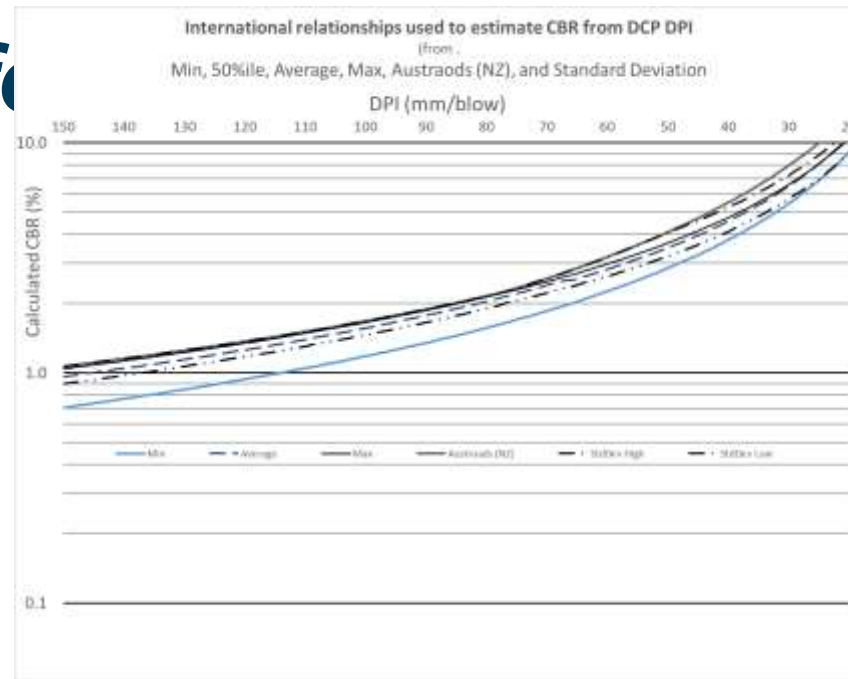
Estimation of Modulus Reaction (M_R) from CBR (inferred)



Over / under estimation pavement thickness



Pavement either over / under performs



Recent test pit investigations

What we have seen

Recent issues in pavement investigation

Test pit

- Generally done in dry season
- Seasonal variation not identified
- SG characterised stronger / weaker
- Too small
- Don't reach subgrade

Scala DCP

- SG soil type & applicability of DCP
- SG characterised stronger / weaker
- Misidentification of M_R – N. Island
- Volcanic
- DCP not recorded at SG start depth

Pavement moisture

- Perched water table not identified!
- Sub-soil Drains not identified

Vane shear

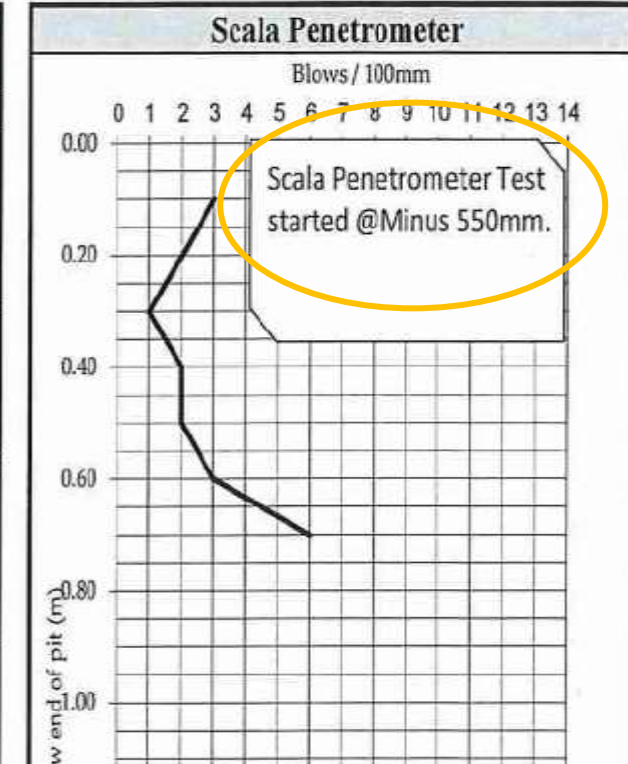
- Rarely done (in silt and clay)
- Moisture sensitive subgrades not identified

Austroroads / NZ guidance does not appear to be followed fully

Test pitting



Depth (mm)	Pavement Description
45	CHIPSEAL: Worn, flushed & rutted.
220	BASECOURSE: AP40mm Angular crushed, sandy silty, greywacke GRAVEL. Re-worked, grey brown, dense, moist.
350	SUBBASE: AP120mm Angular crushed, sandy silty, greywacke COBBLES. Grey brown, dense, moist.
550	SUBGRADE : Medium SAND with minor fine to medium pumice gravel, orange brown, medium dense to loose, moist, pumiceous.
	End of Trench 2.



NZ Good practice:

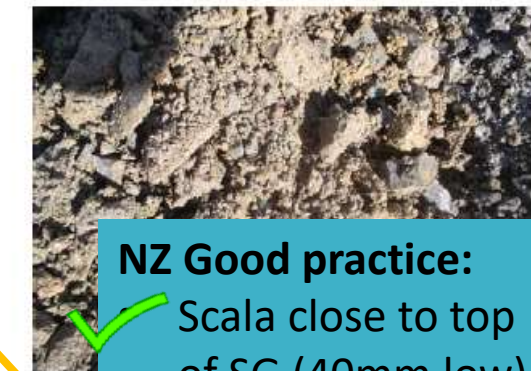
✗ Scala penetrometer testing should also always be used to identify any weak layers to a depth of at least 1m **FROM** the **TOP** of the subgrade.

No knowledge of strength of upper subgrade on which we should be characterising the subgrade!

SITE INVESTIGATION TEST REPORT

Notes: Geonet found under Sub Base, cracking in Asphalt

Layer	Depth (mm)		PRODUCT	Predominant Colour	Secondary Colour	Nominal Size (mm)
1	0	50	Asphalt-POOR	BLACK		
2	50	150	Stabilized Basecourse	GREY	BROWN	40
3	150	350	Basecourse	BROWN	GREY	40
4	350	660	Sub Basecourse	BROWN	GREY	160
5	660		Clay	ORANGE	BROWN	

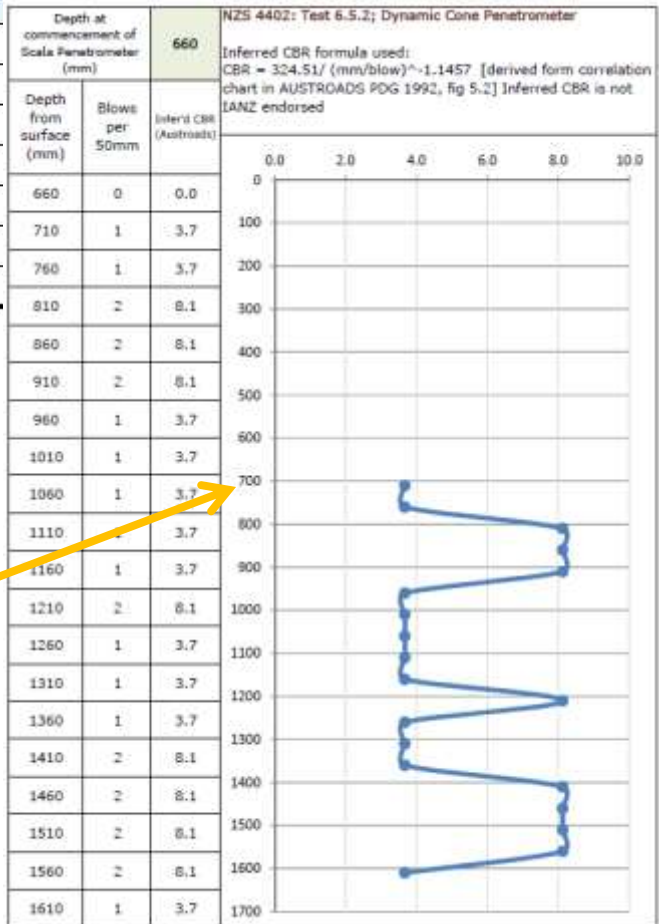


NZ Good practice:

✓ Scala close to top of SG (40mm low)

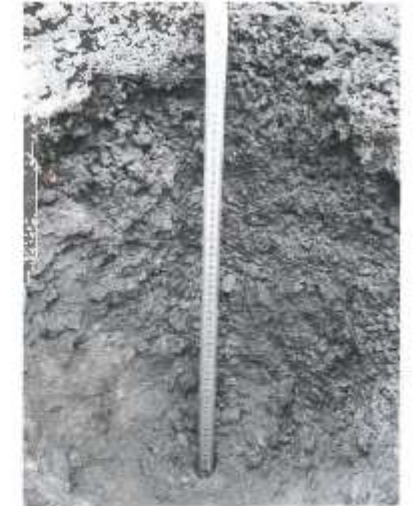
✗ No nominal/max size

✗ No Shear vane??



Test pitting

Depth (mm)	Description	Penetration Resistance Tests		
		Depth	Blows	CBR
0	SURFACE Chipseal Slightly flushing	100		
40	Scabbing of surface nearby	200		
40	GRAVEL AP40 river gravel with moderate broken faces. Well compacted. Highly contaminated with grey silt. Unweathered, Unbound. Damp	300		
		Subgrade not reached		
600	Test pit ended.			
		Notes		
		UTP - Unable to penetrate		



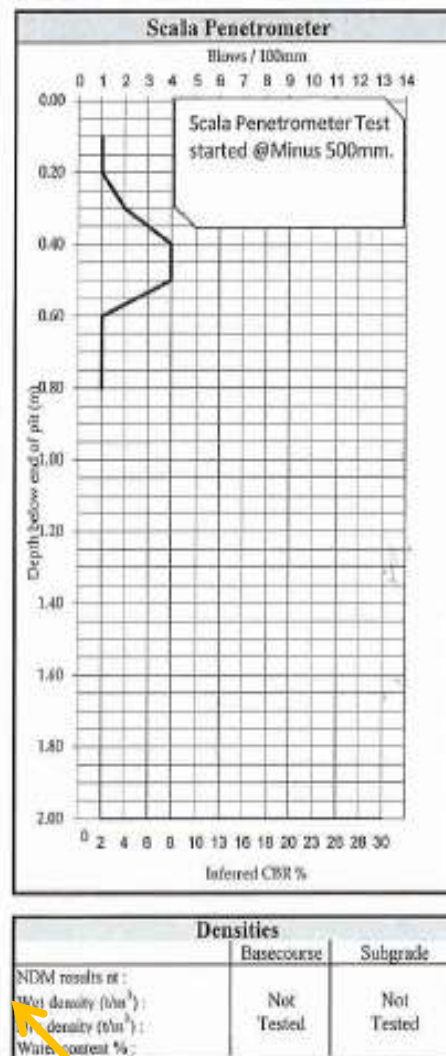
NZ Good practice:

- ✓ Good descriptions
- ✗ Gravel – why try DCP?
- ✗ TP did NOT reach SG
- ✗ Test Pit VERY small!
- ✗ Tape measure impossible to read

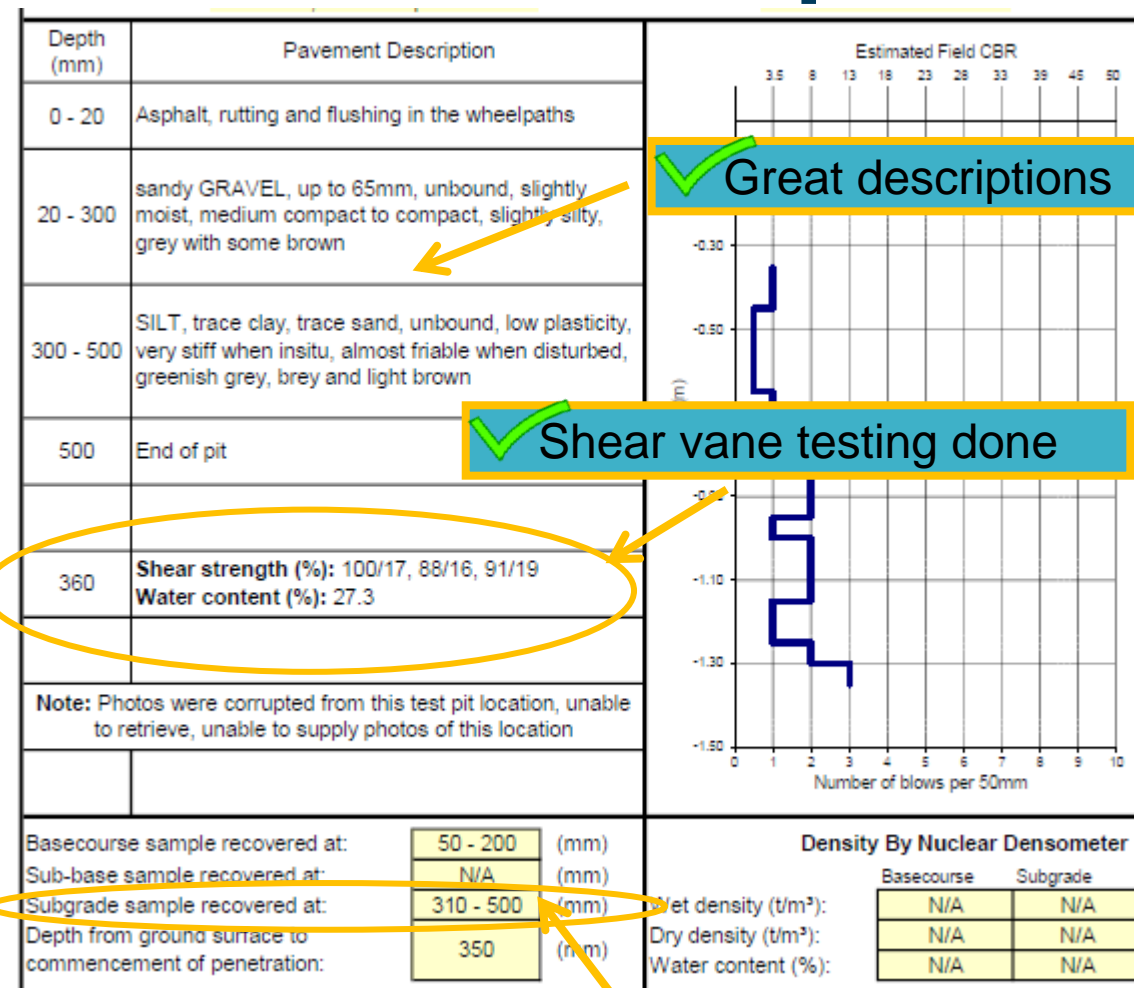
150mm. Was Subgrade 1 a subgrade or a layer?

BASECOURSE: AP40mm Angular crushed, sandy silty, greywacke GRAVEL. Re-worked, densification, grey brown, dense, moist.	260
SUBBASE: AP80mm Sub Angular, sandy silty, greywacke scoria GRAVEL. Grey brown, dense, moist.	360
SUBGRADE: Fine SAND with minor medium to coarse gravel, orange brown, dense, moist, unconsolidated .	500
SUBGRADE II: Sandy SILT (Organic), dark brown, soft, moist.	600
End of Trench 1.	

Basecourse sample recovered at:	260mm
Subbase sample recovered at:	360mm
Subgrade sample recovered at:	500mm
Depth at which scala penetrometer started:	500mm



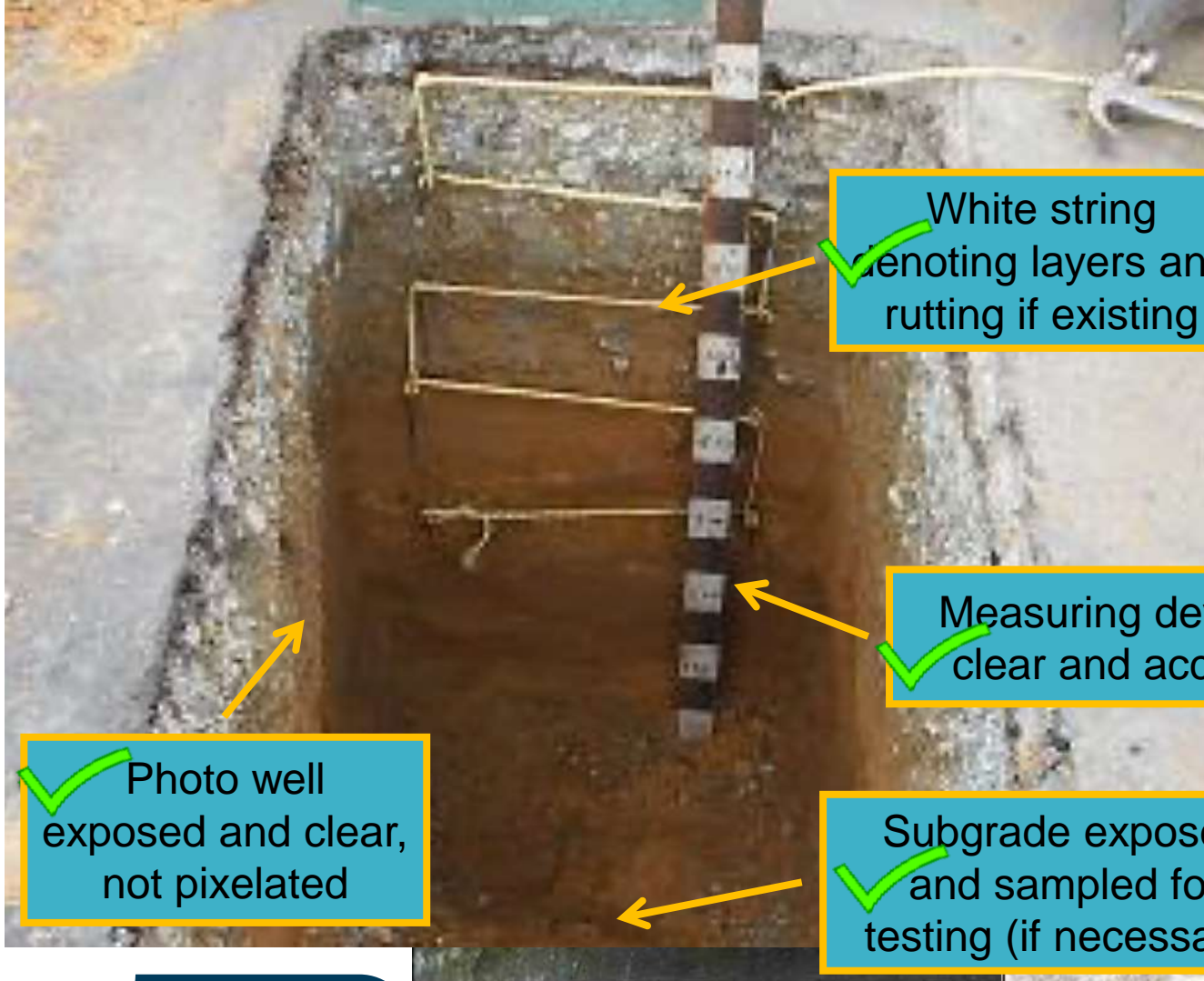
Good example



No Shear Vane testing

SG sampled and tested

Test pitting - Photos



✓ White string denoting layers and rutting if existing

✓ Measuring device is clear and accurate

✓ Photo well exposed and clear, not pixelated

✓ Subgrade exposed and sampled for testing (if necessary)

NZ Good practice:

- ✗ Photos under/over exposed and/or poor quality
- ✗ Measuring devices unclear
- ✗ No Indication of layers



What do we need to improve?

- Investigations
- Test pits
- Insitu testing
- Laboratory testing

Level of investigation *MUST*

equal required level of performance risk



PRACTICAL

Gut feel & experience

Balanced approach

Practical

Technical

Defensible

Traceable

Repeatable

“Accurate”

Adaptable

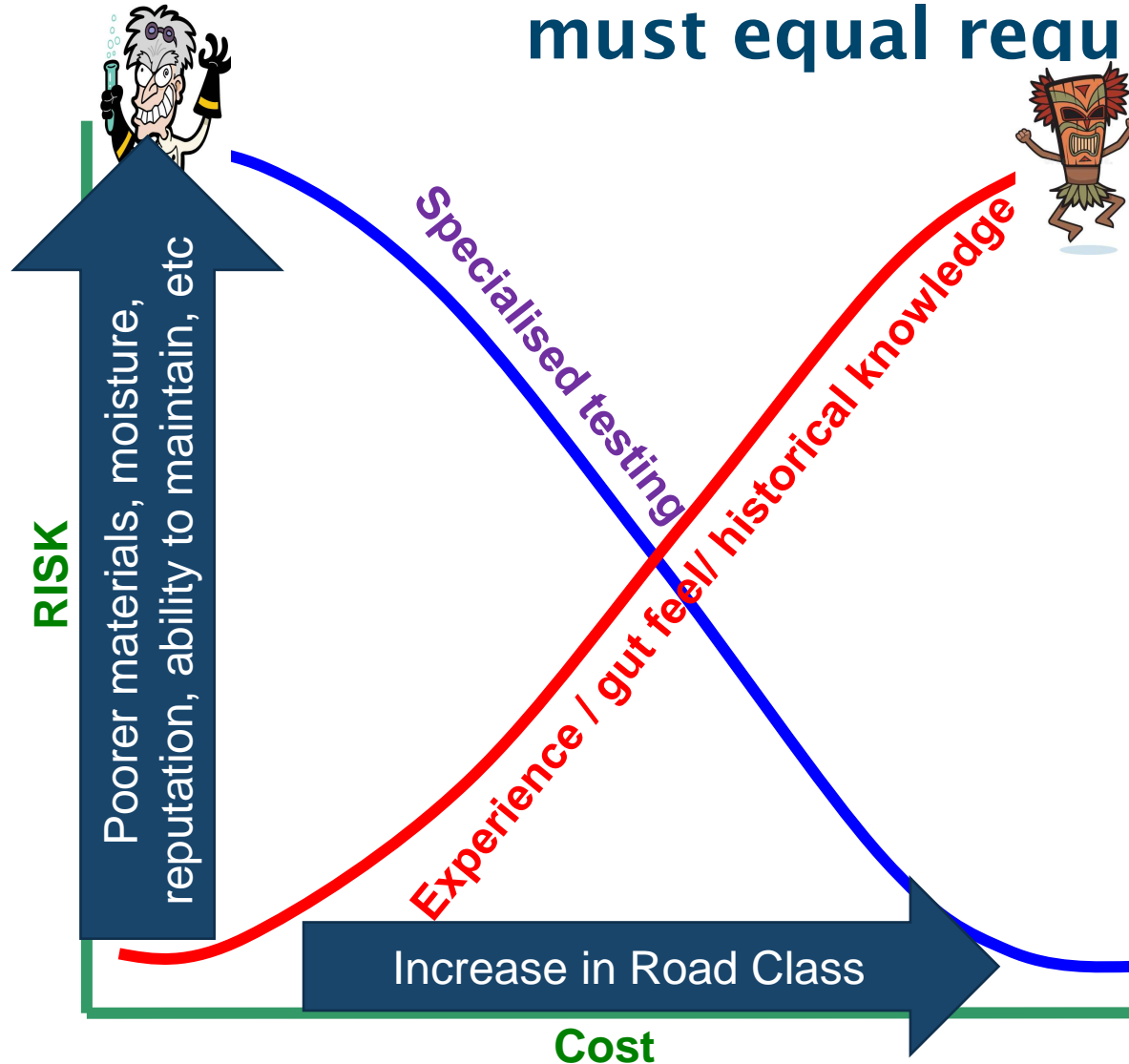


TECHNICAL

Scientific principles and
testing

Level of investigation

must equal required level of performance risk



- **Budget VS Risk.**

- Enough TP & tests to have good idea of FMA.
- Higher order roads, & larger projects = higher risk, = more test pits & testing...

- **Investigation & testing MUST identify:**

- Material related risks MUST be identified
- Additional sampling and testing if required.

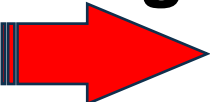
- **Test Pits number MUST represent homogeneous sections:**

- Both good and bad areas.
- Defects mapping.
- FWD analysis – uniform sections
- Geology / fills & cuts / other anomalies.
- Areas where moisture suspected.

BUT can only be reduced if risks are known and understood (previous test results, etc)

Test pits

MUST identify:

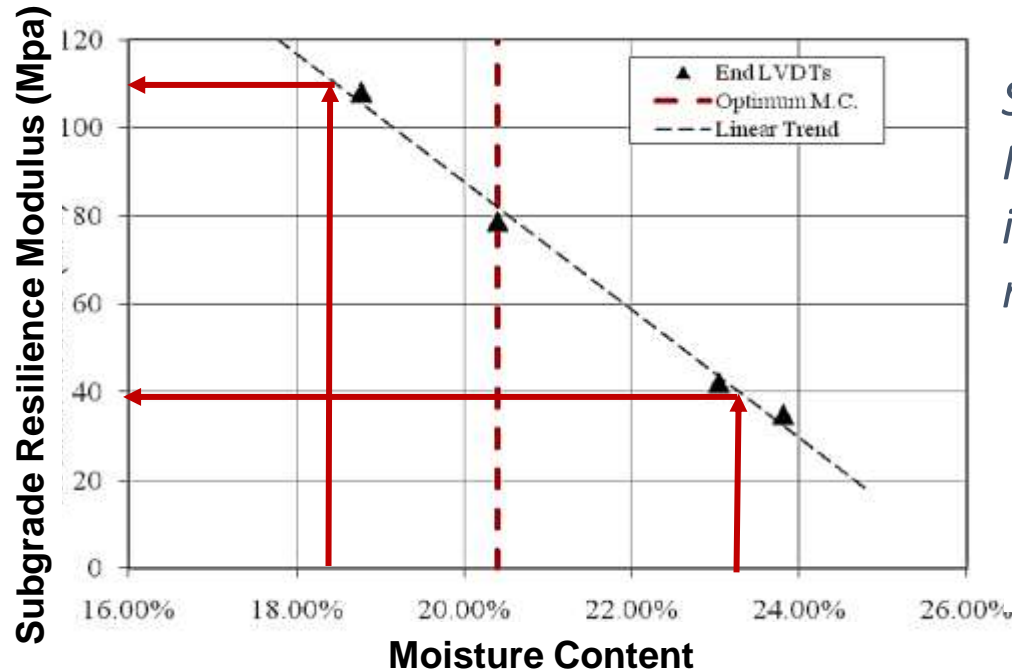
- **Visual assessment of layer characteristics**
- **Subgrade strength** (volcanic, clay, silt, sand, etc)
- **Subgrade variability** (topography, soil type)
- **Moisture changes** during service life
- **Drainage conditions**
 - Presence of subsurface water
 - Depth to the water table
- **Problem subgrades** - expansive or sensitive  addition sampling & testing.



Test pits

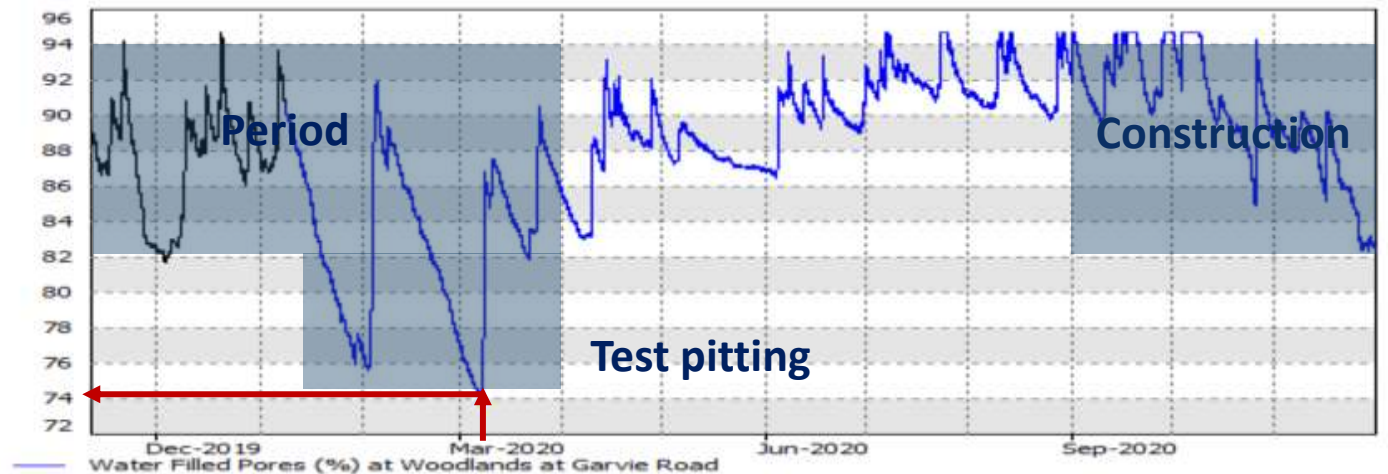
New Zealand guide to pavement evaluation and treatment design requires that test pits are:

- At least *400 mm × 1200 mm*.
- To *SG level*, and sampled after Scala DCP.
- Each layer material described *including moisture* - Field Description of Soils and Rock (NZGS 2005).
- TP ideally done at *wettest time of year*, **OR** dated clearly so seasonal moisture can be noted.



Subgrade Resilient Modulus variation in clay due to moisture content.

H Soliman and A Shalaby,
“Sensitivity of Subgrade Resilient Modulus to Moisture Variation”,
Development of New Technologies for Classification of Materials
Session, 2010 Annual Conference of the Transportation Association of Canada, Halifax, Nova Scotia.



Water filled pores for the construction and post construction. Note the water content at construction and test pitting.

<http://envdata.es.govt.nz/index.aspx?c=soil-moisture&tab=graph>

SG STRENGTH: SCALA DCP

Principal objective: Determine design subgrade CBR.

For the majority of soil types, best correlation with subgrade CBR (Scala DCP) from the Weighted Average blows/50mm for 1st three 50mm intervals:

- ✓ 0-50mm weighting: 0.7
- ✓ 50-100mm weighting: 0.2 and
- ✓ 100-150mm weighting: 0.1 for each interval.

Smits (1990)

- **START AT TOP OF SUBGRADE!**
- **RECORD SCALA AT blows/50mm INTERVALS.**
- **RECORD >1.2m BELOW PAVEMENT SURFACE**

Several Limitations:

1. Surcharge Loading
 - Material strength dependent on confining pressure and loading.
 - DCP in TP with surcharge loading removed - may not represent the insitu strength
2. Seasonal Moisture fluctuation
 - DCP CBR functional subgrade CBR.
 - Pavement foundation @ testing, over-estimation of in-service moisture levels.
3. Non-cohesive & coarse materials (i.e. sand and gravels)
 - Multiple correlation methods, not accurately verified
 - Not considered a reliable method.
4. Fair correlation with fine-grained cohesive material.



FACTORS AFFECTING DCP RESULT

1. ALIGNMENT OF DCP RODS

- If rod is tilted during testing, resistance around the rod will increase.
- Also occurs if DCP rod penetrates through collapsible granular material.

2. DEPTH OF TESTING

- Test results very sensitive to depth of testing.
- If bottom rod of DCP is longer than standard rod, correction to DCPI value should be applied because vertical confinement and skin friction around the rod increases resistance to the penetrating rod.

3. DAMAGED CONE TIP

- If cone tip of the DCP is damaged it will give erroneous test results.

4. APEX ANGLE OF THE CONE

- Penetration rate significantly affected by cone apex angle.
- Penetration rates from DCP 30° are 10% greater than angle of 60°.

5. HAMMER WEIGHT

- The hammer weight exactly 8 kg.
- If weight is less, then rate of penetration will decrease and vice-versa.

6. LIFTING HEIGHT OF HAMMER

- If hammer not lifted to the top restraint plate and dropped freely, impulse force exerted will be reduced and the values of penetration decrease.

7. MOISTURE CONTENT

- DCP test results very sensitive to variations in moisture content.
- As moisture content increases, the penetration rate increases.
- DCP tests should be conducted at worst moisture content when the granular and sub-grade layers are softest and their minimum strength are recorded.

8. MATERIAL COMPOSITION

- DCPI varies with test material composition, soil class, coefficient of curvature, uniformity, density of the layer material and plasticity of the soil.

9. INTENSITY OF COMPACTION

- DCPI influenced by intensity of compaction and confinement of granular and subgrade layers.

Subgrade sensitivity – Shear Vane test

Measure of the loss of strength that occurs when the soil is disturbed or remoulded.
Only for clays and silty clays, especially when saturated.

Shear Strength Ratio = $\frac{\text{Undisturbed shear strength or Peak strength}}{\text{Residual or Remoulded Shear Strength}}$



Definition	Shear Strength Ratio
Insensitive	< 2
Moderately Sensitive	2 – 4
Sensitive	4 – 8
Extra Sensitive	8 – 16
Quick	>16



Table 2 Definition of soil sensitivity levels
(NZ Geotechnical Society, 2005).

Greater Shear Strength Ratio = Greater risk subgrade loses strength due to traffic.

*A man should look for **what is**,
not for what he **thinks** should be.*

Think openly... Ask:

-

Sampling

Requirements

- *Most neglected but most important aspect of testing.*
- Representative, full depth, full width.
- *Each layer* to be sampled but not necessarily tested.
- Sub-grade sampling only *after DCP & shear vane.*
- Lab Soaked CBR if *SG poor or sensitive.*
- Sample sizes large enough!
 - *>35kg if unknown testing or PSD & Indicator tests.*
 - *>60kg California Bearing Ratio.*



Atterberg Constants

Critical part of investigation.

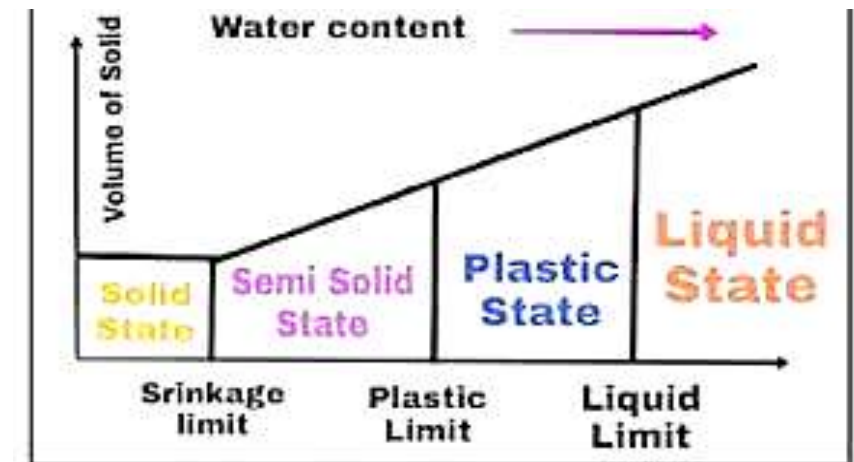
Expansive soils can cause loss of pavement shape due to moisture changes leading to pavement rehabilitation.



Table 5.2: Guide to classification of expansive soils (*Assessing tests NZ PET Ch 5.3*)

Expansive nature	Liquid limit (%)	Plasticity Index	PI x % < 0.425 mm	Swell (%) ⁽¹⁾
Very high	> 70	> 45	> 3200	> 5.0
High	> 70	> 45	2200–3200	2.5–5.0
Moderate	50–70	25–45	1200–2200	0.5–2.5
Low	< 50	< 25	< 1200	< 0.5

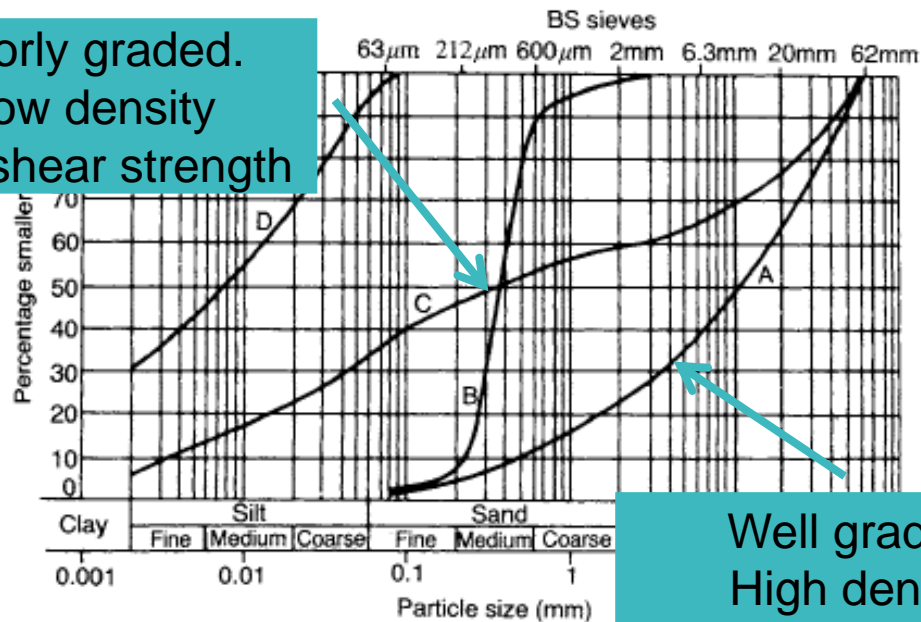
¹ Swell at OMC and 98% MDD using standard compactive effort; four-day soak. Based on 4.5 kg surcharge.



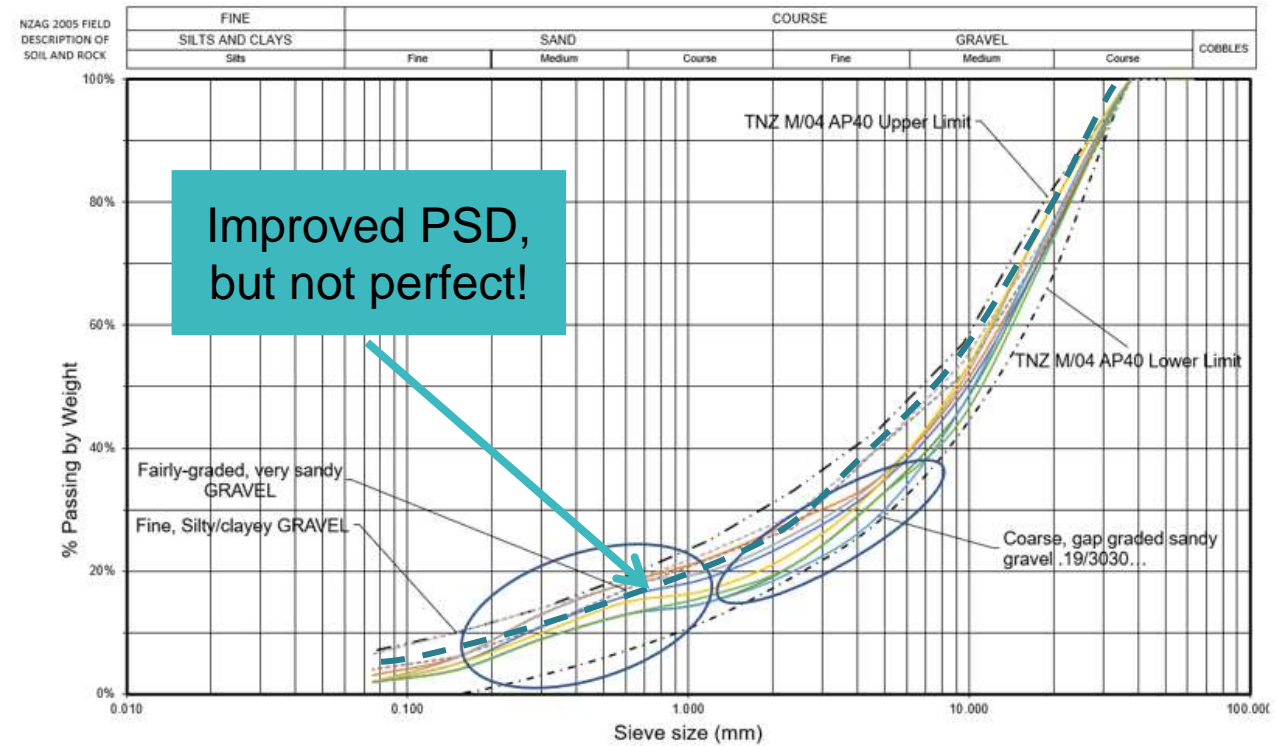
Particle Size Distribution

- Basis of getting maximum density and maximum shear strength.
- Effects well understood for many years!

Poorly graded.
Low density
Low shear strength



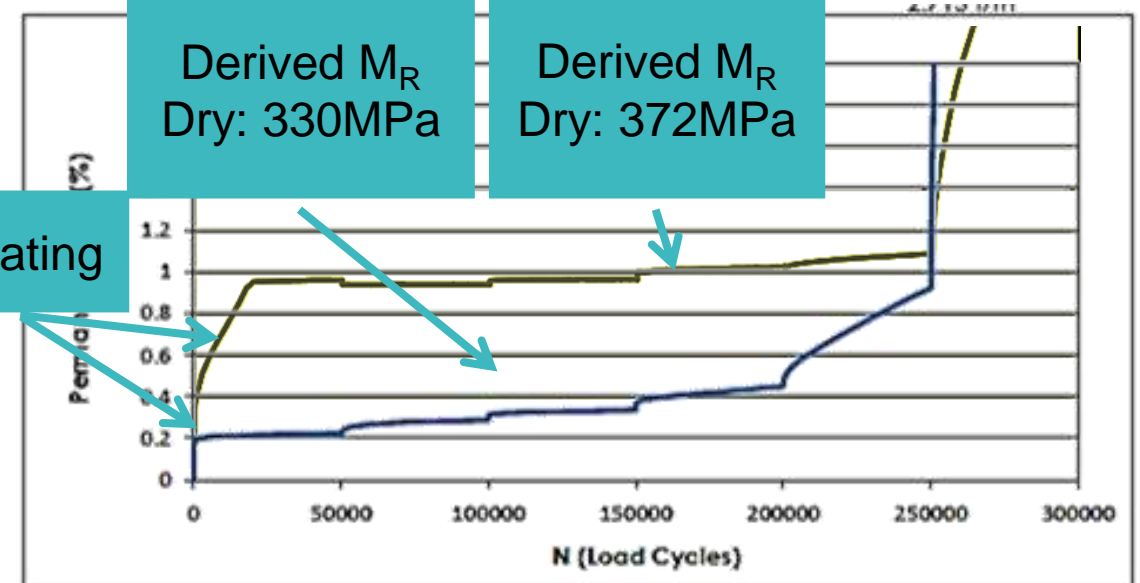
Well graded.
High density
High shear strength



Derived M_R
Dry: 330MPa

Derived M_R
Dry: 372MPa

Seating



California Bearing Ratio

Evaluates strength & moisture susceptibility.

Water content should be the equilibrium value

Soaked vs Unsoaked

- Soaked
 - Compulsory if Water Table <1m below seal or potential for flooding.
 - If sensitive or saturated clay
- Unsoaked: If low rainfall area or deep water table exists.

Test uncertainty is high

- Care needed - sampling to analysis
- No test limits in NZ unlike other countries.
- SANS 3001-GR40:2010 Maximum systematic error between labs
$$E = 3 + 0,01(\text{CBR}) + 0,0015(\text{CBR}^2)$$
 - CBR 3% between CBR 1% and CBR 5%
 - MR between 10 and 50 MPa

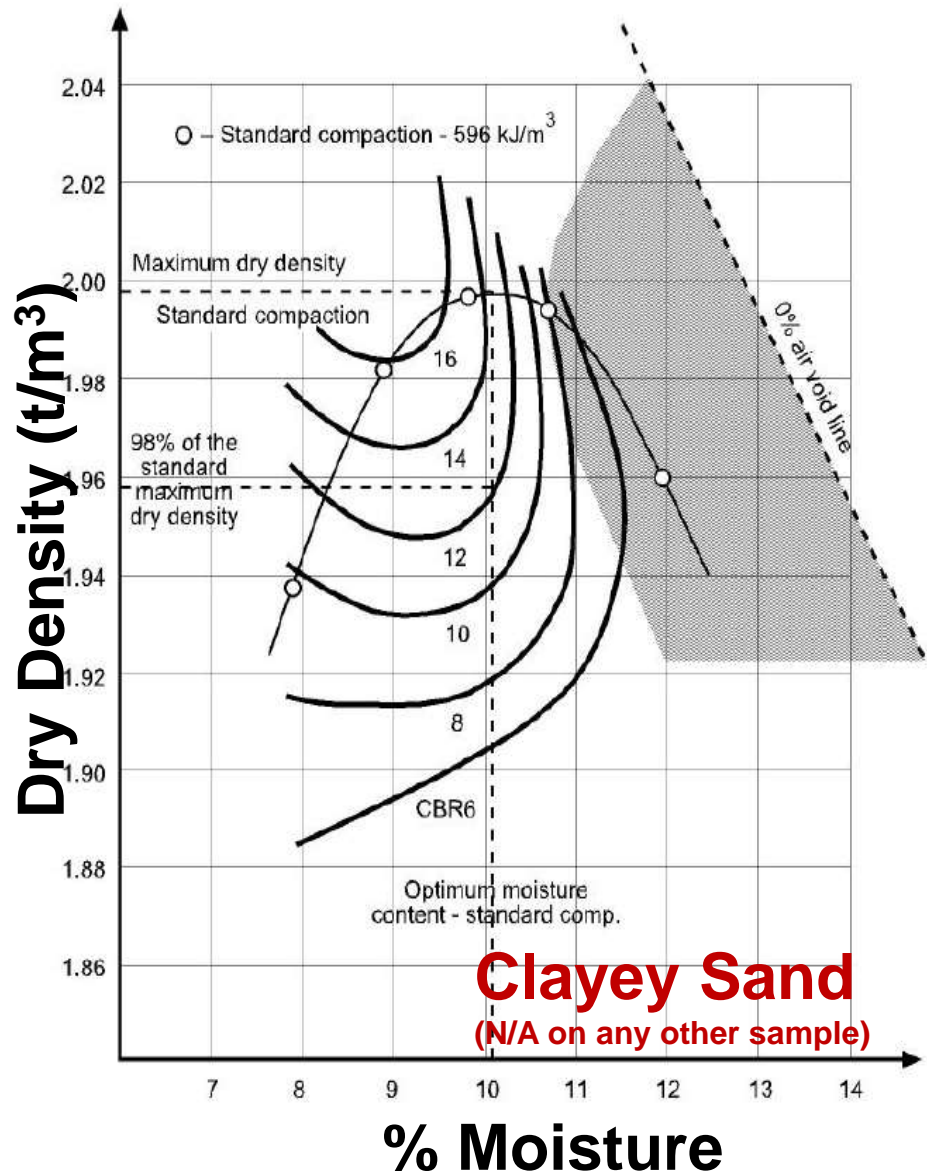


Figure 5.1: Example of variation of CBR with density and moisture content for clayey sand

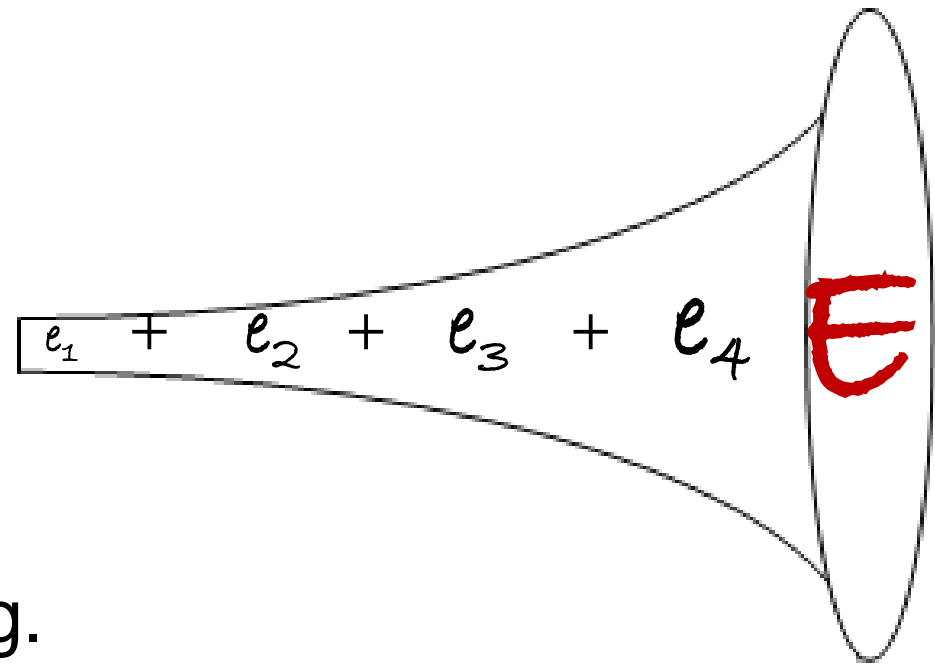
In summary...

Understand!

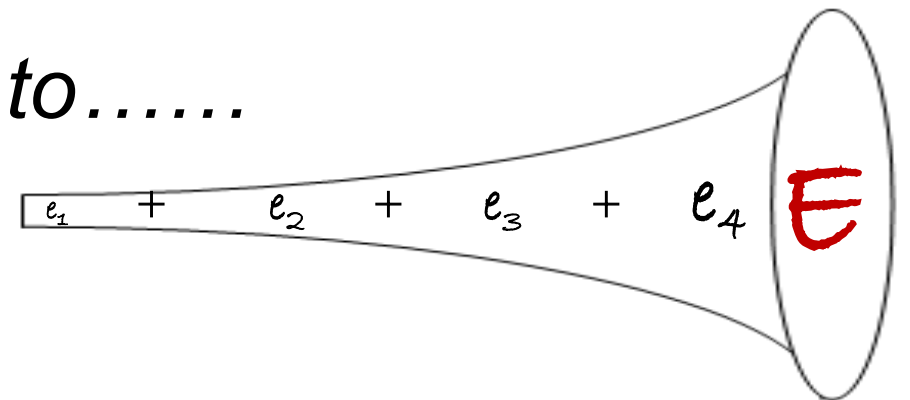
- Potential rehab strategy.
- Risk vs budget.
- What you want out of the testing.
- What test limitations are.

So that the resultant test errors reduce *from...*

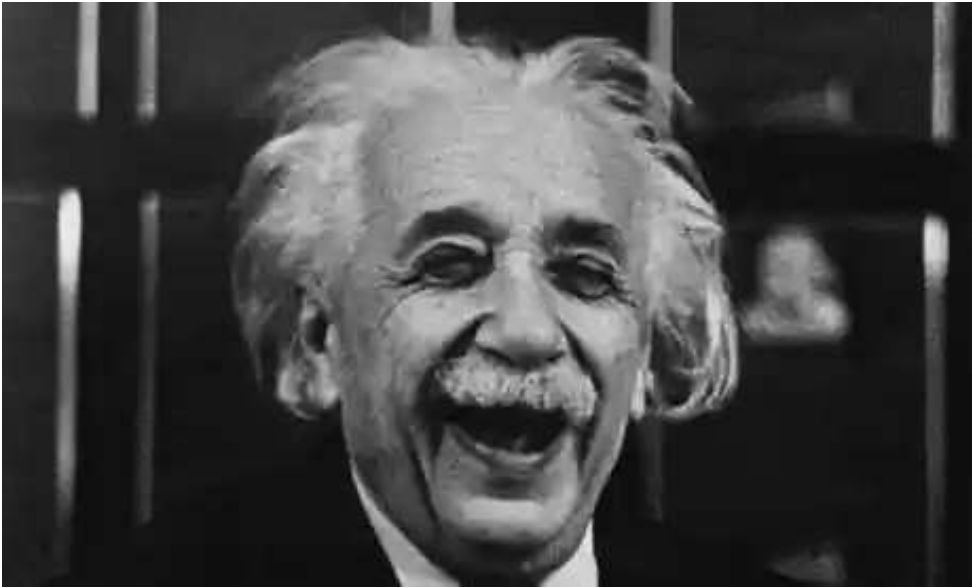
- Be open...
- Question everything!



to.....



*"The important thing is to not stop questioning.
Curiosity has its own reason for existing."*



Albert Einstein, 1879 - 1955

*"I have no special talent.
I am only passionately curious."*



***"A man should look for **what is,**
not for what he thinks should be".***