

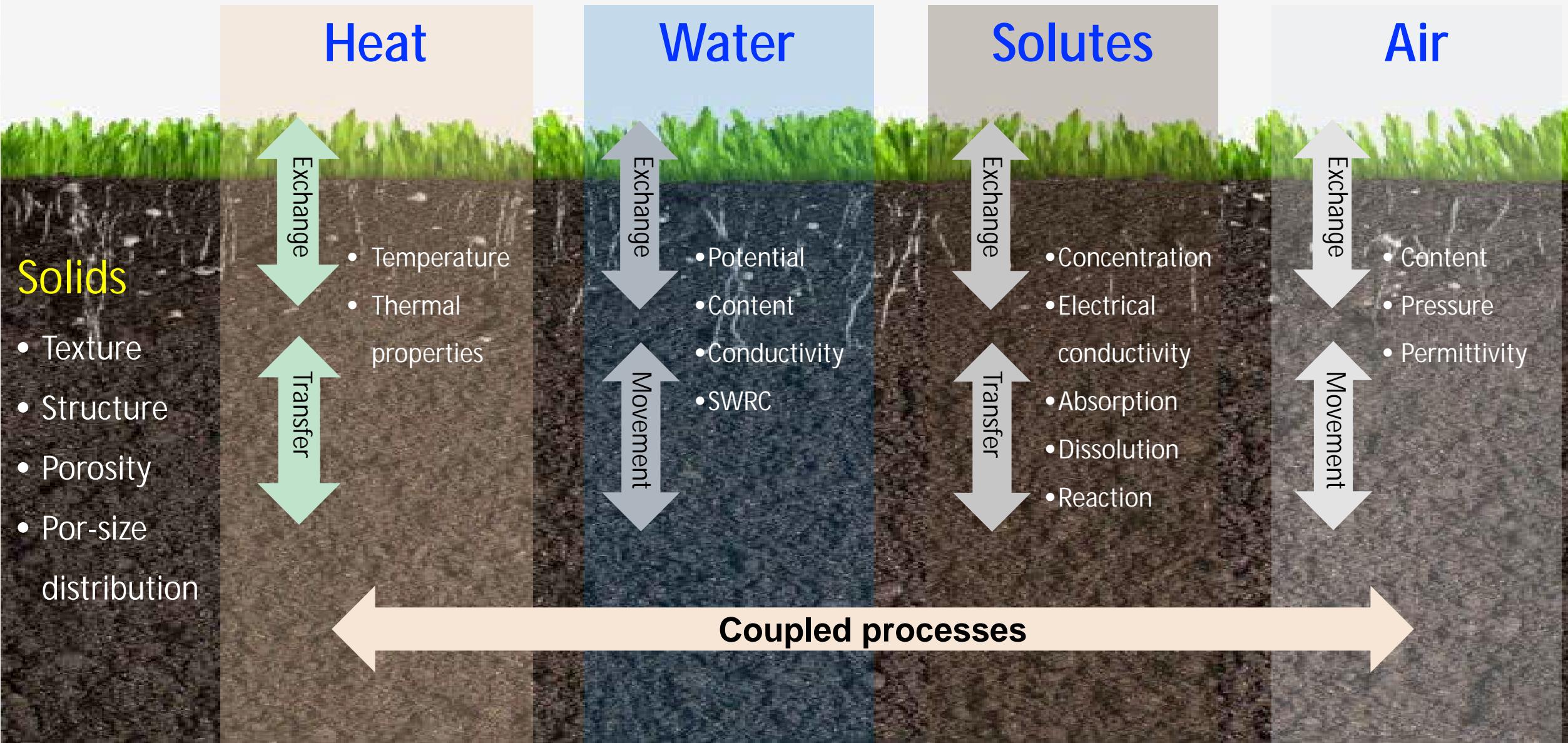


A thermo-TDR approach for simultaneous determination of transport parameters of sandy soils

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Soil Physical Properties & Processes

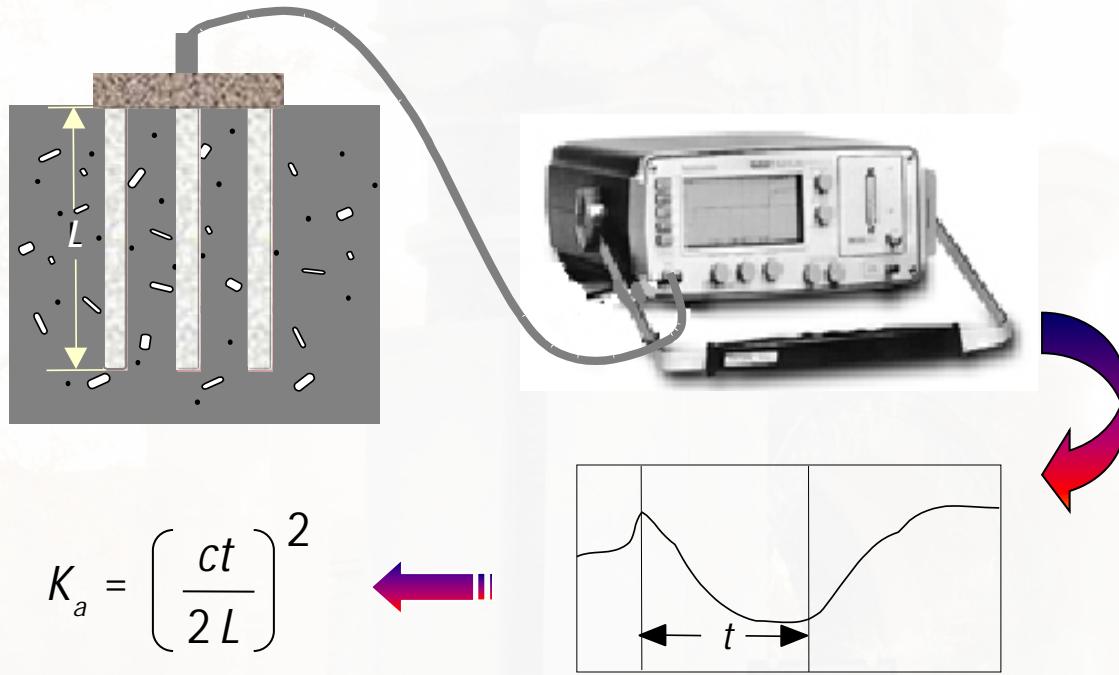


- ü Thermo-TDR technology
- ü Thermo-TDR approach for monitoring soil water retention and gas diffusivity
 - Theory
 - Validation



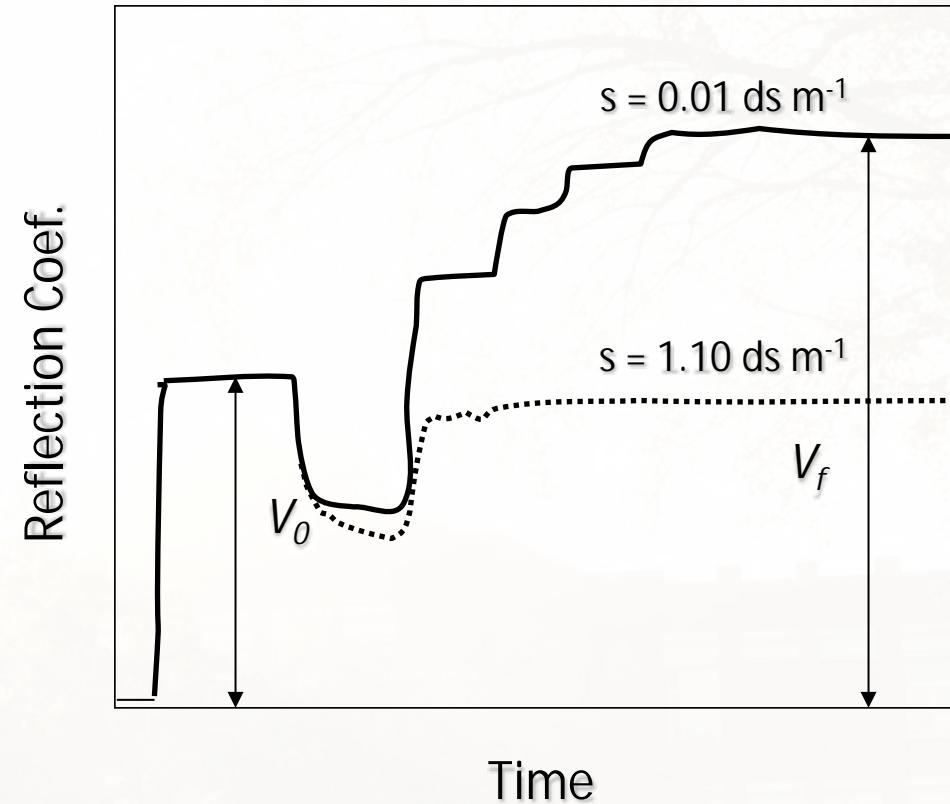
Thermo-TDR technology

TDR: monitoring soil water content and electrical conductivity



$$q = -5.3 \times 10^{-2} + 2.92 \times 10^{-2} K_a - 5.5 \times 10^{-4} K_a^2 + 4.3 \times 10^{-6} K_a^3$$

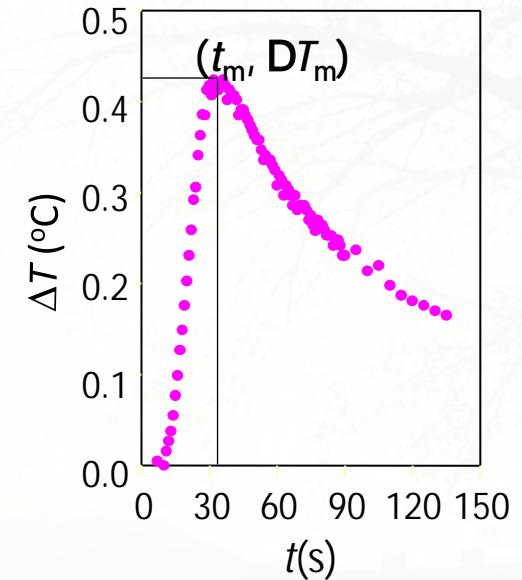
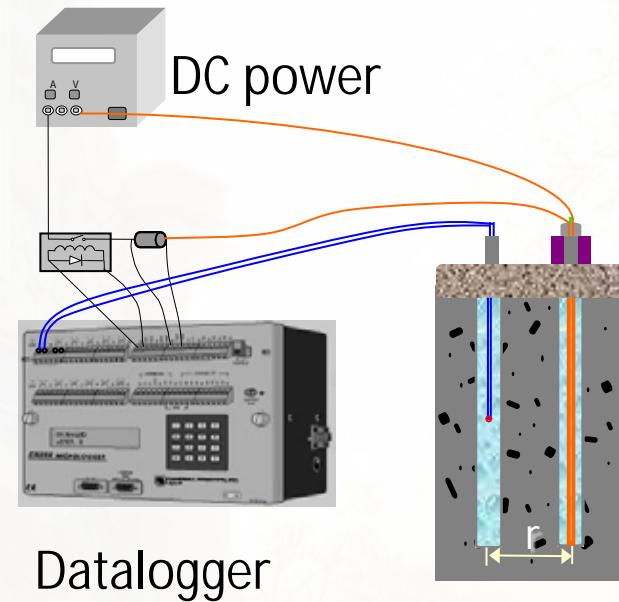
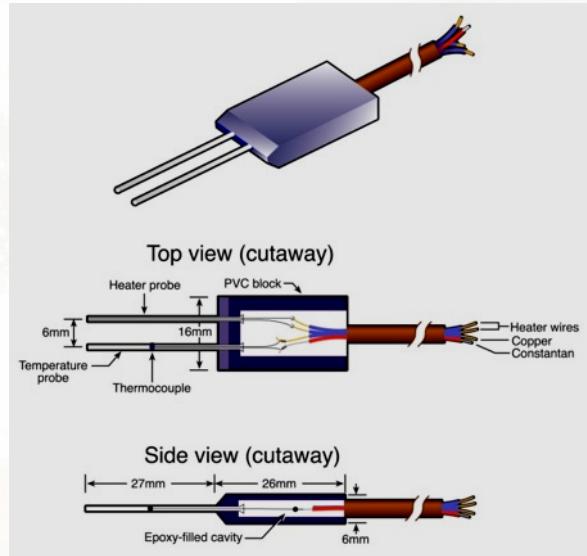
Topp et al. 1980. WRR. 16:579-582



$$\sigma = \frac{K_a}{Z_u} \left[\frac{2V_0}{V_f} - 1 \right]$$

Dalton et al. 1984. Science. 224:989-990

Heat pulse method: measuring soil thermal properties



$$C = \frac{q}{4\pi a} \left[\frac{\ln \left(\frac{r^2 - r_0^2}{r^2 - r_m^2} \right)}{(t_m - t_0)} \right]$$

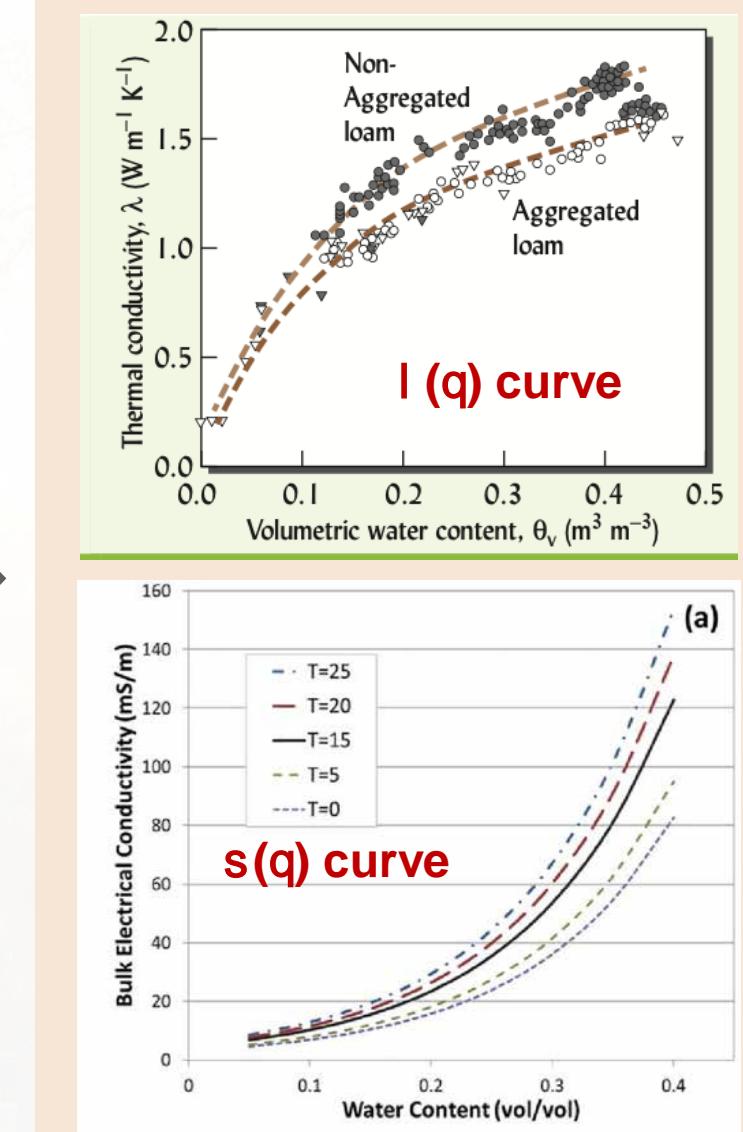
C : Volumetric heat capacity

$$\alpha = \frac{r^2}{4} \left[\frac{1}{(t_m - t_0)} - \frac{1}{t_m} \right] \left[\ln \left(\frac{t_m}{t_m - t_0} \right) \right]^{-1} = a' C$$

a : Thermal diffusivity

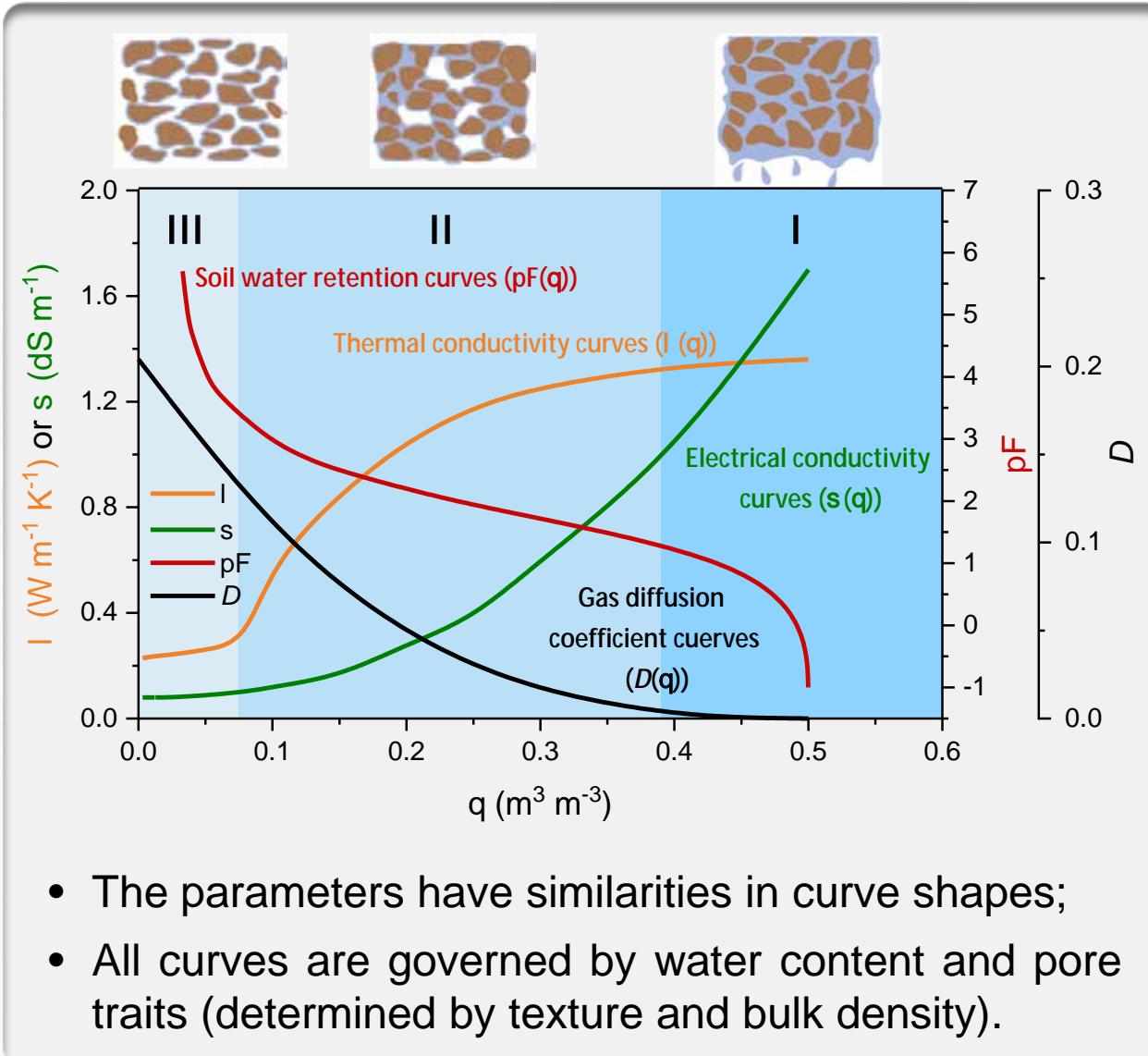
I : Thermal conductivity

Thermo-TDR technology: combining two units into one



Determining soil water retention and gas diffusivity: theory

Similarities between soil transport parameters



Ü Measuring $pF(q)$ & $D(q)$:

- Time and labor consuming
- Difficult to monitor in the field

Ü Measuring $I(q)$ & $s(q)$:

- Relatively quick and simple
- In-situ monitored is possible with thermo-TDR sensors.

- ? How are the four curves correlated with each other?
- ? Is it possible to determine $pF(q)$ and $D(q)$ curves indirectly from easily measured $I(q)$ and $s(q)$ curves?

From I (q) curve to pF(q) curve

van Genuchten (1980)
Soil Sci Soc Am J

$$\frac{\theta - \theta_r}{\theta_s - \theta_r} = \left(\frac{1 + \alpha pF}{1 + \alpha pF} \right)^m$$

θ_s : saturated water content
 θ_r : residual water content
 α, m : Soil specific parameters

Inputs

- Texture
- Bulk density: r_b
- Particle density: r_s
- Measured I (q) curve
- Field capacity (pF_{fc} , q_{fc})

qs $\theta_s = 1 - r_b / r_s$

qr $\frac{\lambda - \lambda_{dry}}{\lambda_{sat} - \lambda_{dry}} = 1 - \left(\frac{1 + \alpha \theta_f}{1 + \alpha \theta_f} \right)^p$

Lu & Dong et al (2015)
J Geotech Geoenviron Eng

a, m $\frac{\theta_{fc} - \theta_r}{\theta_s - \theta_r} = \left(\frac{1 + \alpha pF_{fc}}{1 + \alpha pF_{fc}} \right)^m$

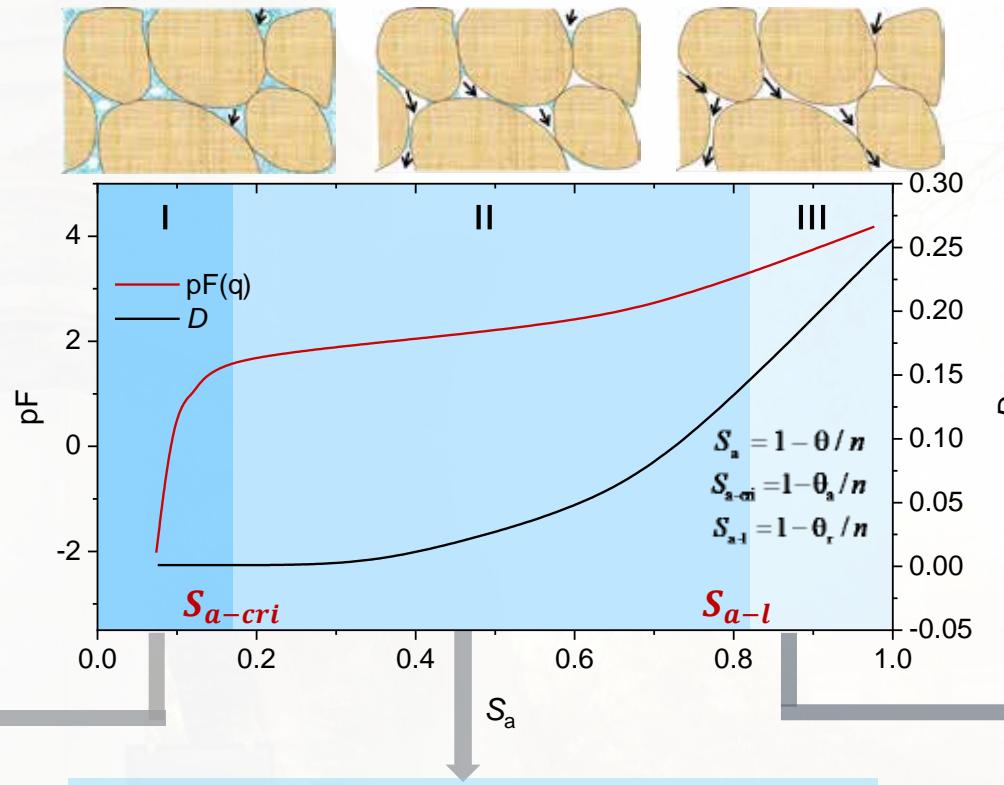
Liu et al (2024)
Soil & Till Res

From $h(q)$ curve to $D(q)$ curve

Section I ($0 < S_a \leq S_{a\text{-cri}}$):

- pF increases dramatically with S_a
- Air diffusion strongly restricted in limited pore space

$$D = 0.0001 \text{ (very low, constant)}$$



Section II ($S_{a\text{-cri}} < S_a < S_{a\text{-l}}$):

- More space for air diffusion
- pF, D increases exponentially with S_a

$$D = D_{dry} - b(1 - S_{a\text{-l}}) \left(\frac{S_a - S_{a\text{-cri}}}{S_{a\text{-l}} - S_{a\text{-cri}}} \right)^c$$



Section III ($S_a \geq S_{a\text{-l}}$):

- Most pore space for air diffusion
- $pF & D$ increases linearly with S_a

$$D = D_{dry} - b(1 - S_a)$$



Determination of model parameters

$$D = \begin{cases} 0.0001 & \text{Section I} \\ [D_{dry} - b(1 - S_{a-l})] \left(\frac{S_a - S_{a-cri}}{S_{a-l} - S_{a-cri}} \right)^c & \text{Section II} \\ D_{dry} - b(1 - S_a) & \text{Section III} \end{cases}$$

Dividing points of degree of air saturation:

$$S_{a-cri} = 1 - \theta_a/n$$

$$S_{a-l} = 1 - \theta_r/n$$

Air-entry water content (θ_a) and residue water content (θ_r) are determined from the pF(q) curve.

Diffusion coefficient of dry soils D_{dry} :

$$D_{dry} = n^{X_{dry}}$$

X_{dry} is the particle shape factor, estimated by fitting the D_{dry} model to measured (n, D_{dry}) data.

Parameters b and c :

Determined by fitting the above $D(q)$ model to measured (S_a, D) data.

Determining soil water retention and gas diffusivity: validation

Measurement on repacked soil columns

Sand:

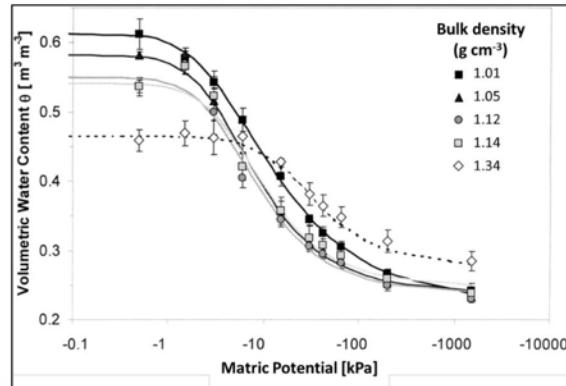
sand - 94%, clay - 5%

r_b : 1.40, 1.50, 1.60 $Mg\ m^{-3}$

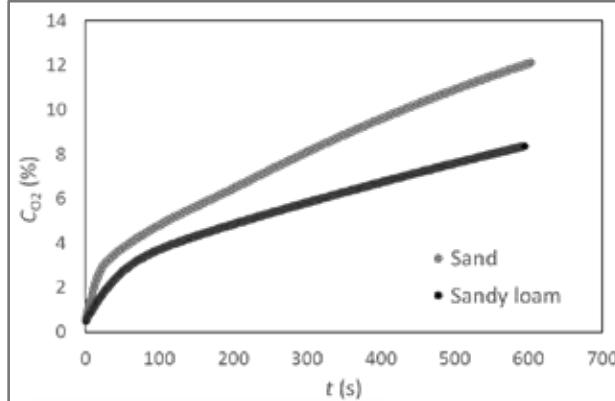
Sandy loam:

sand - 39%, clay - 1%

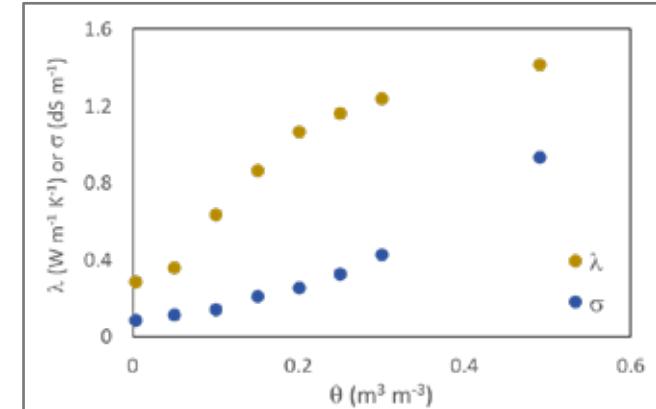
r_b : 1.35, 1.45, 1.55 $Mg\ m^{-3}$



$h(q)$
Sand box, pressure plate



$D(q)$
One-chamber method



$\lambda (q), \sigma (q)$
Thermo-TDR technology

Results: thermo-TDR Measured $I(q)$, $pF(q)$, $D(q)$ curves

Ü Thermal conductivity curve: $I(q)$

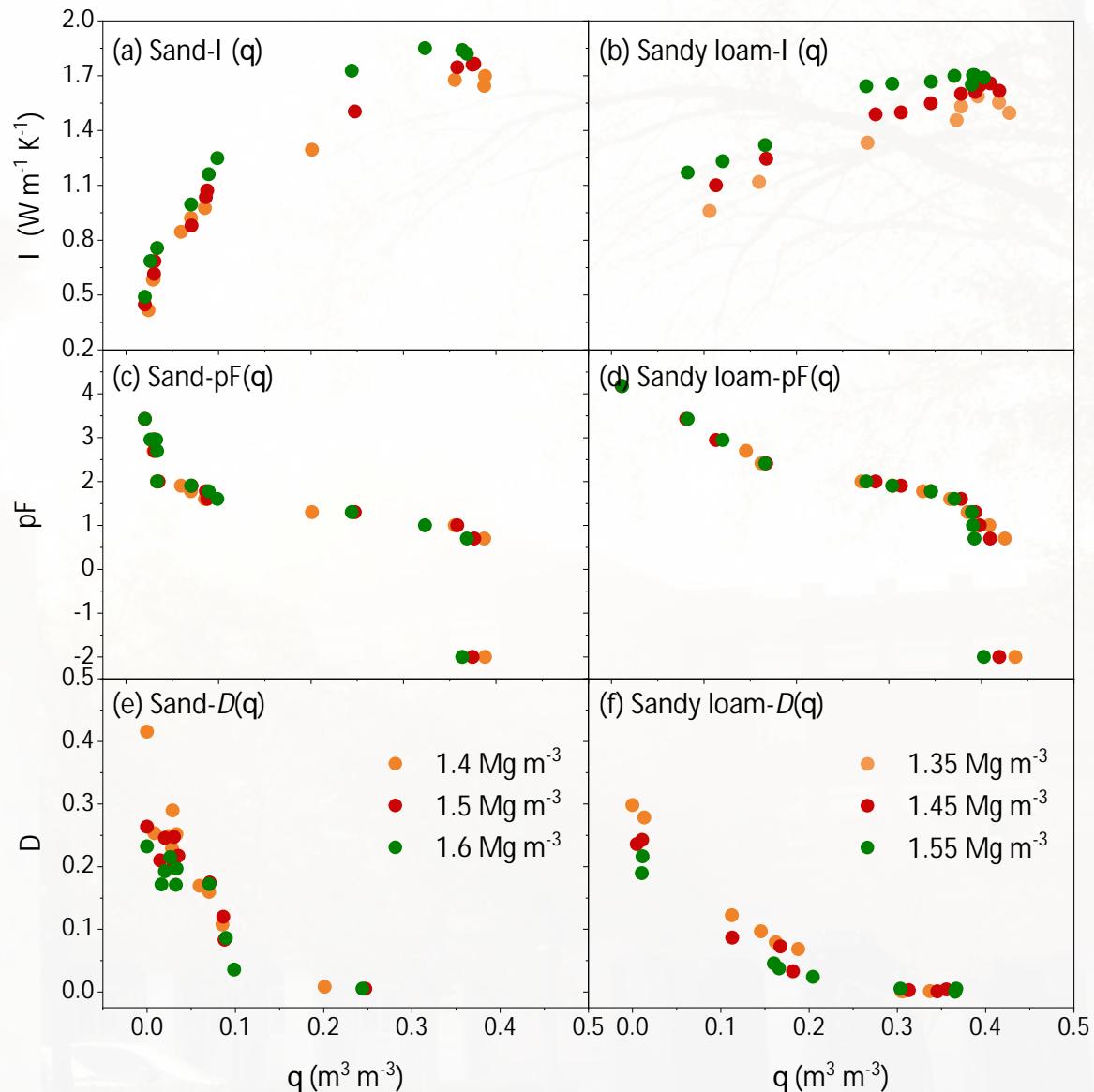
- I increases with both sand content and r_b
- At equivalent q , $I_{\text{sand}} > I_{\text{sandy loam}}$

Ü Water retention curve: $pF(q)$

- Sand shows lower water retention capacity;
- r_b : slightly improves water retention, more pronounced in sandy loam.

Ü Gas Diffusivity: $D(q)$

- Sand requires higher air content (lower q) to activate dominant air-phase diffusion;
- D decreases at greater r_b values, more severe in sandy loam.



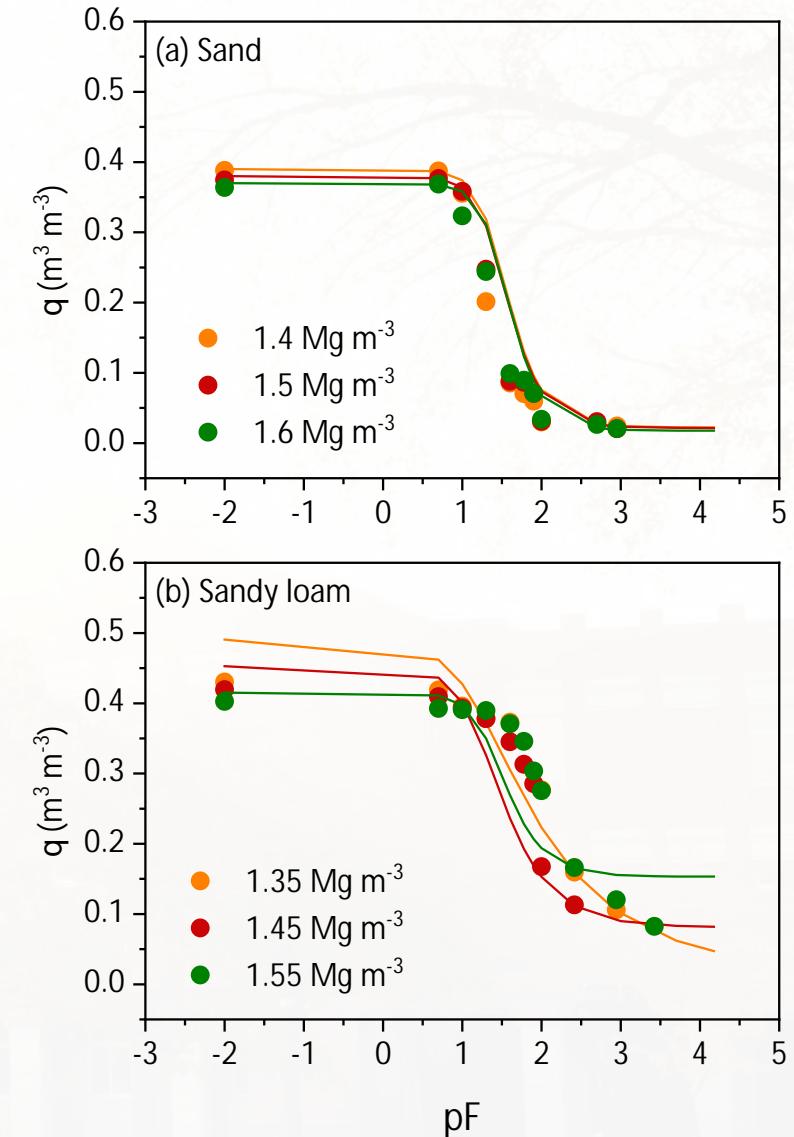
Results: pF(q) curve derived from I (q) curve

Model performance:

- Model fits the measured data well for both soils;
- Model is applicable for predicting water retention behavior under various bulk density and texture scenarios.

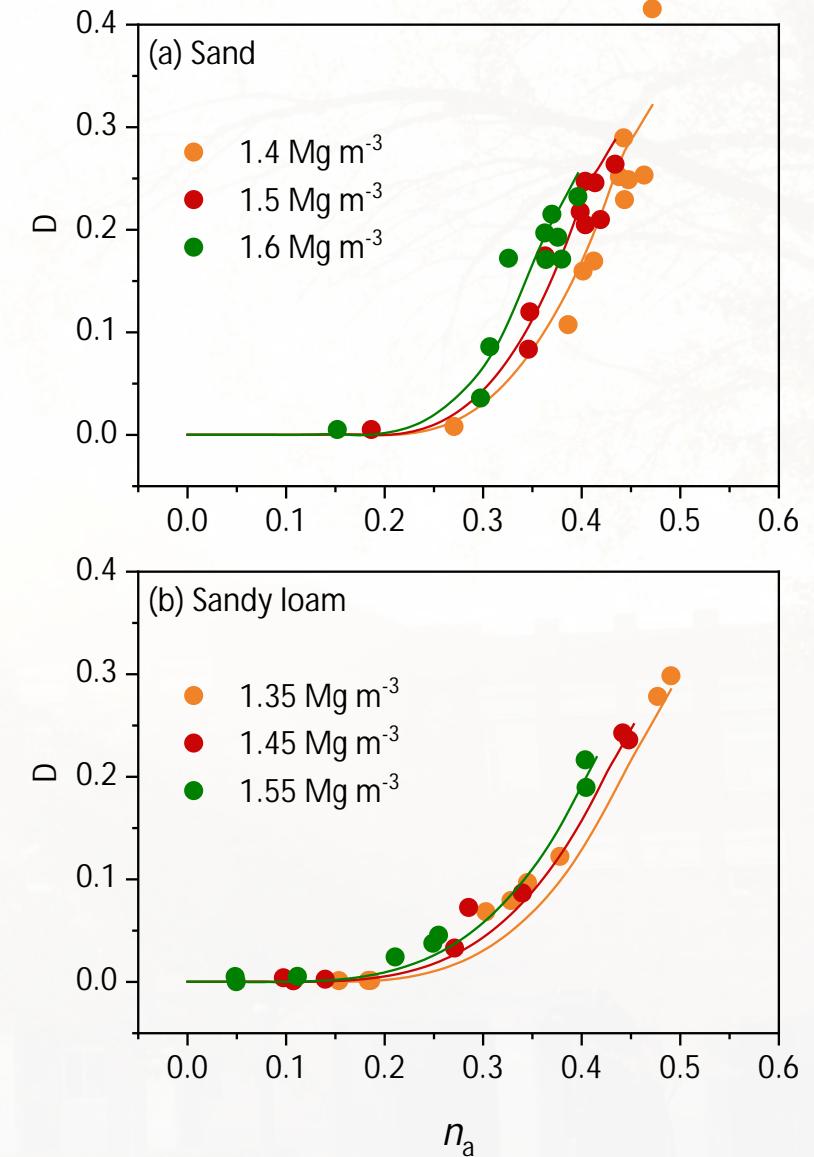
Model errors:

- Acceptable: RMSEs in estimated q : $< 0.055 \text{ m}^3 \text{ m}^{-3}$;
- Slight overestimation near saturation.

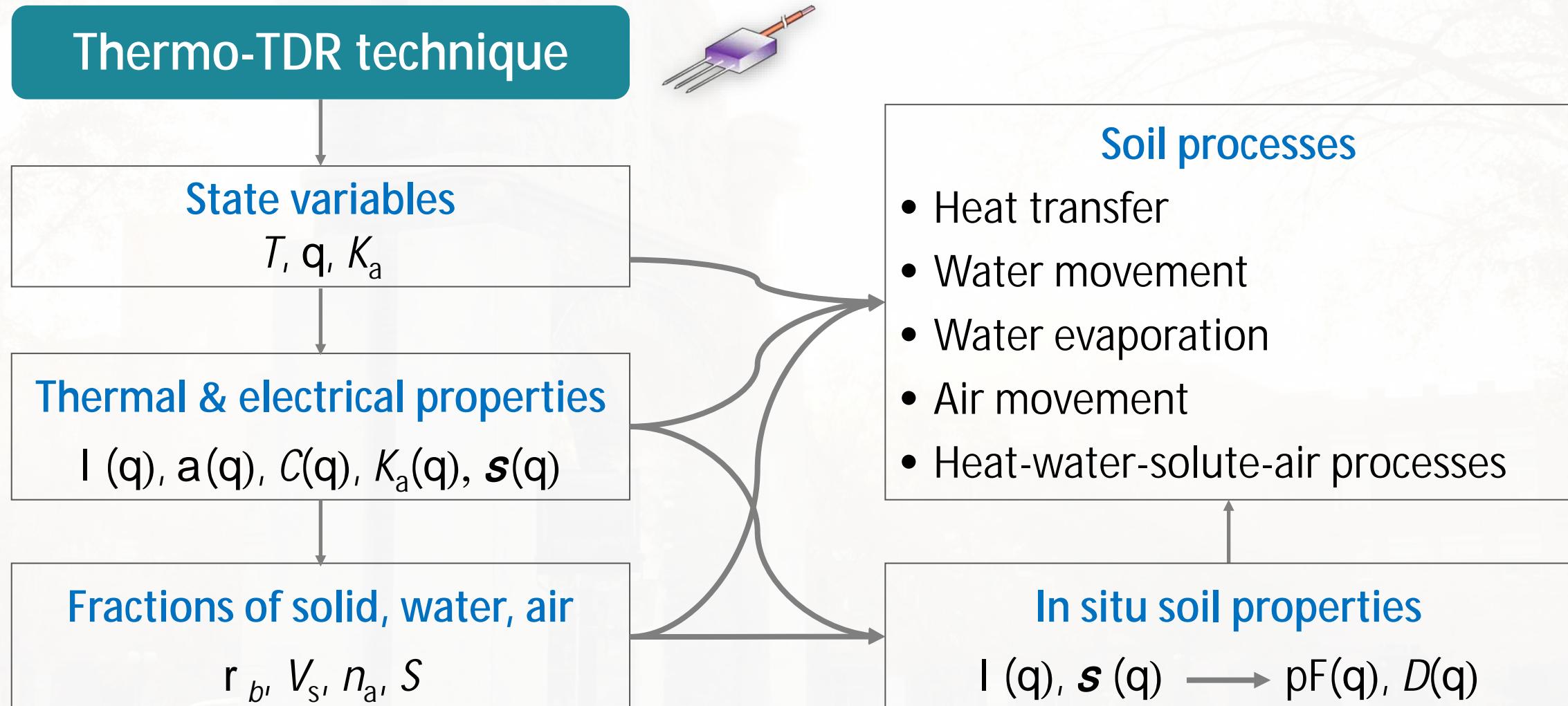


Results: $D(q)$ curve derived from $pF(q)$ curve

- **Performance:** Worked well for both soils across full range of air-filled porosities.
- **Errors:** RMSE of estimated D is low: 0.034 for sand and 0.017 for sandy loam.
- **Robustness:** Accurately captured the effect of bulk density on air diffusivity, as evidenced by the consistent downward shift of the curves with increasing bulk density.



Summary



Acknowledgements

National Natural Science Foundation of China
(42407412 and 42107313)

National Key Research and Development Program
of China (2023YFD1500301)